

FOR ERRATA

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TO BASIC DOCUMENT

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R-5214

DESIGN INFORMATION REPORT FOR THE  
THOR YLR79-NA-13 MAIN ENGINE AND  
LR101-NA-11 VERNIER ENGINES

**ROCKETDYNE**

A DIVISION OF NORTH AMERICAN AVIATION, INC.

6633 CANOGA AVENUE  
CANOGA PARK, CALIFORNIA

Contract AF04(695)-306

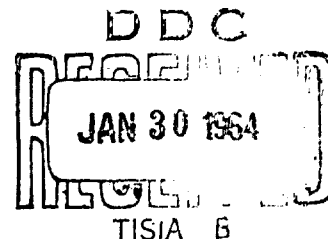
Part I, Item 2b as  
Amended by Item VI of  
Request For Service  
Order 306-64-03

**PREPARED BY**

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**APPROVED BY**

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J. J. Griffin  
Atlas/Thor Program Manager

NO. OF PAGES 79 & viii**REVISIONS**DATE 30 July 1963

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30 Jan 1964	WNP	7	Updated Drawing 104653

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A DIVISION OF NORTH AMERICAN AVIATION, INC.

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FOREWORD

This Design Information Report was prepared in compliance with AF04(695)-306, Part I, Item 2b as amended by Item VI of Request for Service Order 306-64-03.

ABSTRACT

This report consists of three major sections: (1) a description of the LV-2A propulsion system, consisting of the YLR79-NA-13 main engine and the LRI01-NA-11 vernier engines, (2) installation and geometry information, and (3) performance data.

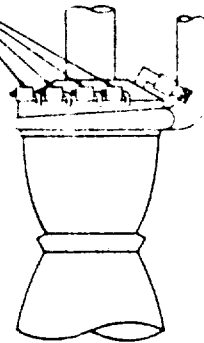


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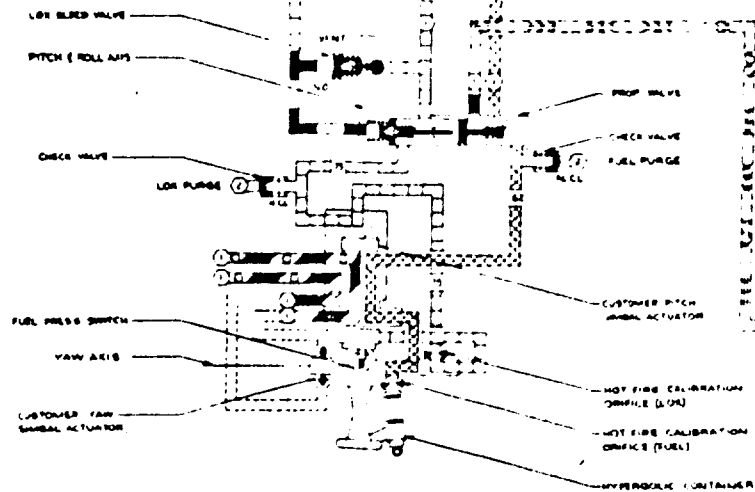
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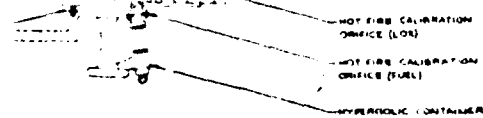
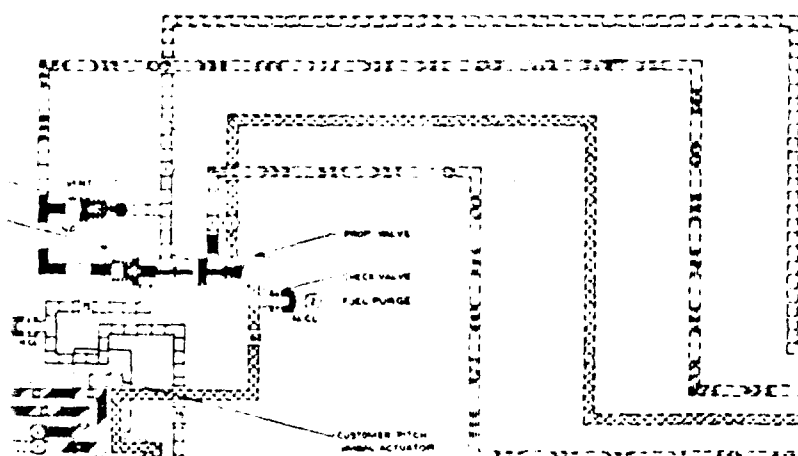
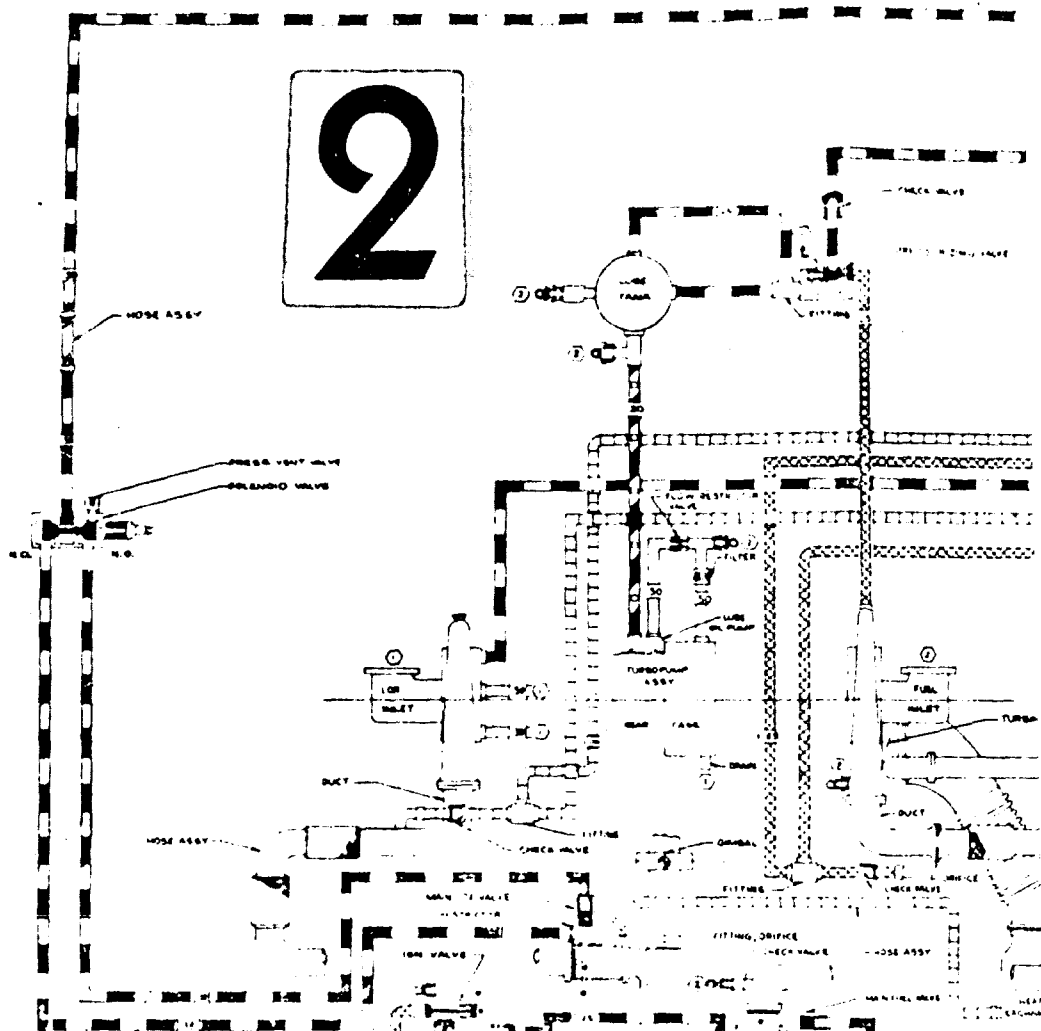
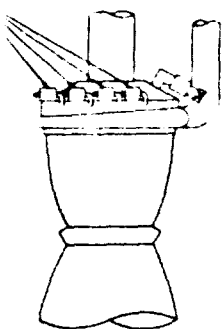
FUEL RELEASE PRESSURE SWITCHES



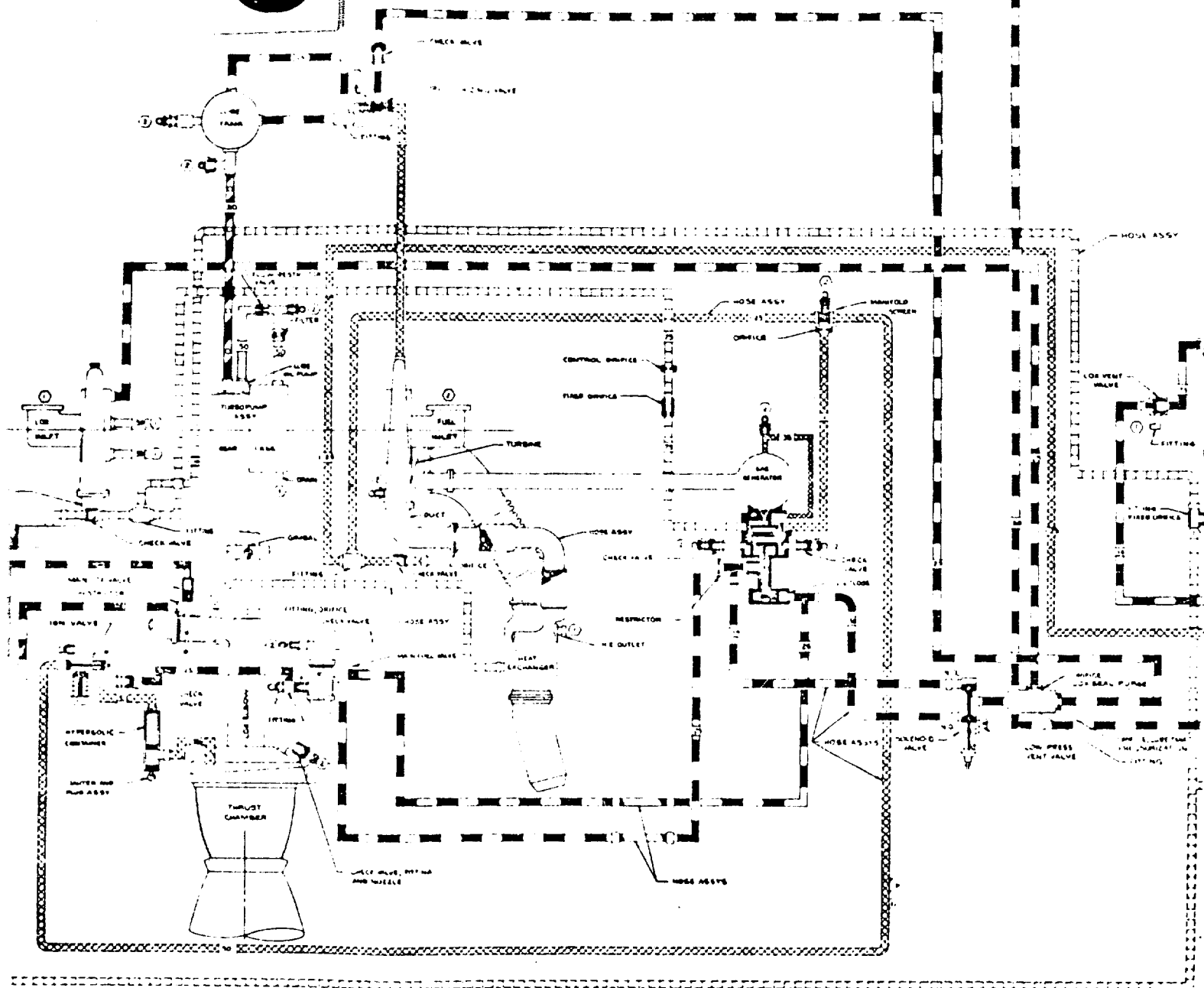
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REVISIONS WITH CHANNELS

1. REVISED FORMAT  
2. ADDRESS PHENAMATIC CODE

SCHEMATIC CODE

HOT GAS		
PNEUMATIC		
HYDRAULIC		
LUBE		
OXYGEN		
FUEL		

R-5214

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① 2 SERVICE CONNECTIONS  
① 4 CUSTOMER CONNECTIONS

কম্পিউটার, ইন্টারনেট, মোবাইল ফোন, ইত্যাদি

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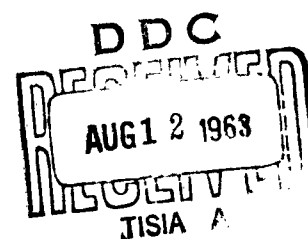
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**ROCKETDYNE**

A DIVISION OF NORTH AMERICAN AVIATION, INC.

CANOGA PARK, CALIFORNIA



R-5214

DESIGN INFORMATION REPORT FOR THE  
LV-2A PROPULSION SYSTEM  
(YLR79-NA-13 Main Engine and  
LR101-NA-11 Vernier Engines)

**ROCKETDYNE**

A DIVISION OF NORTH AMERICAN AVIATION, INC.

6633 CANOGA AVENUE  
CANOGA PARK, CALIFORNIA

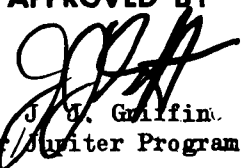
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DATE 30 July 1963

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### FOREWORD

This Design Information Report was prepared in compliance with AF04(695)-306, Part I, Item 2b as amended by Item VI of Request for Service Order 306-63-01.

### ABSTRACT

This report consists of three major sections: (1) a description of the LV-2A propulsion system, consisting of the YLR79-NA-13 main engine and the LR101-NA-11 vernier engines, (2) installation and geometry information, and (3) performance data.

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INTRODUCTION

The function of this report is to compile in handbook form the various items of engine design information in which the customer has expressed prime interest. It is also intended as an aid to design and to ensure compatibility of missile structure and the LV-2A propulsion system.

This report is not intended to supersede or duplicate existing model specification or Rocketdyne Field Service manuals.

Additions and revisions will be issued periodically to maintain this report on a current basis.

SECTION I: PROPULSION SYSTEM DESCRIPTION  
AND OPERATING REQUIREMENTS

PROPULSION SYSTEM DESCRIPTION

The LV-2A propulsion system (Fig. 1 ) is composed of a booster main engine (Air Force designation YLR79-NA-13) and two vernier engines (Air Force designation LRL01-NA-11) which provide roll control and finite impulse adjustment at the end of flight. The complete propulsion unit is a liquid bipropellant system and operates on liquid oxygen and RJ-1 hydrocarbon fuel. The main engine has a maximum over-all length of 142.587 inches and a maximum envelope diameter of 76.117 inches. The engine is rated to deliver a thrust of 170,000 pounds under sea-level conditions for a mainstage duration of 175 seconds. An additional 2120 pounds total thrust is developed by the two vernier engines during pump-fed operation and 1660 pounds total thrust during tank-fed operation for approximately 9 seconds after main engine cutoff.

Both the main and vernier engines are of the single-start, fixed-thrust type with no provision for restarting the engines or for intermediate thrust control. System propellant flowrates are controlled exclusively by orificing. All thrust chambers are gimbal-mounted for trajectory control and adjustment. The main engine thrust chamber is provided with a baffled injector. Ignition in all chambers is by means of hypergolic fluid. The entire propulsion system is controlled by an electrical system and a pneumatic system. Nitrogen gas is used in the latter system to operate all pneumatically controlled valves. Electrical power to control the engines is supplied from an external source until the missile is airborne, after which the missile's electrical system supplies the required electrical power.

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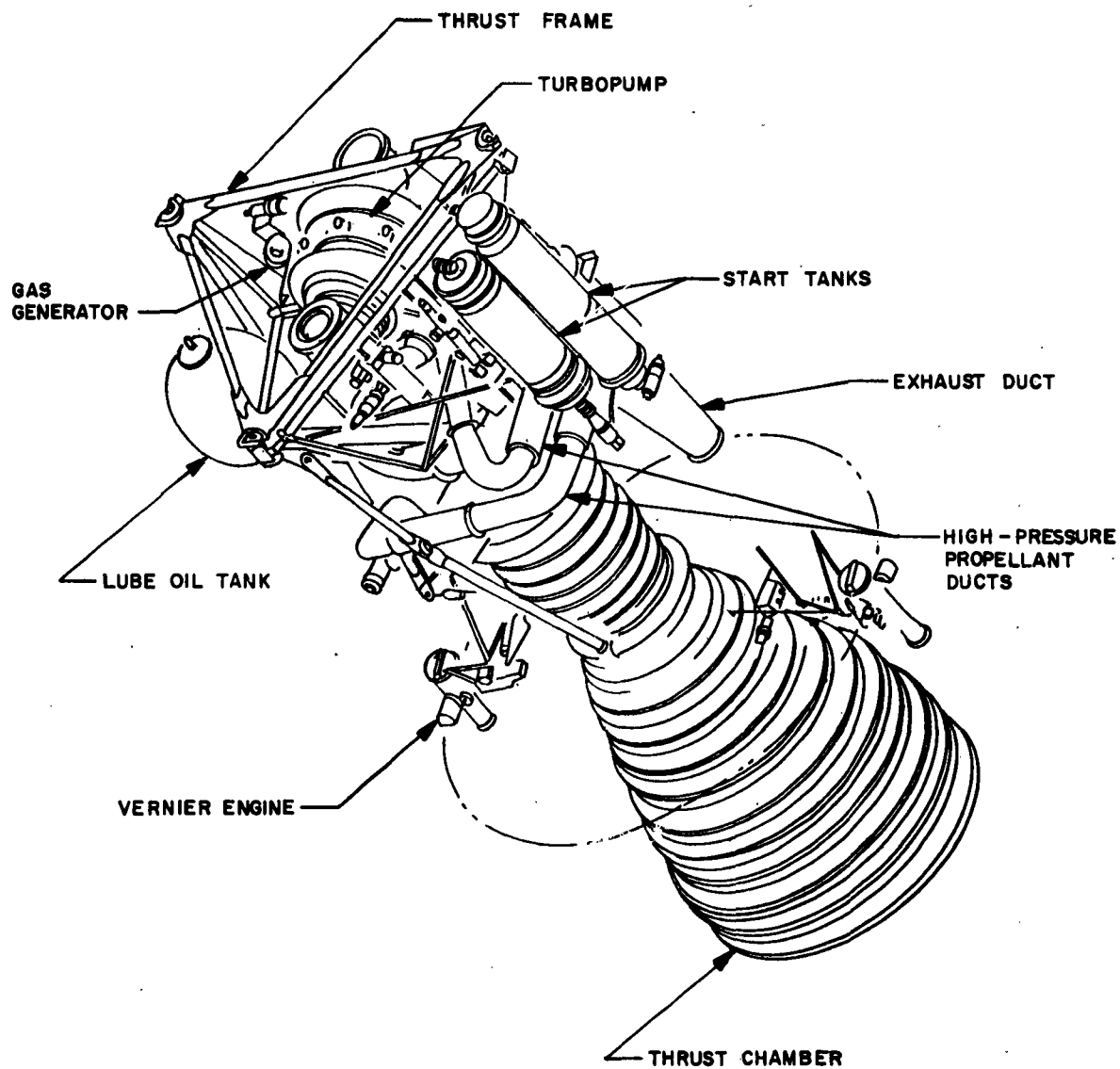


Figure 1. LV-2A Propulsion System

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The turbopump for the main engine provides one accessory drive pad to be used for the attachment of missile accessories. The accessory drive pad is capable of delivering 100 horsepower for the intended flight duration. The accessory drive pad conforms to the Air Force-Navy Aeronautical Design Standard AND20002-X11-K, with the following exceptions:

1. Maximum speed is 4200 rpm; minimum speed is 3650 rpm.
2. Direction of rotation is counterclockwise facing the accessory drive pad.
3. No provision is made for lubrication of accessories.

One single-element heat exchanger for gasifying liquid oxygen to be used as LOX tank pressurant is installed in the turbopump exhaust duct.

A list of propulsion system installation drawings is given in Table 1 .

A schematic of the main engine and details of the control orifice locations are shown in Drawings 104653 and 408113. Control orifice locations for the LR101-NA-11 vernier engines are shown in Drawing 350670.

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TABLE 1

LV-2A PROPULSION SYSTEM INSTALLATION DRAWINGS

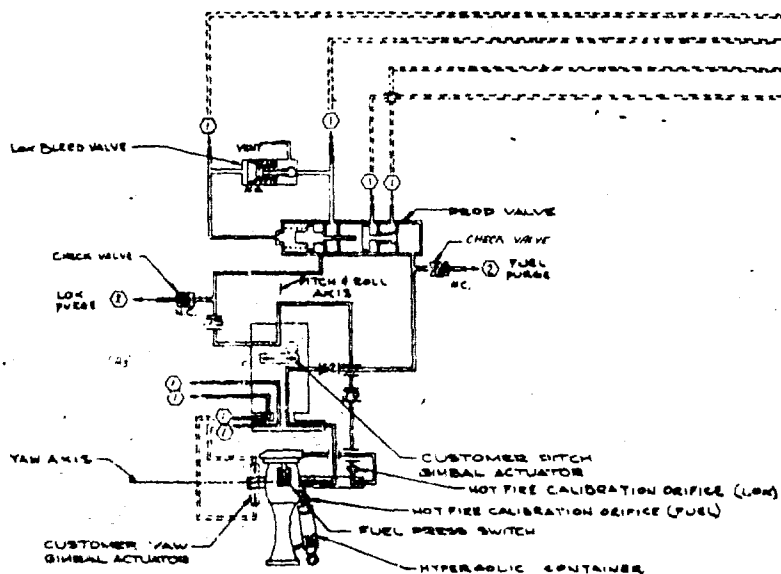
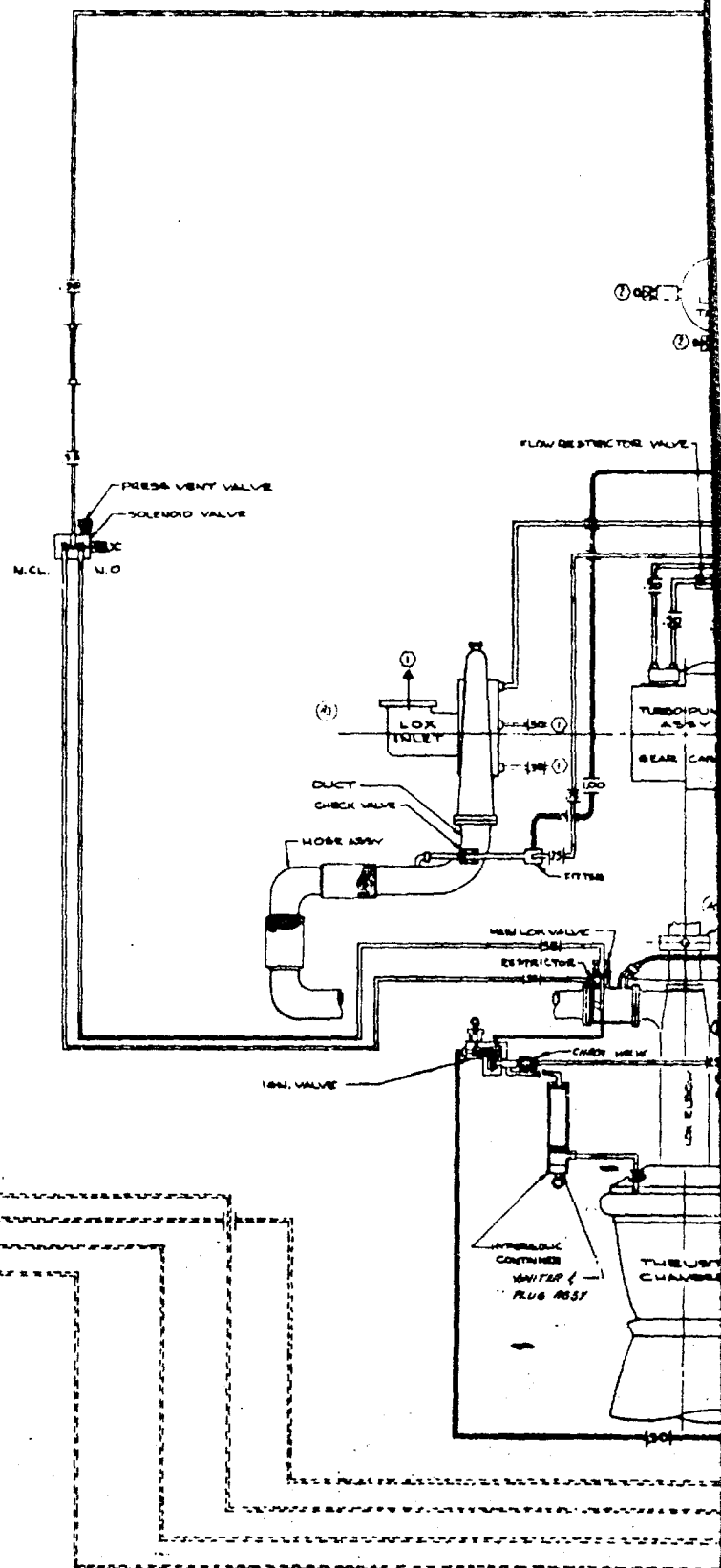
YLR79-NA-13 Main Engine

Engine Assembly Drawing	104651
Major Component Installation	104652
Start System Installation	308451
Gas Generator and Exhaust Installation	308452
Propellant Feed System Installation	407226
Electrical Equipment Installation	502101
Pneumatic System Installation	556351
Lube System Installation	556352
Loose Equipment List	651601

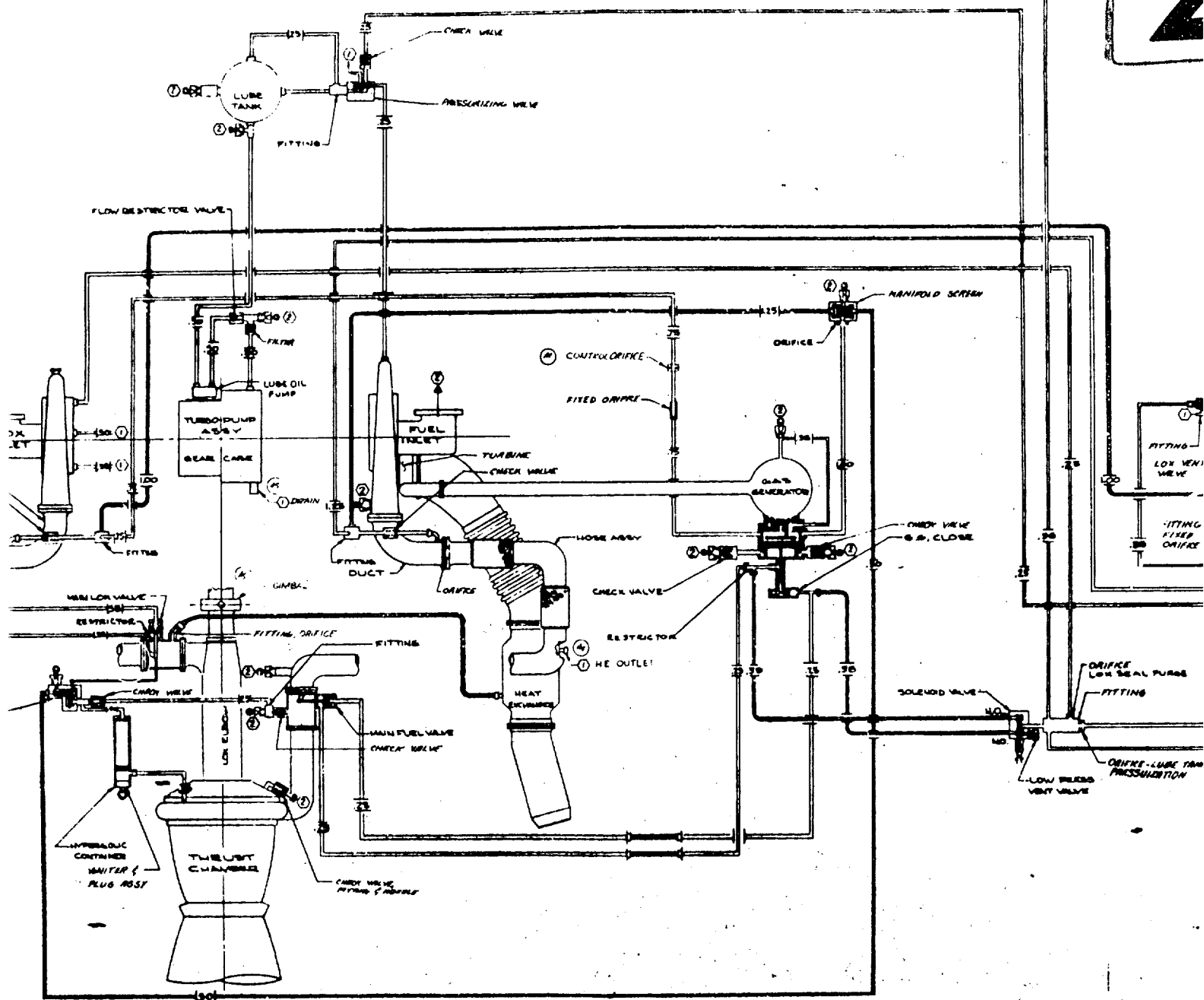
LR101-NA-11 Vernier Engine

Engine Assembly Drawing	350655
Gimbal Body Installation	350660
Propellant Feed System Installation	350665
Orifice and Accessory Installation	350670
Loose Equipment List	350674
Electrical Installation	350675

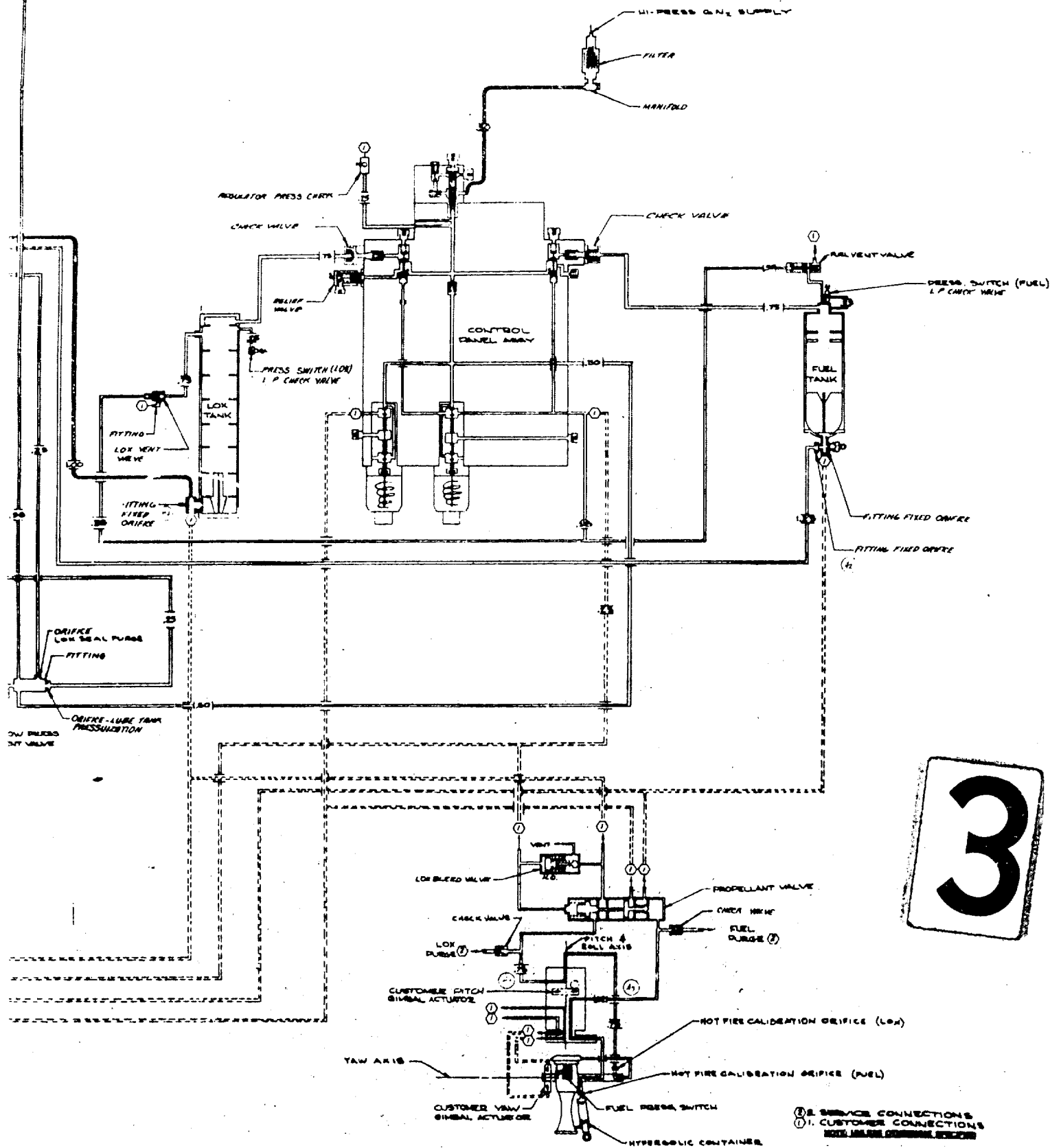
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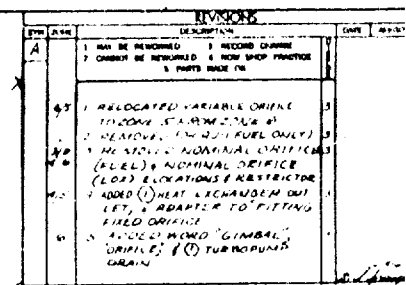
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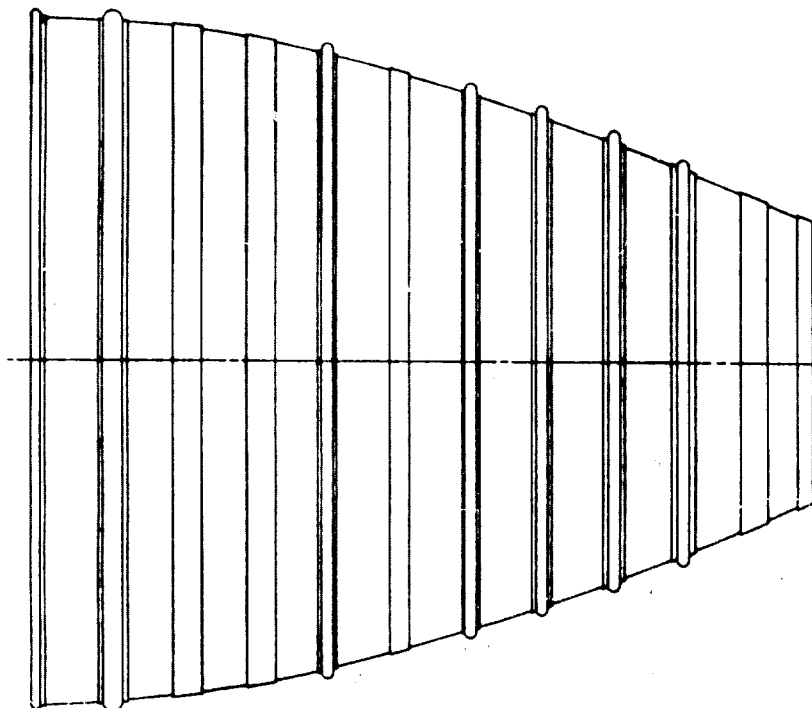
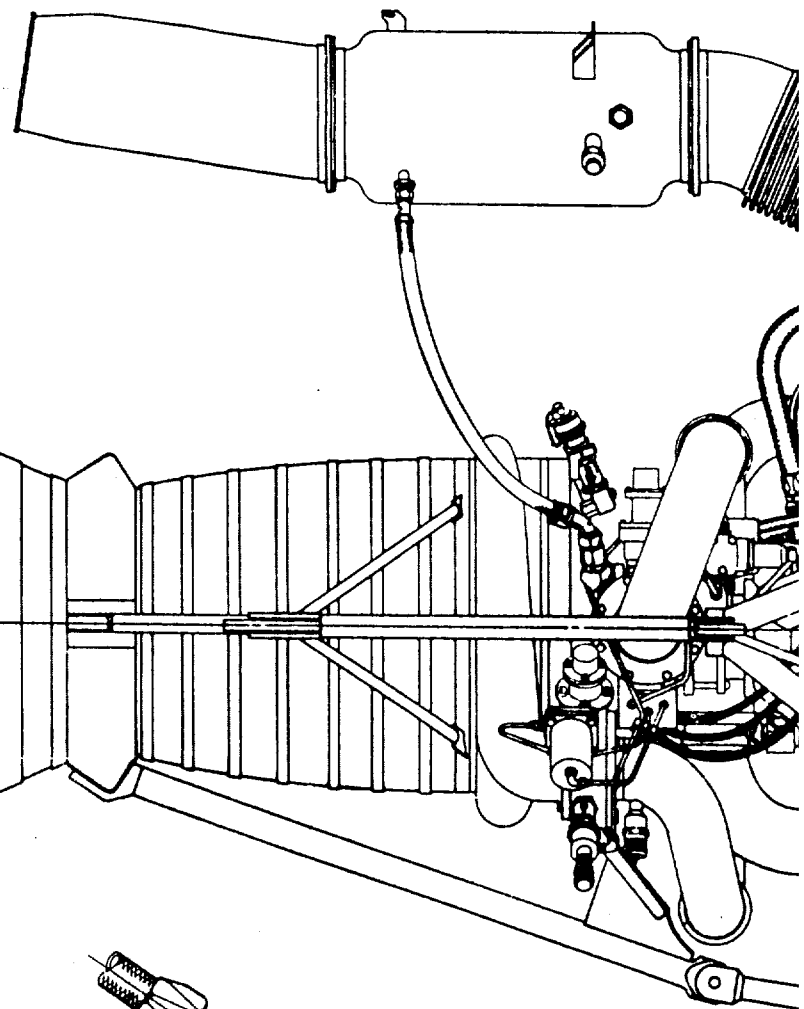






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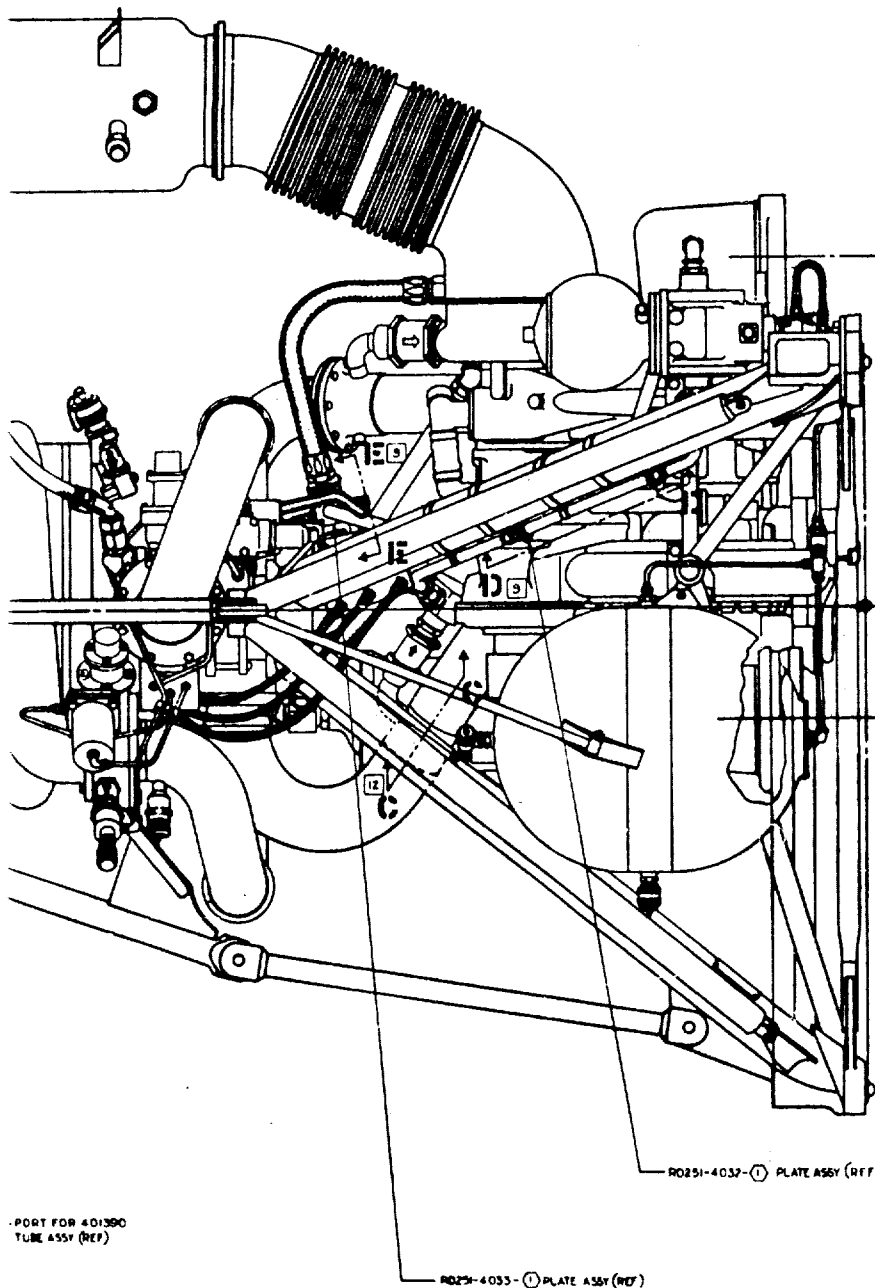


- 521916-3000 HOSE ASSY (REF)
- AN815-160 UNION (REF)
- 401858 FITTING (REF)  
ROTATED 90° FOR CLARITY
- HA5-2603279 CHECK VALVE (REF)
- PORT FOR 401300  
TUBE ASSY (REF)
- 401046 DUCT ASSY OF (REF)

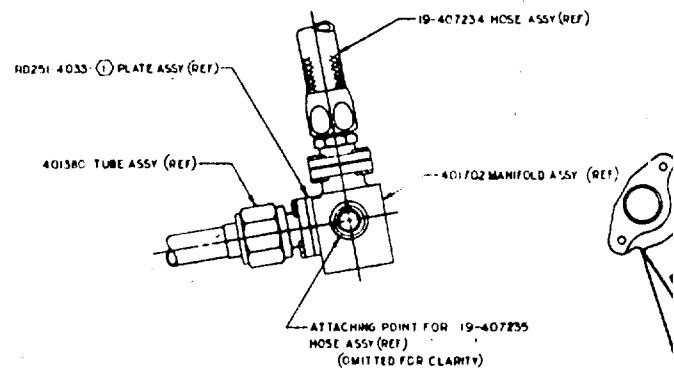
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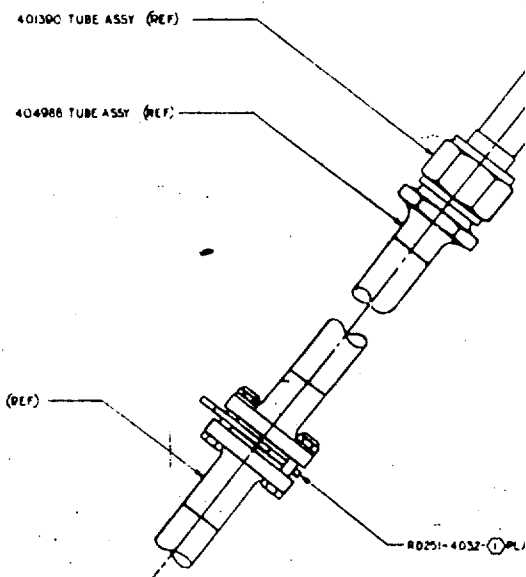




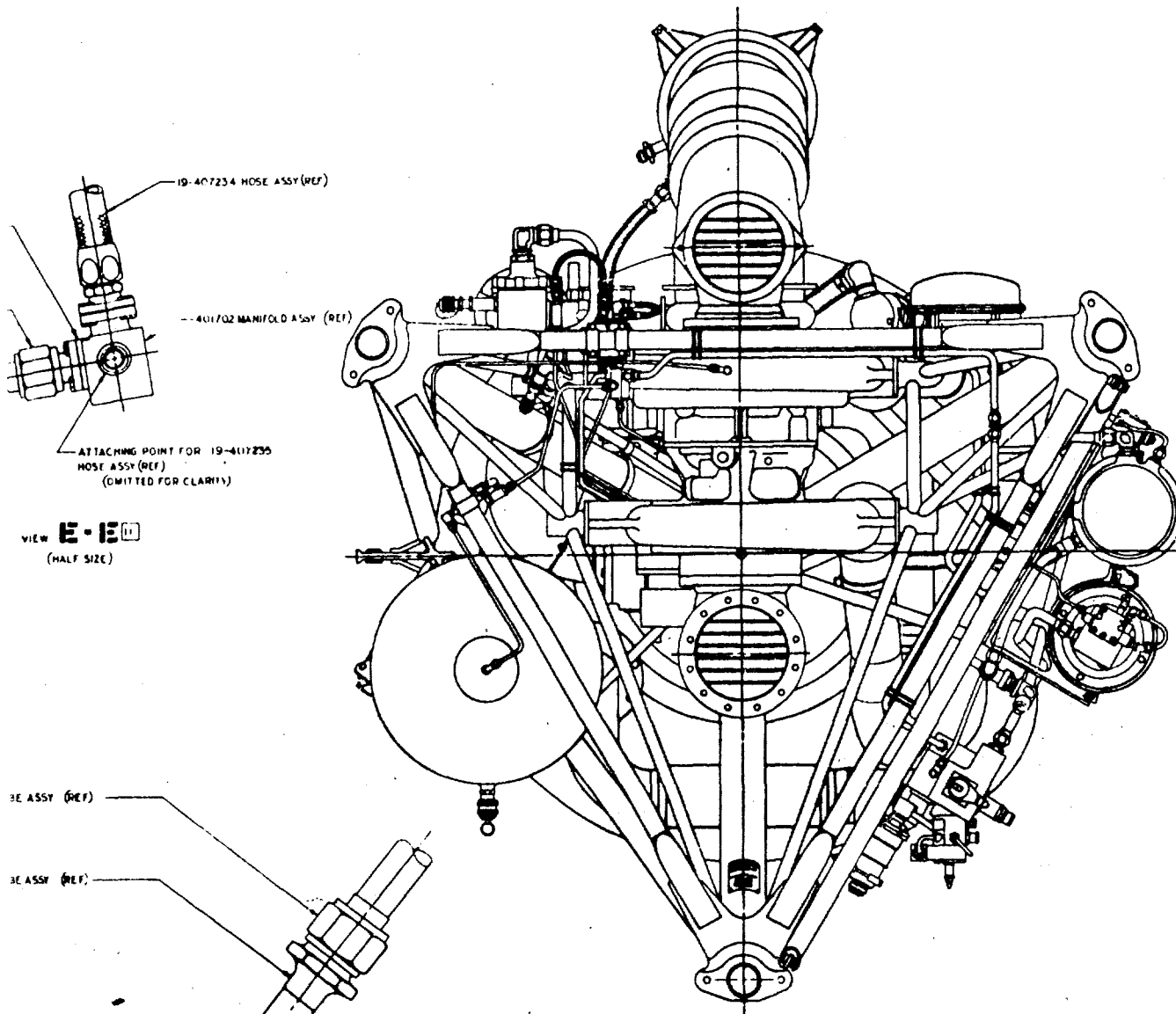
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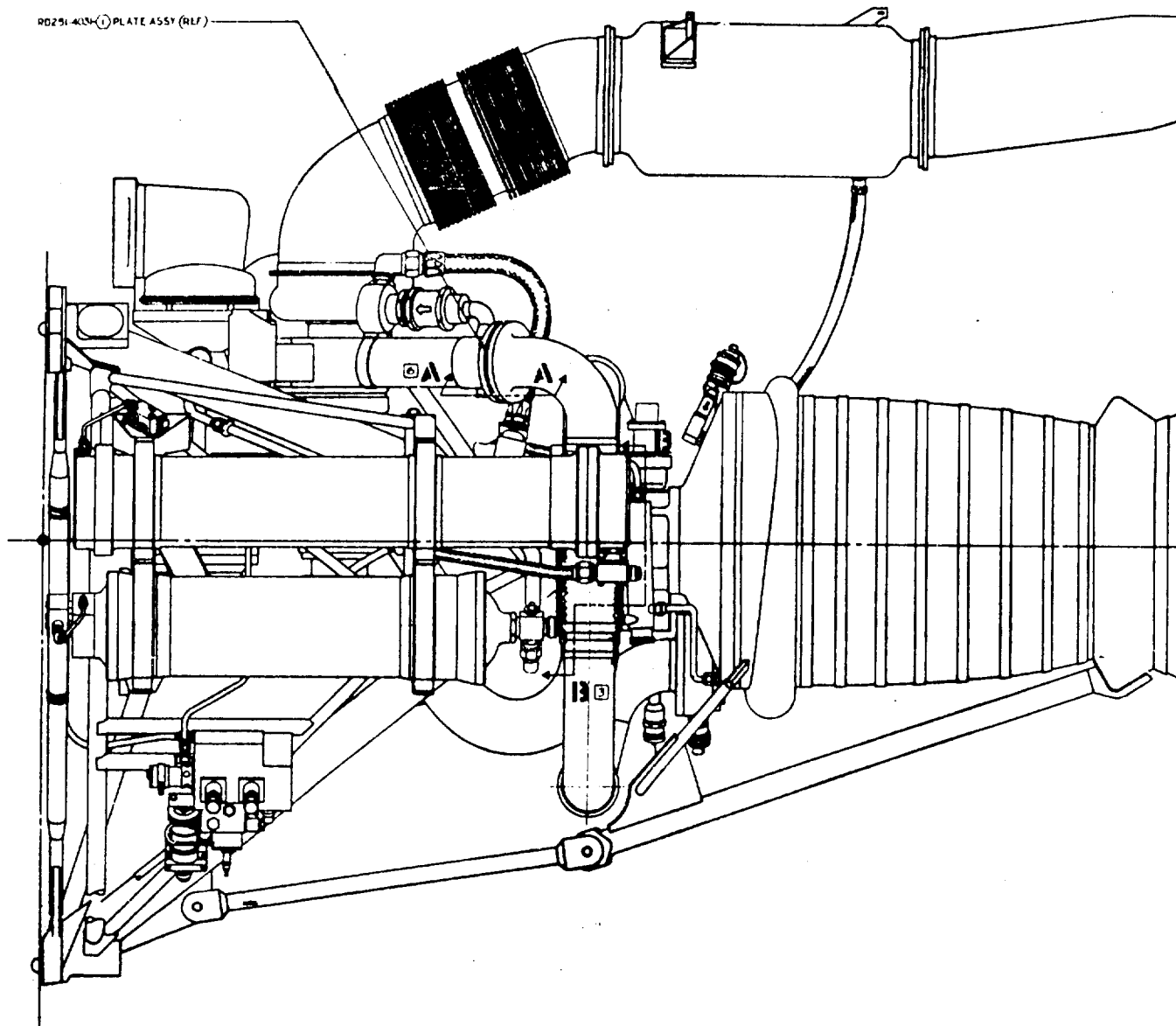
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VIEW D-D  
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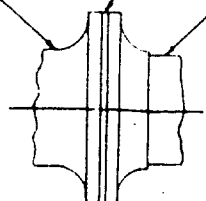
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RD251-403-1 PLATE ASSY (REF)

40179 DUCT (REF)

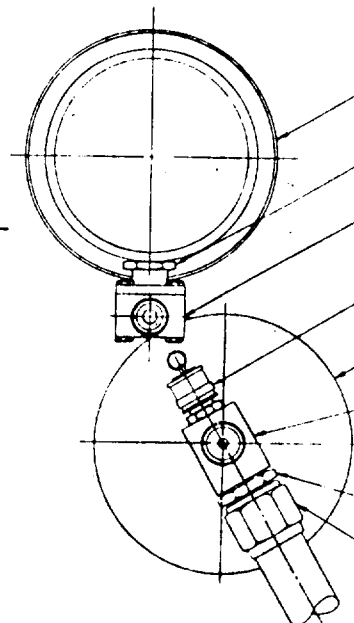
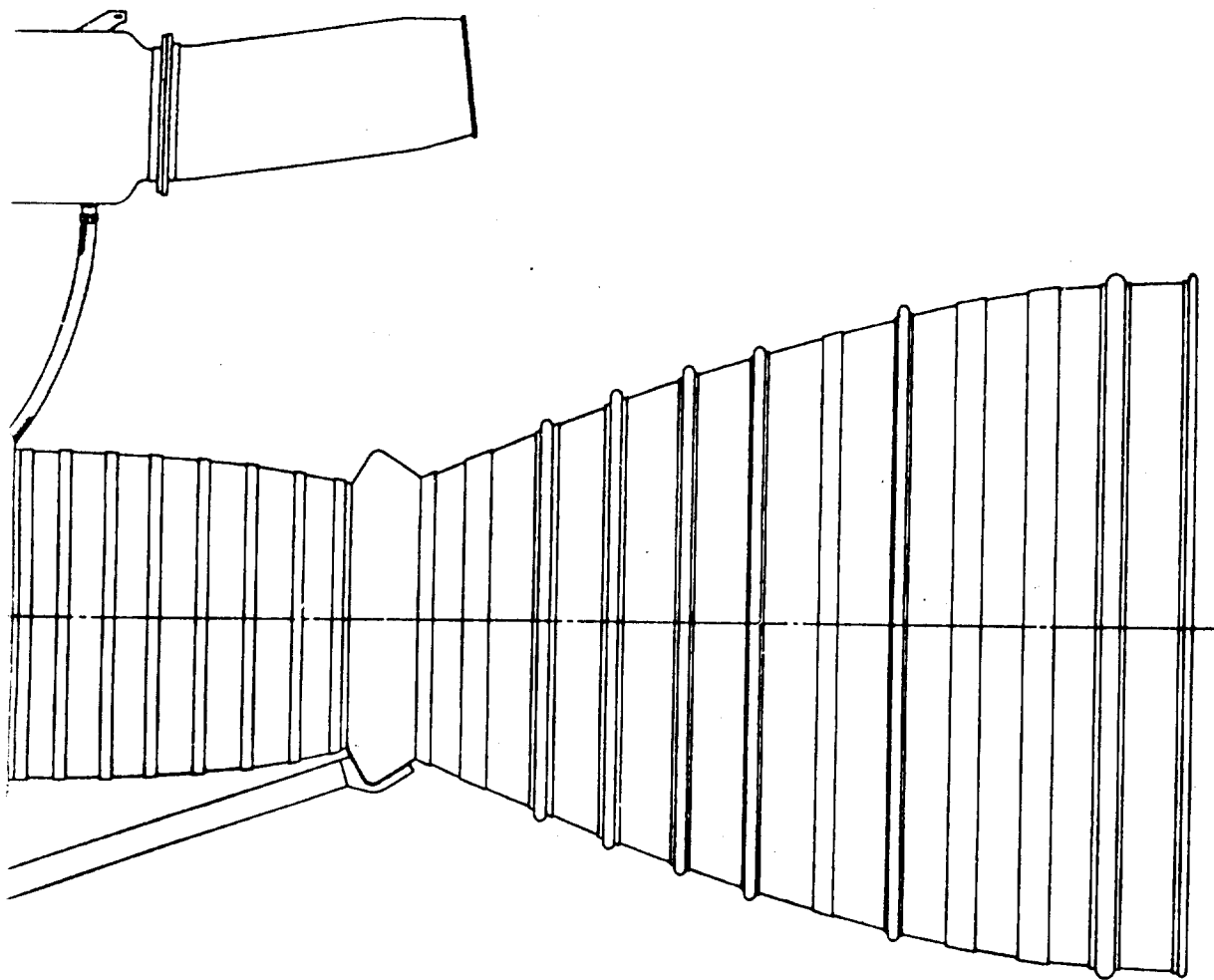
401409 HOSE ASSY (REF)



VIEW A-A

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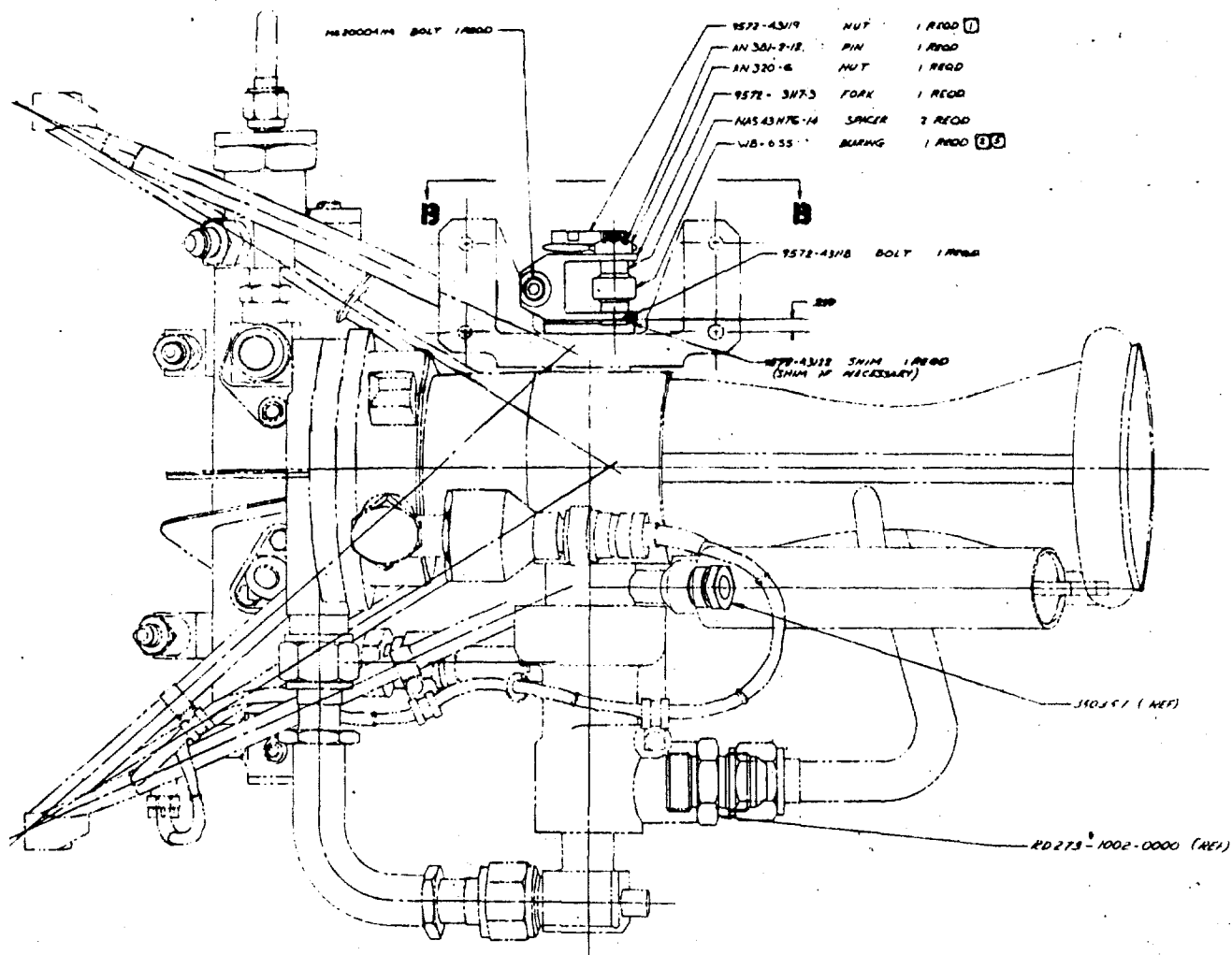


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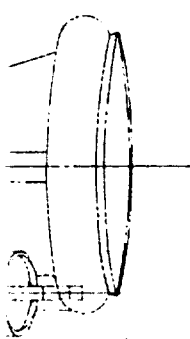




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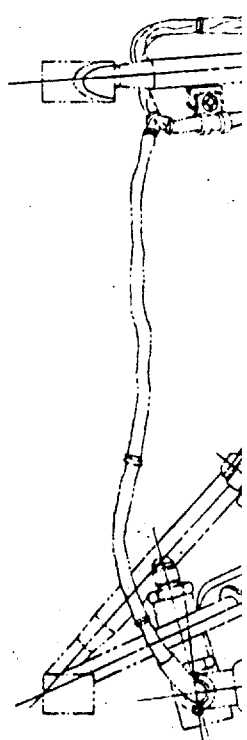
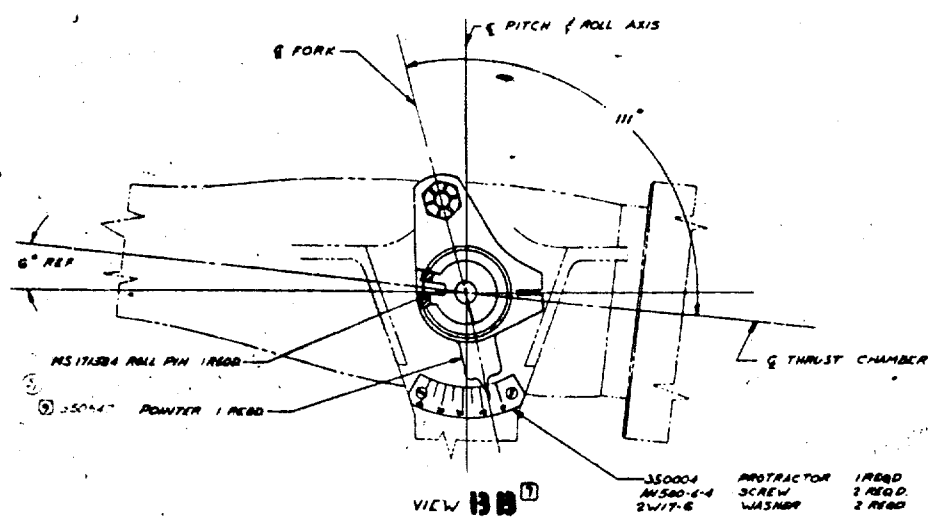
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MAE 26.501 SWITCH  
MS 1725-4 PACKING

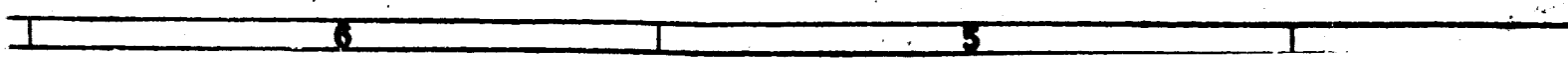


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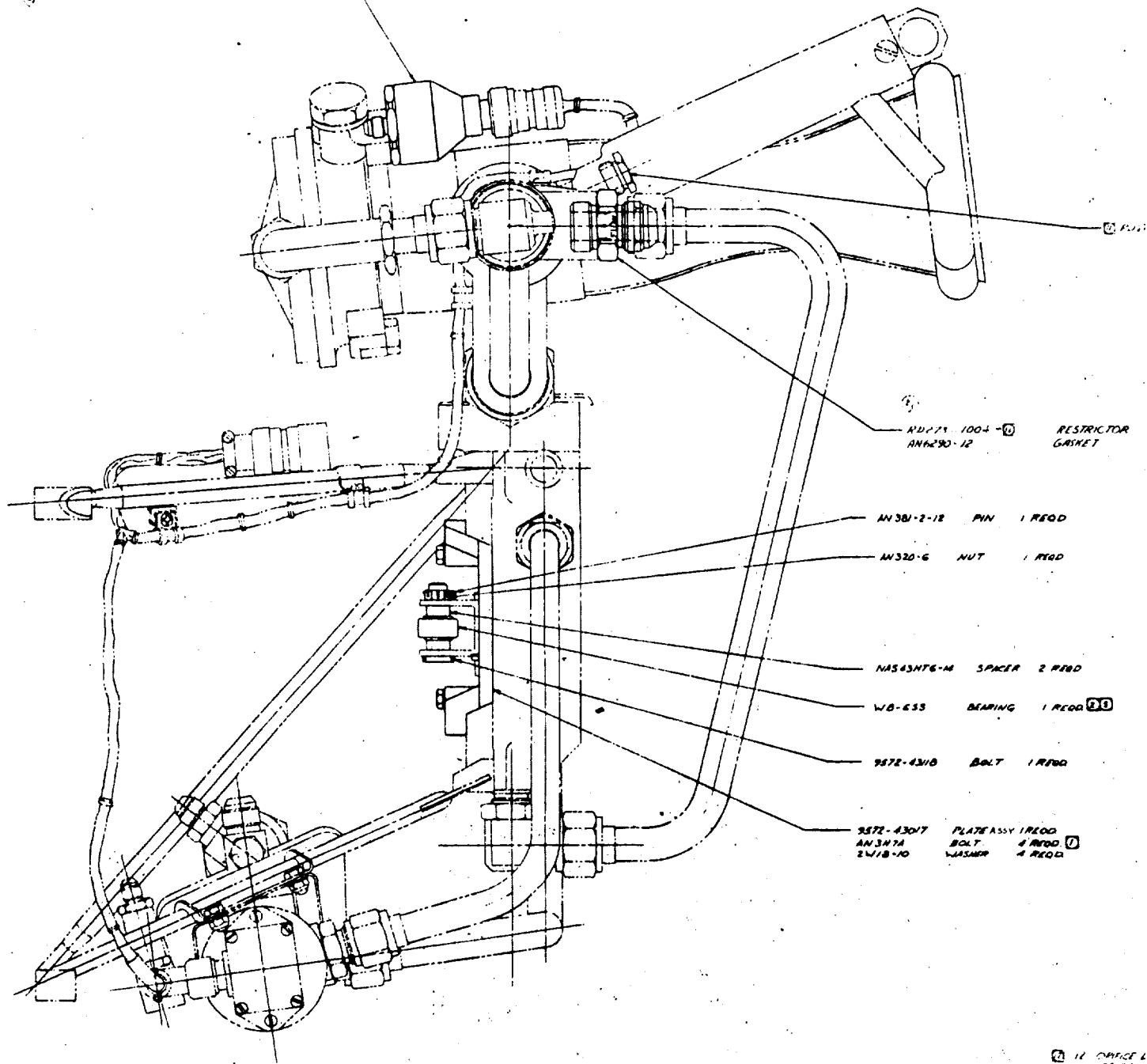
10273-1002-0000 (REF)



2



1. WAS 26501 SWITCH 1 REQD  
 2. MOUNTING & PACKING 1 REQD



AN 271-100-1 RESTRICTOR GASKET  
 AN 290-12

AN 301-2-12 PIN 1 REQD

AN 320-6 NUT 1 REQD

NAS 43HT6-M SPACER 2 REQD

WB-655 BEARING 1 REQD 20

9572-4310 BOLT 1 REQD

9572-4307 PLATE ASSY 1 REQD  
 AN 347A BOLT 4 REQD 7  
 2 1/8-10 WASHER 4 REQD

12. OFFICE & IDENTIFY PERFECT
11. PASSIVATE
10. VERIFY CL. RA 2200
9. COMMERCIAL BEFORE OR WARE INSTALL
8. WARE INSTALL
7. CLEAN PER
6. INST 11 THRU
5. ALTERNATE 1 FROM SOUT
4. INSTALL PER LOW SERV
3. 5-125-111-AN
2. PAY BY PWD
1. INSTALL LOCK

3

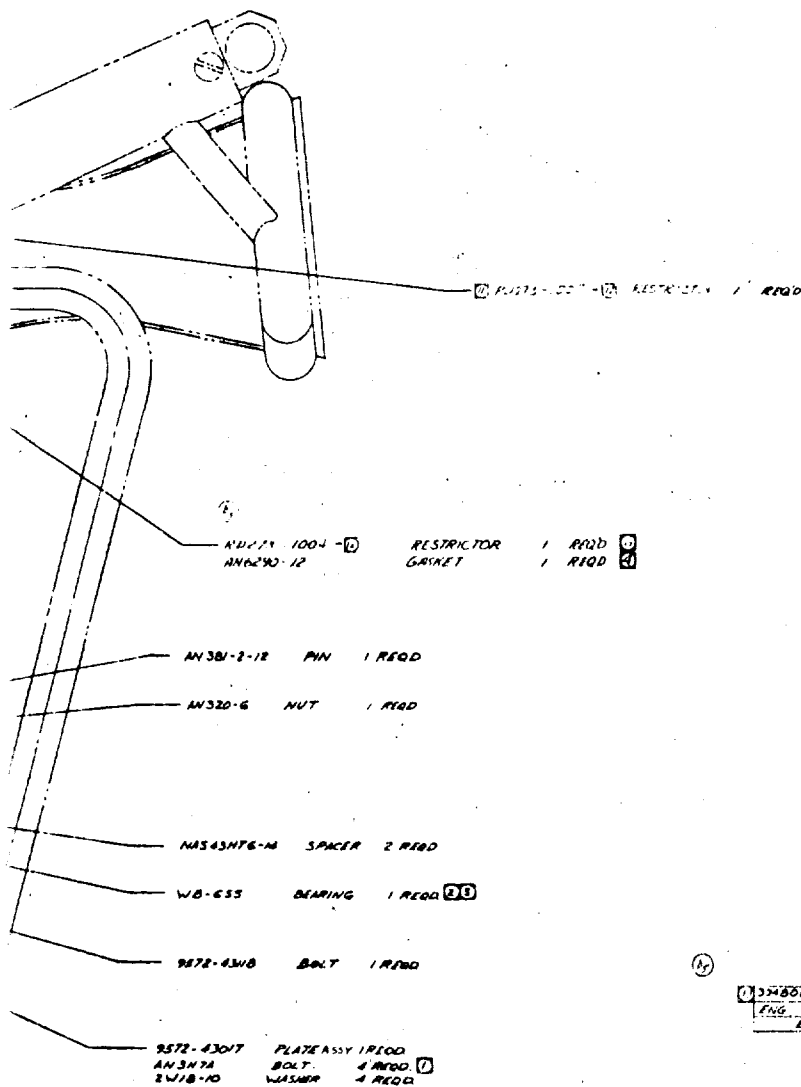


FIG.	THRU	MODEL
334601	334934	4400-44
EFFECTIVE ON		

350647 SUPERSEDES 350003 FOR FUTURE PROCUREMENT

12. PRICE DIA TO BE DETERMINED BY RADIO-032. IDENTIFY ALTERED PARTS PER RADIO-032 TO REFLECT THE OFFICE DIA.
  11. PASSIVATE PER RADIO-032.
  10. VERIFY COMPLIANCE WITH DIMENSIONS RADIO-032 PRIOR TO INSTALLATION.
  9. COMMERCIAL PART, SEE WAS SPEC BEFORE ORDERING.
  8. WIRE INSTALLATION PER RADIO-001.
  7. CLEAN PER RADIO-004 (10X SERVICE).
  6. INST LL THREADED FASTENERS PER RADIO-002.
  5. ALTERNATE PART NO BND-6710, MAY BE PURCHASED FROM SOUTHWEST PRODUCTS CO. QUARTZ, CALIF.
  4. INSTALL PER PARADISE & LUBRICATE RE RADIO-004 FOR LONG SERVICE LIFE.
  3. INSTALL AFTER 4-8 HRS OVEN DRYING TO DR-RECOMMENDED BY OXYGENATION TEST.
  2. MAY BE PURCHASED FROM STERIL-AD-15N HAS, AURORA, IL.
  1. INSTALL LOCK WIRE PER RADIO-002.
- NOTE: INSTALL OTHERS AS SPECIFIED



<b>DRILL HOLE TOLERANCES</b> 1/8" TO 1/4" ± .005 1/4" TO 3/8" ± .005 3/8" TO 1/2" ± .005 1/2" TO 3/4" ± .005 3/4" TO 1" ± .005 1" TO 1 1/4" ± .005 1 1/4" TO 1 1/2" ± .005 1 1/2" TO 1 3/4" ± .005 1 3/4" TO 2" ± .005 2" TO 2 1/4" ± .005 2 1/4" TO 2 1/2" ± .005 2 1/2" TO 2 3/4" ± .005 2 3/4" TO 3" ± .005 3" TO 3 1/4" ± .005 3 1/4" TO 3 1/2" ± .005 3 1/2" TO 3 3/4" ± .005 3 3/4" TO 4" ± .005 4" TO 4 1/4" ± .005 4 1/4" TO 4 1/2" ± .005 4 1/2" TO 4 3/4" ± .005 4 3/4" TO 5" ± .005 5" TO 5 1/4" ± .005 5 1/4" TO 5 1/2" ± .005 5 1/2" TO 5 3/4" ± .005 5 3/4" TO 6" ± .005 6" TO 6 1/4" ± .005 6 1/4" TO 6 1/2" ± .005 6 1/2" TO 6 3/4" ± .005 6 3/4" TO 7" ± .005 7" TO 7 1/4" ± .005 7 1/4" TO 7 1/2" ± .005 7 1/2" TO 7 3/4" ± .005 7 3/4" TO 8" ± .005 8" TO 8 1/4" ± .005 8 1/4" TO 8 1/2" ± .005 8 1/2" TO 8 3/4" ± .005 8 3/4" TO 9" ± .005 9" TO 9 1/4" ± .005 9 1/4" TO 9 1/2" ± .005 9 1/2" TO 9 3/4" ± .005 9 3/4" TO 10" ± .005 10" TO 10 1/4" ± .005 10 1/4" TO 10 1/2" ± .005 10 1/2" TO 10 3/4" ± .005 10 3/4" TO 11" ± .005 11" TO 11 1/4" ± .005 11 1/4" TO 11 1/2" ± .005 11 1/2" TO 11 3/4" ± .005 11 3/4" TO 12" ± .005 12" TO 12 1/4" ± .005 12 1/4" TO 12 1/2" ± .005 12 1/2" TO 12 3/4" ± .005 12 3/4" TO 13" ± .005 13" TO 13 1/4" ± .005 13 1/4" TO 13 1/2" ± .005 13 1/2" TO 13 3/4" ± .005 13 3/4" TO 14" ± .005 14" TO 14 1/4" ± .005 14 1/4" TO 14 1/2" ± .005 14 1/2" TO 14 3/4" ± .005 14 3/4" TO 15" ± .005 15" TO 15 1/4" ± .005 15 1/4" TO 15 1/2" ± .005 15 1/2" TO 15 3/4" ± .005 15 3/4" TO 16" ± .005 16" TO 16 1/4" ± .005 16 1/4" TO 16 1/2" ± .005 16 1/2" TO 16 3/4" ± .005 16 3/4" TO 17" ± .005 17" TO 17 1/4" ± .005 17 1/4" TO 17 1/2" ± .005 17 1/2" TO 17 3/4" ± .005 17 3/4" TO 18" ± .005 18" TO 18 1/4" ± .005 18 1/4" TO 18 1/2" ± .005 18 1/2" TO 18 3/4" ± .005 18 3/4" TO 19" ± .005 19" TO 19 1/4" ± .005 19 1/4" TO 19 1/2" ± .005 19 1/2" TO 19 3/4" ± .005 19 3/4" TO 20" ± .005 20" TO 20 1/4" ± .005 20 1/4" TO 20 1/2" ± .005 20 1/2" TO 20 3/4" ± .005 20 3/4" TO 21" ± .005 21" TO 21 1/4" ± .005 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## CUSTOMER CONNECT INFORMATION

This portion of the report contains information related to LV-2A propulsion system installation, weight distribution, instrumentation, electrical requirements, and general operating requirements and limitations.

### ALLOWABLE INSTALLATION MISALIGNMENTS

The coordinate system used by Rocketdyne for designating reference axes and their origins is given in Fig. 2. Data are intended for use in the orientation of the LV-2A propulsion system in the Thor missile boattail.

Table 2 lists the customer connect points, coordinates the expected flight deflections of each point, and the allowable installation misalignments of the LOX and fuel pump inlet bellows for the main engine. The recommended maximum installation misalignment is based upon an inlet bellows approximately 13.5 inches long with an axial spring rate of 600 lb/in. and a maximum lateral spring rate of 500 lb/in. The recommendations assume that:

1. The bellows spring rates will be verified by laboratory test.
2. No liners are present in the bellows unless tests prove that there is a possibility of the liners "bottoming" or "hanging up" when subjected to maximum deflections resulting from the sum of allowable installation misalignment and turbopump and missile deflections.

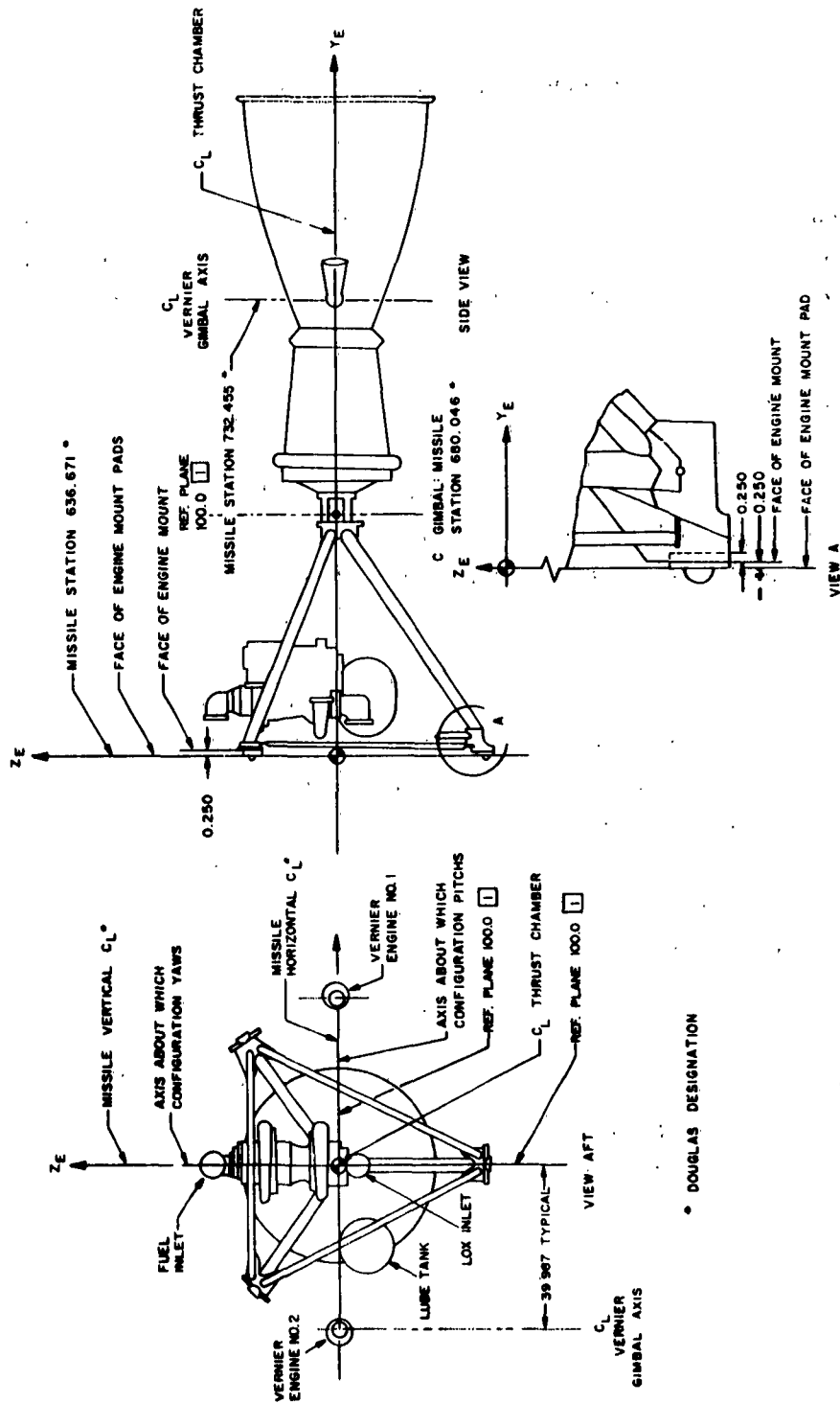


Figure 2. Coordinate System

# 1

TABLE 2

LV-2A PROPULSION  
DEFLECTIONS AND ALLOWABLE INST

Customer Connect Points	Coordinates, inches (Drawing No. 104654)			Approximate Flight Deflection	
	X	Y	Z	$\Delta X$	$\Delta Y$
Geometrical center of triangle formed by the three thrust missile attach points.	0.000	0.000	0.000		
Mount Attach to Missile	28.919	0.000	16.697	The three thrust mount-to-mis will deflect radially (outboa	
Mount Attach to Missile	-28.919	0.000	16.697		
Mount Attach to Missile	0.000	0.000	-33.393		
Turbopump, LOX Inlet Elbow	0.000 $\pm 0.187$	6.500 $\pm 0.132$	-7.776 $\pm 0.187$	$\pm 0.12$	+0.12 to -0.37
Turbopump, Fuel Inlet Elbow	0.000 $\pm 0.187$	5.250 $\pm 0.132$	23.963 $\pm 0.187$	$\pm 0.12$	+0.31 to -0.12
Forward Pitch Actuator Attach Point (Center of Bearing)	0.000 $\pm 0.12$	12.407 $\pm 0.12$	-28.703 $\pm 0.12$		
Aft Pitch Actuator Attach Point (Center of Bearing)	0.000 $\pm 0.37$	43.375 $\pm 0.37$	-24.000 $\pm 0.34$		
Forward Yaw Actuator Attach Point (Center of Bearing)	-24.000 $\pm 0.34$	43.375 $\pm 0.12$	0.000 $\pm 0.12$	Deflections of actuator attach	
Aft Yaw Actuator Attach Point (Center of Bearing)	-28.703 $\pm 0.12$	74.341 $\pm 0.12$	0.000 $\pm 0.12$		
Forward Attach Lug, Heat Exchanger	6.12 $\pm 0.12$	51.27 $\pm 0.12$	40.69 $\pm 0.12$	The three heat exchanger attac enclosed by these lugs must no closed by the three thrust att	
Forward Attach Lug, Heat Exchanger	6.12 $\pm 0.12$	51.27 $\pm 0.12$	40.69 $\pm 0.12$		
Aft Attach Lug, Heat Exchanger (Center of Slot)	0.00 $\pm 0.12$	66.25 $\pm 0.12$	41.32 $\pm 0.12$		

\*Refer to note 1 on drawing 104654. The total transverse misalignment shall not exceed C  
R-5214

TABLE 2

LV-2A PROPULSION SYSTEM

AND ALLOWABLE INSTALLATION MISALIGNMENTS

e Flight Deflections, inches		Allowable Installation Misalignment With Respect To Engine, inches					
$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$	$\theta X$	$\theta Y$	$\theta Z$
thrust mount-to-missile attach points are within 0.010 inch of true position. The attach points at radially (outboard) 0.044 $\pm$ 0.010 (NA-13) inch during flight.							
+0.12 to -0.37	+0.25 to -0.12	$\pm 0.50^*$	0.50 Tension or Compression	$\pm 0.50$	$\pm 3^*$	0	$\pm 3$
+0.31 to -0.12	+0.25 to -0.12	$\pm 0.50^*$	0.75 $\pm$ 0.50 Tension	$\pm 0.50$	$\pm 3^*$	0	$\pm 3$
of actuator attach points do not affect the missile structure,							
eat exchanger attach lugs are mated with the missile. The centroid of the triangular area these lugs must not deflect more than 0.37 inch relative to the centroid of the area en- the three thrust attach points.							

shall not exceed 0.50 inch.

2



1

TABLE 2  
(Continued)

Customer Connect Points	Coordinates, inches (Drawing No. 104654)			Approximate Flight Deflections, i		
	X	Y	Z	$\Delta X$	$\Delta Y$	$\Delta Z$
Oxygen Outlet, Heat Exchanger	-7.93 $\pm 0.12$	51.37 $\pm 0.12$	30.87 $\pm 0.12$	Deflects with missile		
Aft End Heat Exchanger	0.00 $\pm 0.12$	69.43 $\pm 0.12^*$	34.57 $\pm 0.12$	Deflects with missile		
LOX Supply to Vernier Engine	30.63 $\pm 0.12$	47.07 +0.34 -0.27	-2.48 +0.47 -0.49	$\pm 0.12$	+0.31 to -0.12	$\pm 0.$
Fuel Supply to Vernier Engines	28.15 +0.29 -0.31	40.85 +0.27 -0.28	-6.82 +0.33 -0.31	$\pm 0.12$	+0.25 to -0.12	$\pm 0.$
Main Oil Discharge	1.33 $\pm 0.12$	29.73 $\pm 0.12$	14.72 $\pm 0.12$	$\pm 0.12$	+0.19 to -0.12	$\pm 0.$
Fuel Start Tank Vent Valve Vent	20.19 $\pm 0.12$	12.53 $\pm 0.12$	-0.18 $\pm 0.12$	$\pm 0.12$	+0.25 to -0.12	$\pm 0.$
LOX Start Tank Vent Valve Vent	24.70 $\pm 0.12$	6.54 $\pm 0.12$	-14.06 $\pm 0.12$	$\pm 0.12$	+0.19 to -0.12	$\pm 0.1$
High-Pressure Gaseous Nitrogen Supply	8.65 $\pm 0.12$	11.35 $\pm 0.12$	-26.45 $\pm 0.12$	$\pm 0.12$	+0.19 to -0.12	$\pm 0.1$
Center Tachometer Mount Pad (No gasket)	-0.40 $\pm 0.12$	20.07 $\pm 0.12$	-3.76 $\pm 0.12$	$\pm 0.25$	+0.12 to -0.25	$\pm 0.2$
Center Hydraulic Pump Mount Pad (No gasket)	3.96 $\pm 0.12$	24.85 $\pm 0.12$	-1.26 $\pm 0.12$	$\pm 0.25$	+0.12 to -0.25	$\pm 0.2$
LOX Seal Drain	-2.00 $\pm 0.12$	30.17 $\pm 0.12$	15.98 $\pm 0.12$	$\pm 0.25$	+0.19 to -0.12	$\pm 0.3$
Oil Seal Drain	-3.50 $\pm 0.12$	29.90 $\pm 0.12$	15.87 $\pm 0.12$	$\pm 0.12$	+0.25 to -0.12	$\pm 0.3$
Pressure Takeoff from Pneumatic Manifold	15.08 $\pm 0.12$	7.40 $\pm 0.12$	-15.17 $\pm 0.12$	$\pm 0.12$	+0.19 to -0.12	$\pm 0.1$

\*Refer to note 7 on drawing 104654

**TABLE 2**  
**(Continued)**

Maximum Flight Deflections, inches		Allowable Installation Misalignment With Respect to Engine, inches					
$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$	$\theta X$	$\theta Y$	$\theta Z$
s with missile		<p>The customer connect points are to be connected with no load applied except that necessary to support its weight. The parts shall be designed and installed to provide for both maximum missile and maximum flight deflections.</p> <p><b>Turbine Exhaust System</b></p> <p>(a) The aft flange of the turbine exhaust duct assembly shall be parallel with the heat exchanger flange within four degrees.</p> <p>(b) The distance between the two flanges shall be <math>0.31 \pm 0.25</math> inch</p> <p>(c) The misalignment of the centerline of the two flanges shall not exceed 0.38 inch</p>					
s with missile							
+0.31 to -0.12	$\pm 0.12$						
+0.25 to -0.12	$\pm 0.12$						
+0.19 to -0.12	$\pm 0.37$						
+0.25 to -0.12	$\pm 0.12$						
+0.19 to -0.12	$\pm 0.12$						
+0.19 to -0.12	$\pm 0.12$						
+0.12 to -0.25	$\pm 0.25$						
+0.12 to -0.25	$\pm 0.25$						
+0.19 to -0.12	$\pm 0.37$						
+0.25 to -0.12	$\pm 0.37$						
+0.19 to -0.12	$\pm 0.12$						

**2**

TABLE  
(Continued)

Customer Connect Points	Coordinates, inches (Drawing No. 104654)			Approximate Flight Deflection		
	X	Y	Z	$\Delta X$	$\Delta Y$	
Electrical Ground Connection	17.25*	11.40	17.48	$\pm 0.19$	+0.25 to -0.12	
Missile Interconnection	17.25	14.05	17.55	$\pm 0.19$	+0.25 to -0.12	
Missile Power Connection	19.35*	13.25	17.55	$\pm 0.19$	+0.25 to -0.12	
Vernier LOX Vent Valve Control Solenoid Exit	14.33 $\pm 0.12$	21.18 $\pm 0.12$	-3.41 $\pm 0.12$	$\pm 0.12$	+0.19 to -0.12	
Vernier Engine Propellant Valve Control Solenoid Exit	15.92 $\pm 0.12$	23.31 $\pm 0.12$	-4.33 $\pm 0.12$	$\pm 0.12$	+0.19 to -0.12	
Lube Tank Vent and Overflow	-19.23 $\pm 0.12$	2.59 $\pm 0.12$	5.27 $\pm 0.12$	$\pm 0.06$		$\pm 0.06$
Lube Tank Horizontal Drain						

\*Refer to note 9 on drawing 104654

1

R-5214

TABLE 2  
(Continued)

ate Flight Deflections, inches		Allowable Installation Misalignment With Respect to Engine, inches					
$\Delta Y$	$\Delta Z$	$\Delta X$	$\Delta Y$	$\Delta Z$	$\theta X$	$\theta Y$	$\theta Z$
+0.25 to -0.12	$\pm 0.19$	These values are based on inlet bellows which have an axial inlet bellows with an axial spring rate of 600 lb/in. and a maximum transverse spring rate of 500 lb/in.					
+0.25 to -0.12	$\pm 0.19$						
+0.25 to -0.12	$\pm 0.19$						
+0.19 to -0.12	$\pm 0.12$						
+0.19 to -0.12	$\pm 0.12$						
$\pm 0.06$	$\pm 0.06$						



#### WEIGHT DISTRIBUTION AND FLUID VOLUMES

Weight, balance, inertia, and fluid volume information for the LV-2A propulsion system configurations is presented in Tables 3 and 4.

This data may be used in determining missile deadweight distribution, structural requirements, basic loads, stability, performance, and control requirements.

#### CUSTOMER CONNECT AND INSTRUMENTATION DRAWINGS

The locations of connections that are necessary for the operation of the LV-2A propulsion system in the missile are shown in Drawings 104654 and 350723. Locations shown include those for supply connections, drain and vent connections, and flush and purge connections. Structural attachments and accessory pad information are shown, as well as gimbal bearing alignment and lubrication points.

The instrumentation tap locations on the main vernier engines that are available for use appear in Drawings 702827 and 350050.

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TABLE 3

CENTER OF GRAVITY, MOMENT OF INERTIA, AND WEIGHTS  
FOR MAIN ENGINE (RJ-1 FUEL)

Propulsion system weights and centers of gravity\* (including vernier engines)

Condition	Weight, pounds	Y Arm, inches	X Arm, inches	Z Arm, inches
Dry	2116	100.2	100.4	103.3
Wet	2690	100.0	100.6	102.3
Burnout	2468	101.5	100.5	102.8

\*Reference point (gimbal bearing) is (100,100,100).

Moments of inertia of the propulsion system about axes through its center of gravity, wet and dry, with corresponding radii of gyration

Condition	Weight, pounds	Y Roll	X Pitch	Z Yaw
Dry	2116	167 slug sq ft 19.1 inches	616 slug sq ft 36.7 inches	626 slug sq ft 37.0 inches
Wet	2690	223 slug sq ft 19.6 inches	782 slug sq ft 36.7 inches	816 slug sq ft 37.5 inches

Moment of inertia of the gimballed mass about the gimbal axes (verniers not included)

Condition	Weight, pounds	Y Roll, slug sq ft	X Pitch, slug sq ft
Dry	828	32	311
Wet	1057	44	416

Longitudinal (Y axis) location of center of gravity of the gimballed mass in inches aft of the gimbal axis.

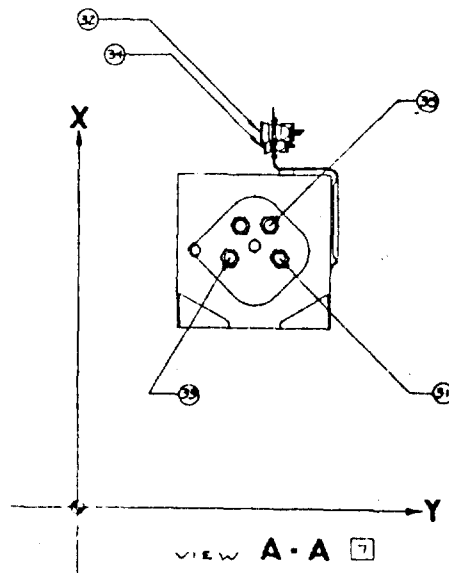
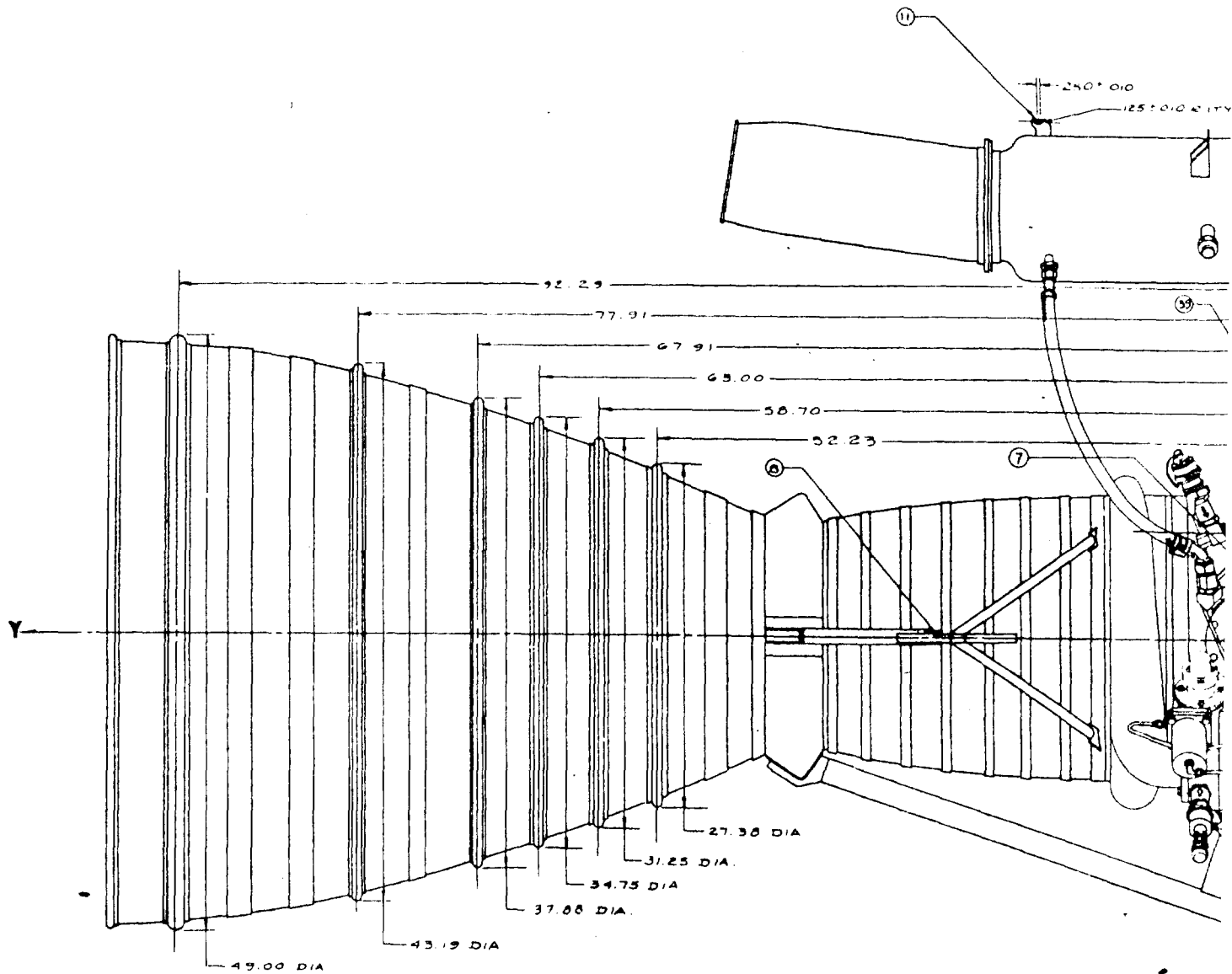
Dry = 29.0 inches  
Wet = 29.2 inches

**ROCKETDYNE**  
A DIVISION OF NORTH AMERICAN AVIATION, INC

TABLE 4

MAIN ENGINE FLUID VOLUME DATA

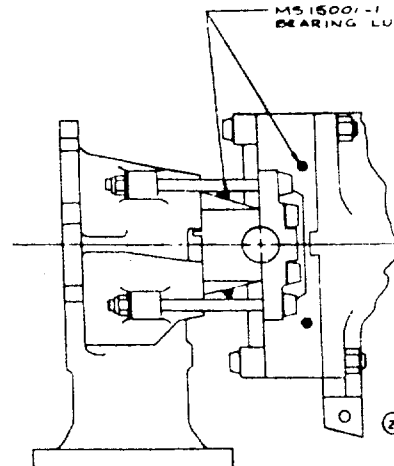
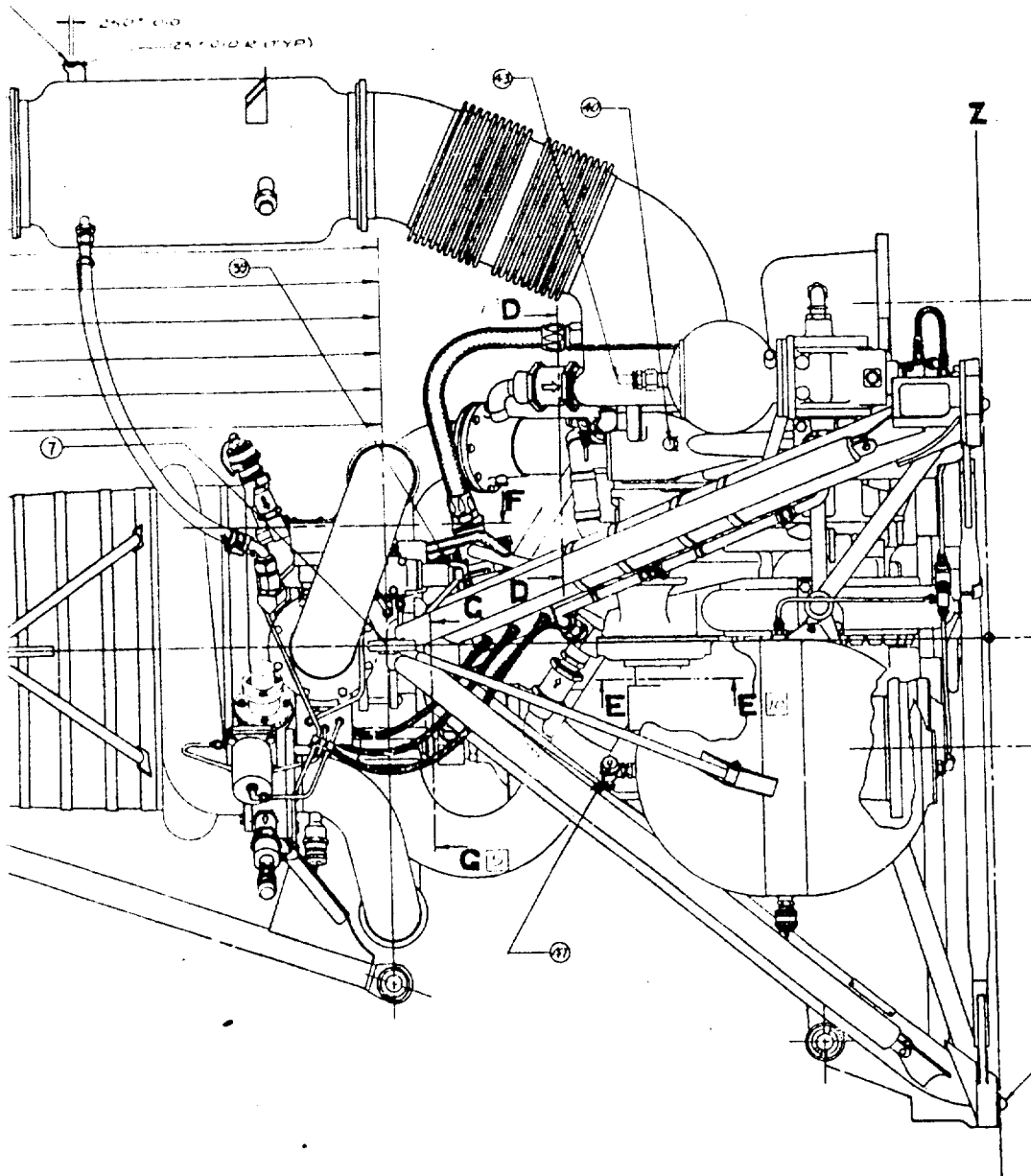
Component	Fuel Volume, cu in.	Liquid Oxygen Volume, cu in.	Oil Volume, cu in.
Thrust Chamber	3987	935	3927
Main Ducts	1111	1614	
Turbopump	950	945	
Lubrication System			
Start System	1319	1454	
Vernier Engines (2)	106	46	
Miscellaneous Units	120	183	



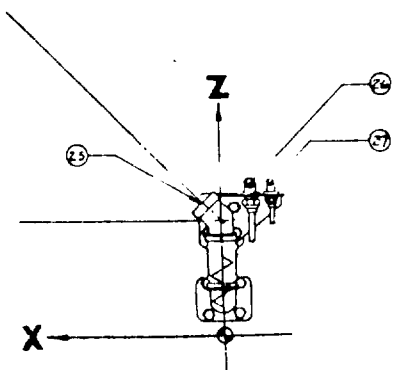
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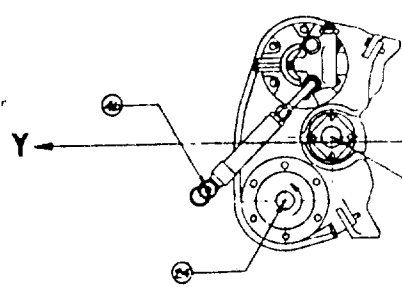


VIEW F-F  
SCALE 1/2



VIEW D-D

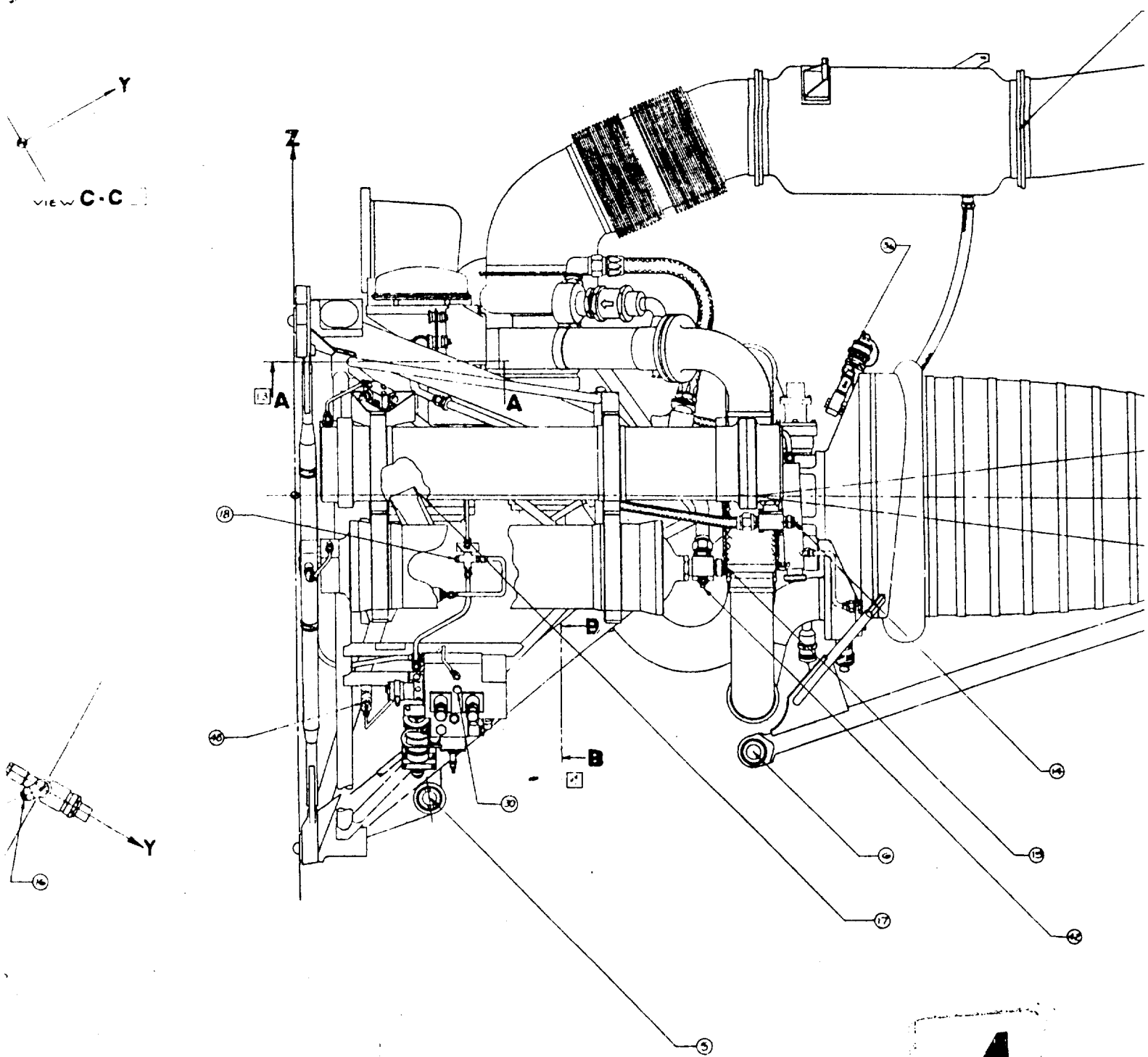
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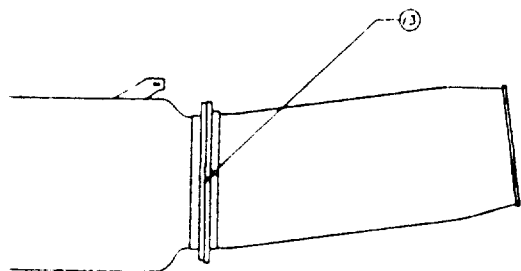
VIEW E-E



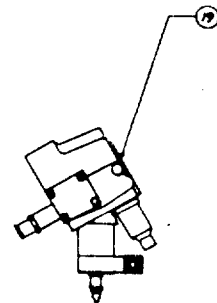
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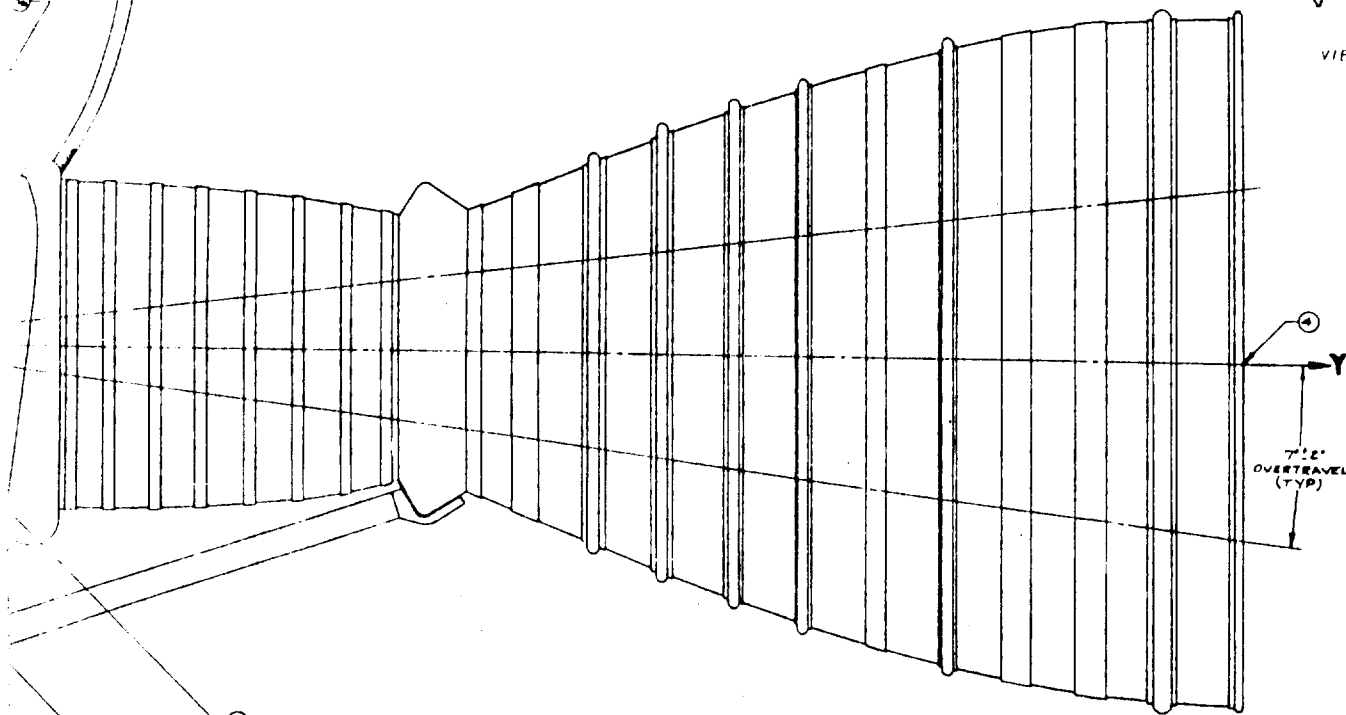
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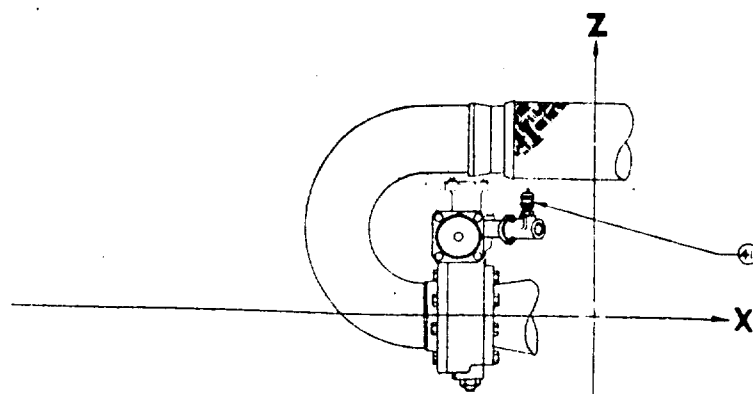
X ——— Z



VIEW B-B 17




NO.	OF	REASON	X
1	(1)	0	-0.00
2	(1)	10	-0.00
3	(1)	9	0.00
4	(1)	4	0.00
5	(1)	6	0.00
6	(1)	6	0.00
7	(1)	12	-0.00
8	(1)	14	-0.00
9	(1)	8	-0.00
10	(1)	10	-0.00
11	(1)	12	-0.00
12	(1)	5	-0.00
13	(1)	6	0.00
14	(1)	6	-0.00
15	(1)	6	-0.00
16	(1)	6	-0.00
17	(1)	6	-0.00
18	(1)	6	-0.00
19	(1)	6	-0.00
20	(1)	6	-0.00
21	(1)	6	-0.00
22	(1)	6	-0.00
23	(1)	10	-0.00
24	(1)	10	-0.00
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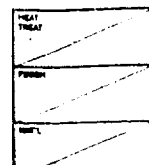


VIEW C-C 12

5

NO	Q	P	R	DISTANCES FROM ORIGIN			DESCRIPTION	END OF CONNECTION
				X	Y	Z		
1	0	0	0	0.000	0.000	0.000	MOUNT ATTACH TO MISSILE	
2	1	0	0	0.000	0.000	0.000	MOUNT ATTACH TO MISSILE	
3	2	0	0	0.000	0.000	0.000	MOUNT ATTACH TO MISSILE	
4	3	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
5	4	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
6	5	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
7	6	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
8	7	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
9	8	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
10	9	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
11	10	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
12	11	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
13	12	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
14	13	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
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35	34	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
36	35	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
37	36	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
38	37	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
39	38	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
40	39	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02
41	40	0	0	0.000	0.000	0.000	END OF THRUST CHAMBER	40.02E.02

8 12 THE BRUNING CO, LINCOLN, NEBRASKA  
 11 13 THESE DIMS NOT TO BE FELD TO 1% TOLERANCE  
 14 14 BEND AVIATION CORP SCHULDA DN, SHELBY  
 17 15 CHANGE OF DIM WITH FULL TANK - .20 (MAX)  
 20 16 SYMBOL  DENOTES ORIGIN OF REFERENCE  
 23 17 SYSTEM POSITIVE DIRECTIONS FROM ORIGIN ARE  
 26 18 INDICATED BY ARROWHEADS ON AXES  
 29 19 FOR ALIGNMENT TOLERANCES REFER TO 9578 94000+  
 32 20 TOLERANCES 1/2 FOR DIMENSIONED CUSTOMER CONNECTIONS  
 35 21 REFLECTION ON R/R 79-1M31 ENGINES  
 38 22 E.D. WIGGINS LTD TORO, CO,  
 41 23 LOS ANGELES 23, CALIF  
 44 24 SOUTHWEST PRODUCTS CO, DUARTE, CALIF  
 47 25 SERVICE CONNECTION  
 50 26 CUSTOMER CONNECTION TO MISSILE



DATE		TIME		DESCRIPTION		DATE	APPROVED
				1 MAY BE REBOOKED	2 RECORDING CHARGE		
				3 CANNOT BE REBOOKED	4 NOW SHOP PRACTICE		
				5 PARTS MADE ON			

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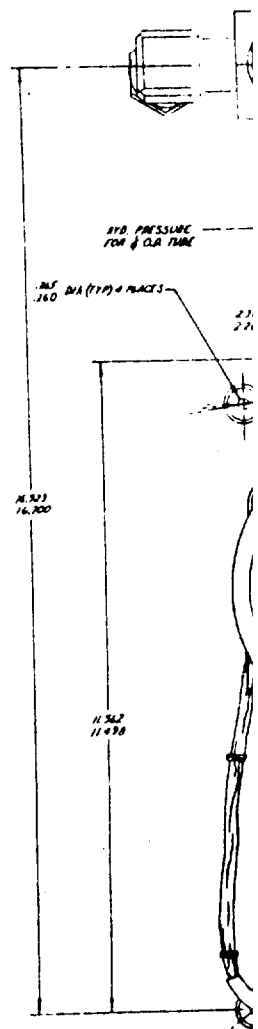
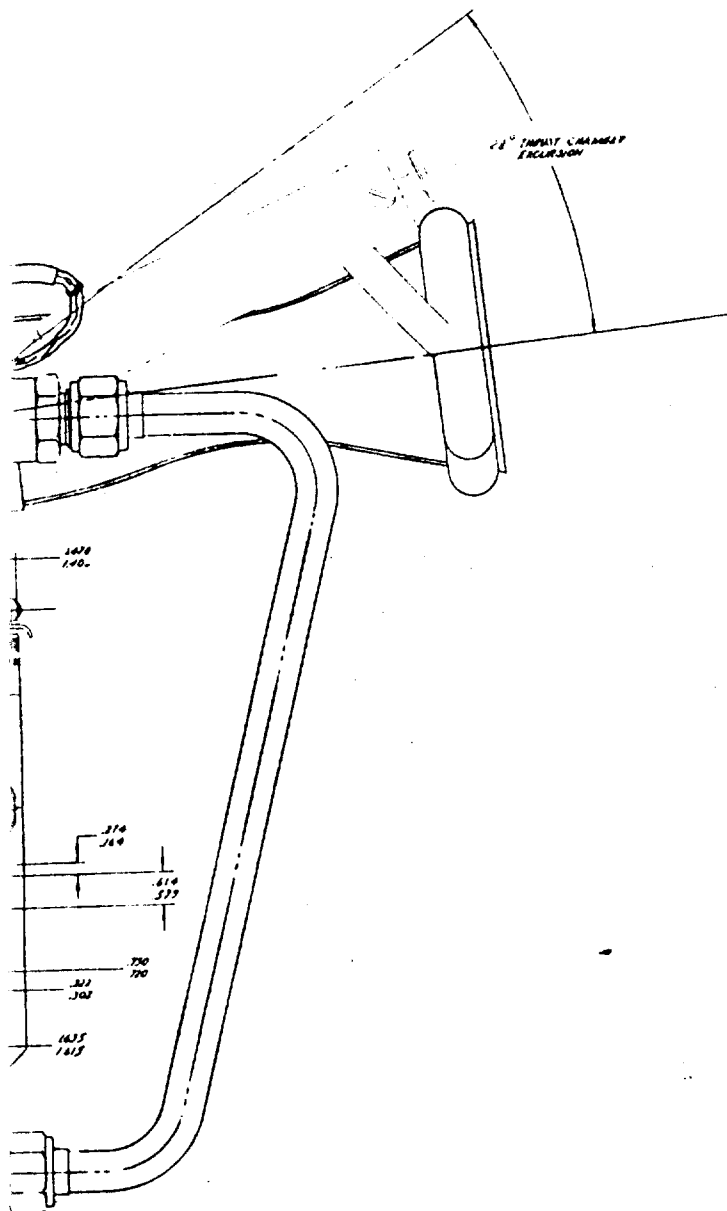
12 THE BRUNING CO, LINCOLN, NEBRASKA  
11 THERE DIMS NOT TO BE HELD TO :12 TOLERANCE  
10 BENDIX AVIATION CORP SCITILLA DV, SIDNEY, N.Y  
9 CHANGE OF DIM. WITH FULL TANK - .20 (MAX)  
8 SYMBOL \* DENOTES ORIGIN OF REFERENCE  
7 SYSTEM. POSITIVE DIRECTIONS FROM ORIGIN ARE  
6 INDICATED BY ARROWHEADS ON AXES  
5 FOR ALIGNMENT TOLERANCES REFER TO 937E 94000+  
4 TOLERANCES : 1E FOR UNKNOWN CUSTOMER CONNECTIONS  
3 EFFECTIVE ON KR 79-1A-13 ENGINES  
2 EB WIGGINS OIL TOOL CO.  
1 LOS ANGELES 23, CALIF  
9 SOUTHWEST PRODUCTS CO., DUARTE, CALIF  
8 SERVICE CONNECTION  
7 CUSTOMER CONNECTION TO MISSILE  
6  
5  
4  
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REFERENCE ONLY

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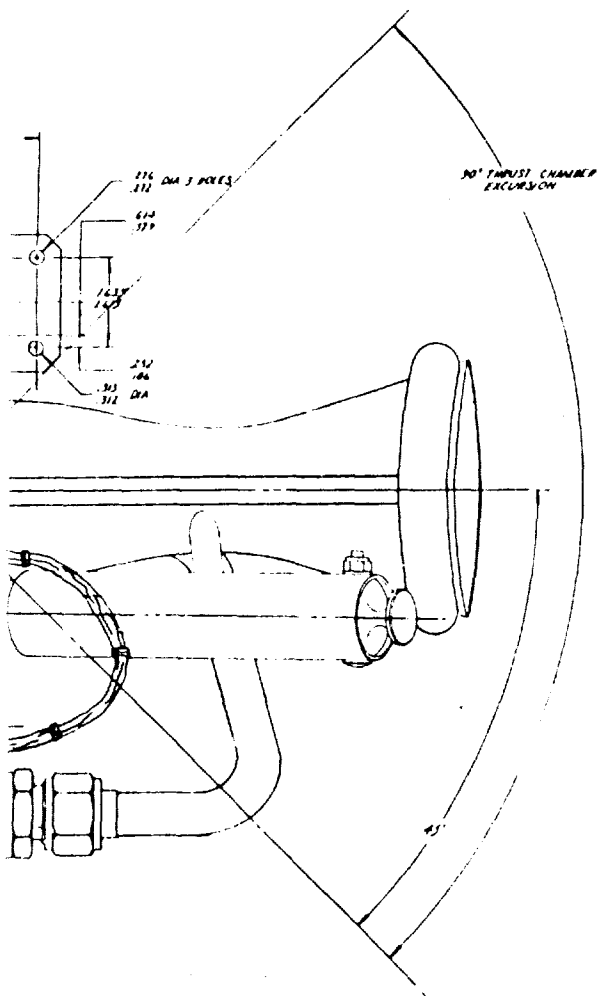


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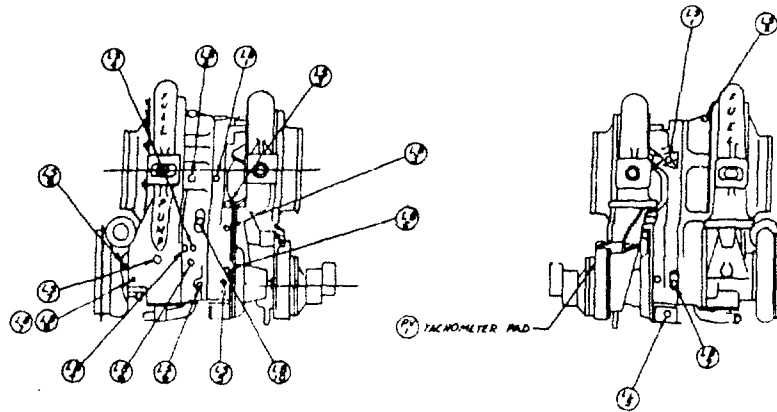


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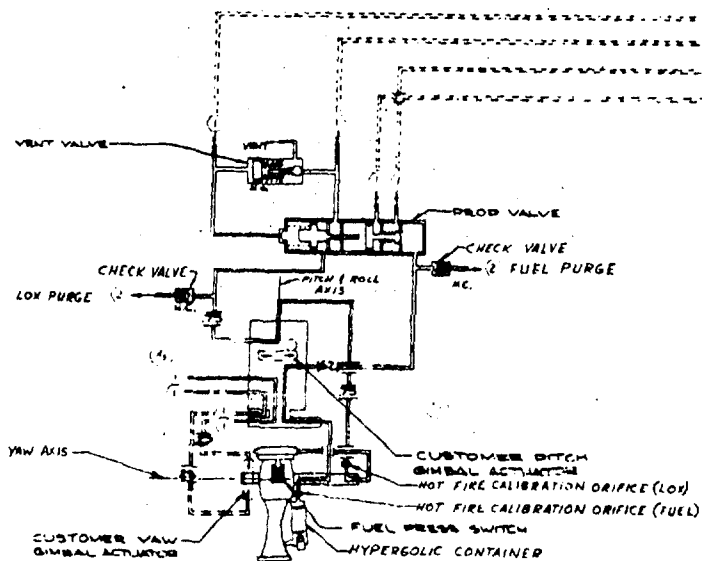
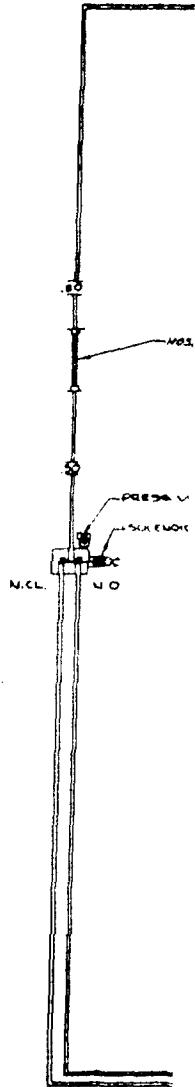
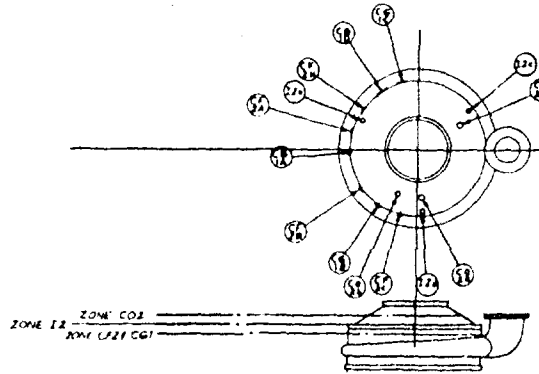
1. FOR CUSTOMER CONNECTIONS ON 3LR-10-MA-11.  
NOTE: UNLESS OTHERWISE SPECIFIED

DRILLING HOLES
1/8" TO 1/4" DIA.
1/4" TO 3/8" DIA.
3/8" TO 1/2" DIA.
1/2" TO 3/4" DIA.
3/4" TO 1" DIA.
1" TO 1 1/2" DIA.

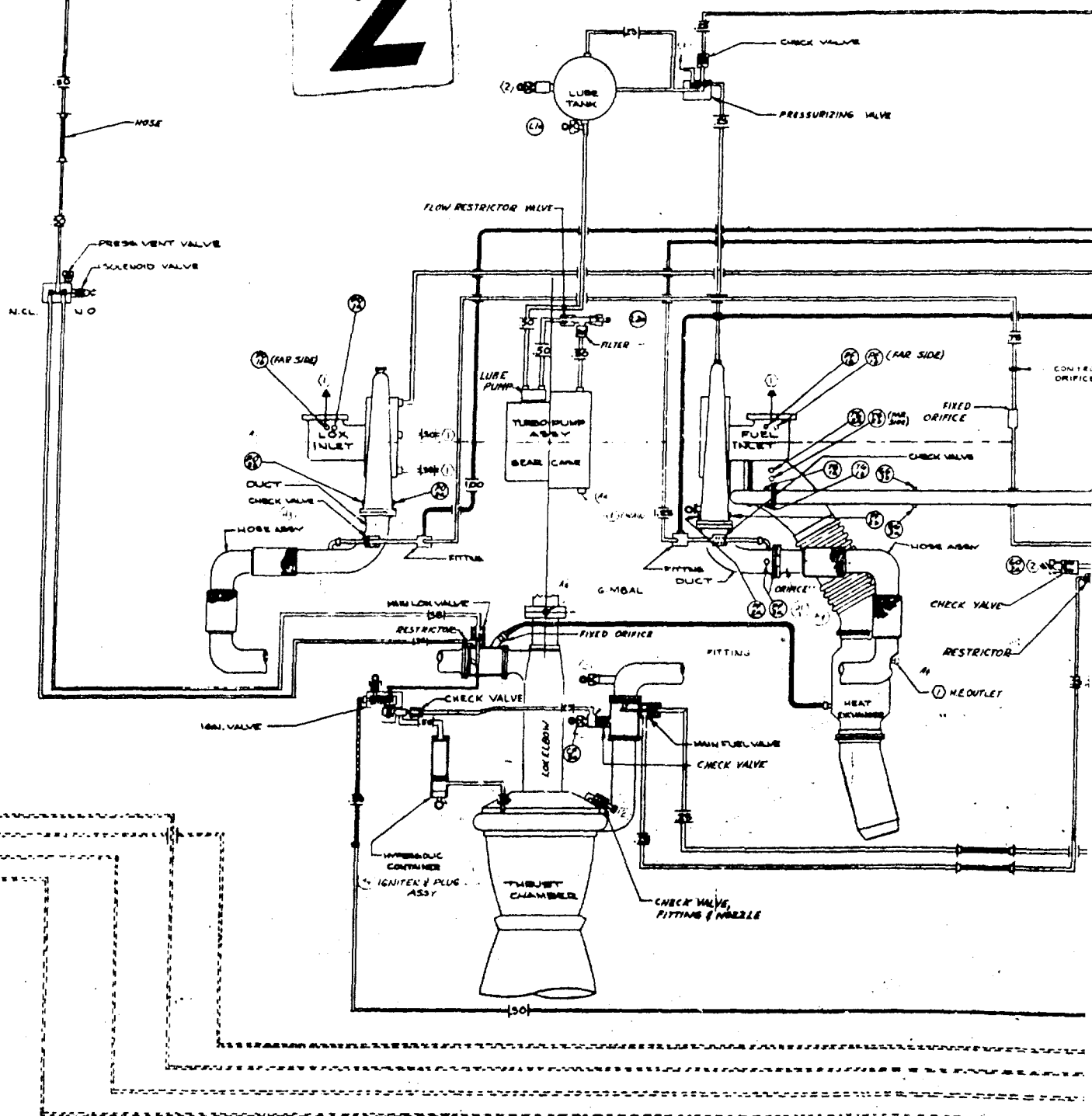




TURBOPUMP TAP POINT LOCATIONS



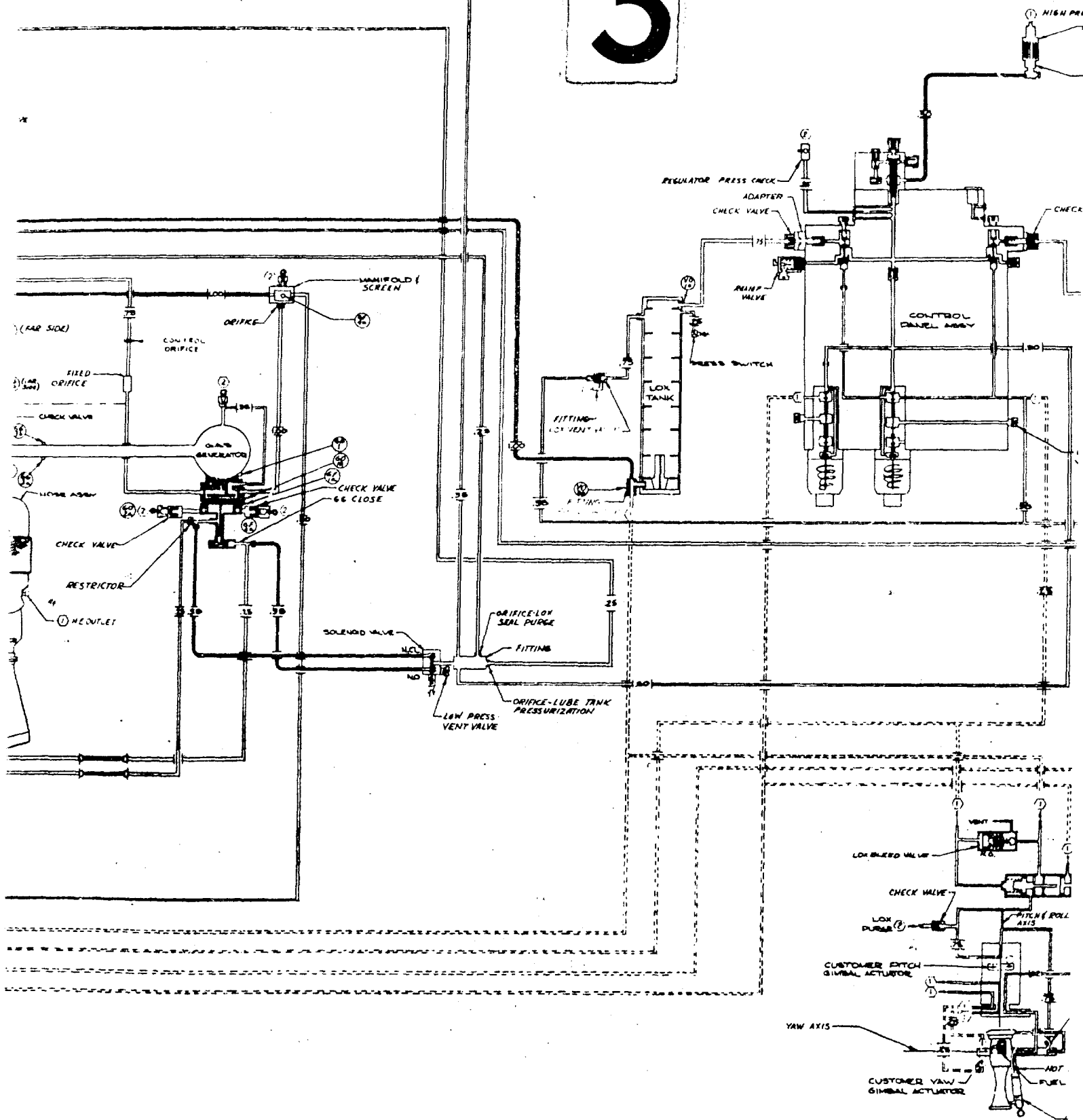
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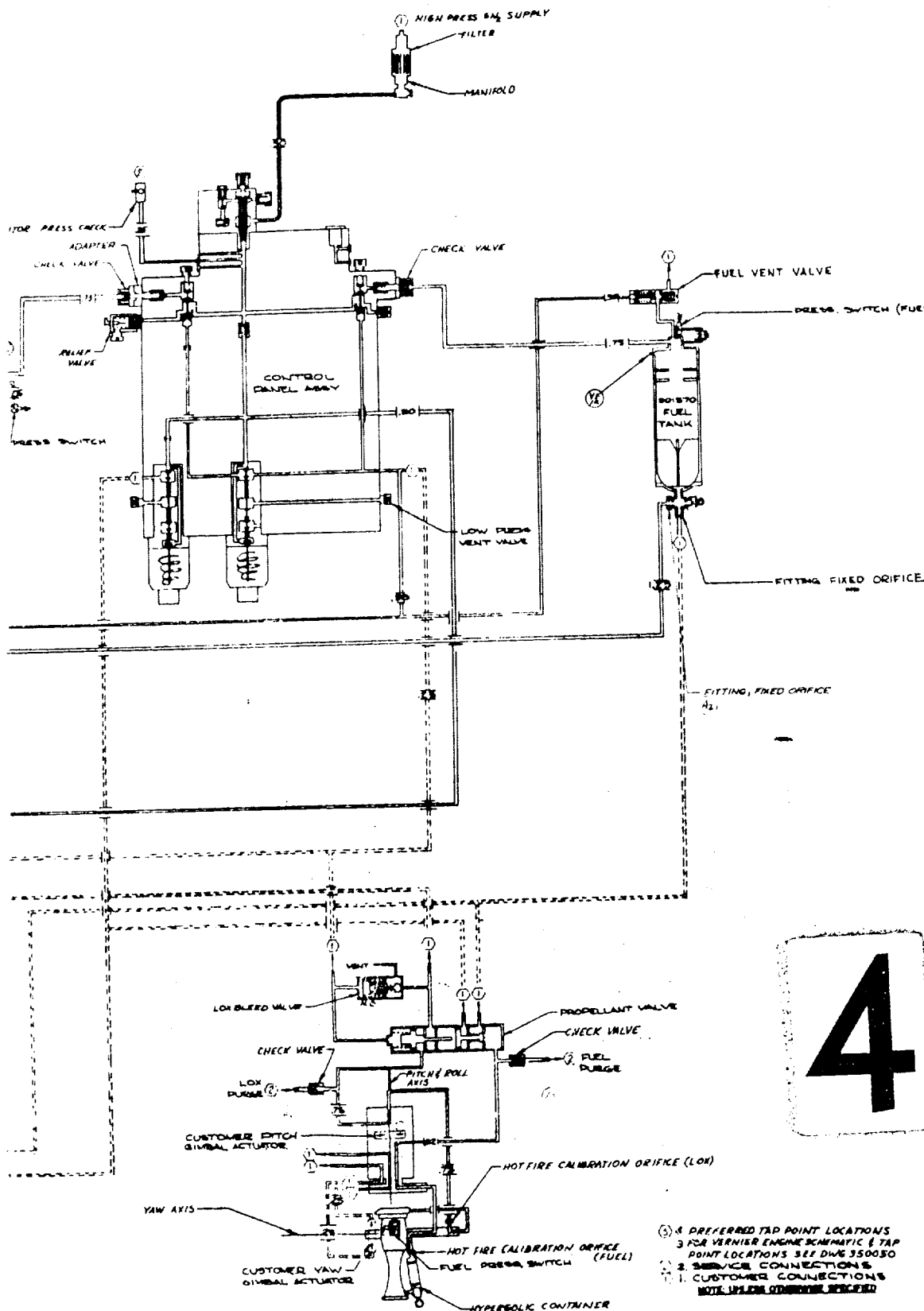


'URGE

ION ORIFICE (LOX)  
ION ORIFICE (FUEL)

3





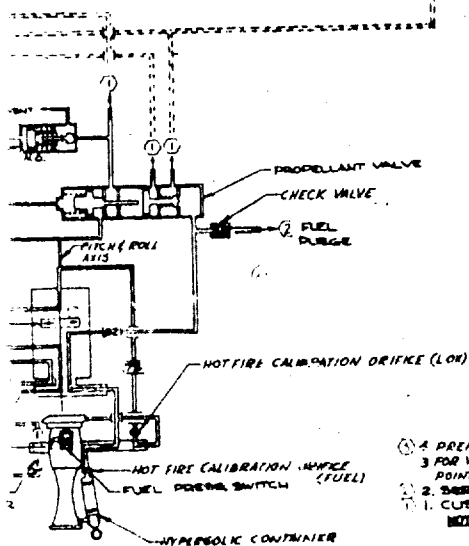
APPROX	TAP LOCATION
1	TC FUEL INLET MANIFOLD
2	TC FUEL INJECTION
3	TC FUEL INJECTION
4	TC FUEL INJECTION
5	TC FUEL INJECTION
6	TC FUEL INJECTION
7	TC FUEL INJECTION
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97	TC FUEL INJECTION
98	TC FUEL INJECTION
99	TC FUEL INJECTION
100	TC FUEL INJECTION

4

1. PREFERRED TAP POINT LOCATIONS  
2. SERVICE CONNECTIONS  
3. CUSTOMER CONNECTIONS  
NOTE: UPON CUSTOMER SPECIFICATION

ITEM	DESCRIPTION	QUANTITY	UNIT
1	1/2" NPT FUEL INLET	1	PC
2	1/2" NPT FUEL INLET	1	PC
3	1/2" NPT FUEL INLET	1	PC
4	1/2" NPT FUEL INLET	1	PC
5	1/2" NPT FUEL INLET	1	PC
6	1/2" NPT FUEL INLET	1	PC
7	1/2" NPT FUEL INLET	1	PC
8	1/2" NPT FUEL INLET	1	PC
9	1/2" NPT FUEL INLET	1	PC
10	1/2" NPT FUEL INLET	1	PC
11	1/2" NPT FUEL INLET	1	PC
12	1/2" NPT FUEL INLET	1	PC
13	1/2" NPT FUEL INLET	1	PC
14	1/2" NPT FUEL INLET	1	PC
15	1/2" NPT FUEL INLET	1	PC
16	1/2" NPT FUEL INLET	1	PC
17	1/2" NPT FUEL INLET	1	PC
18	1/2" NPT FUEL INLET	1	PC
19	1/2" NPT FUEL INLET	1	PC
20	1/2" NPT FUEL INLET	1	PC
21	1/2" NPT FUEL INLET	1	PC
22	1/2" NPT FUEL INLET	1	PC
23	1/2" NPT FUEL INLET	1	PC
24	1/2" NPT FUEL INLET	1	PC
25	1/2" NPT FUEL INLET	1	PC
26	1/2" NPT FUEL INLET	1	PC
27	1/2" NPT FUEL INLET	1	PC
28	1/2" NPT FUEL INLET	1	PC
29	1/2" NPT FUEL INLET	1	PC
30	1/2" NPT FUEL INLET	1	PC
31	1/2" NPT FUEL INLET	1	PC
32	1/2" NPT FUEL INLET	1	PC
33	1/2" NPT FUEL INLET	1	PC
34	1/2" NPT FUEL INLET	1	PC
35	1/2" NPT FUEL INLET	1	PC
36	1/2" NPT FUEL INLET	1	PC
37	1/2" NPT FUEL INLET	1	PC
38	1/2" NPT FUEL INLET	1	PC
39	1/2" NPT FUEL INLET	1	PC
40	1/2" NPT FUEL INLET	1	PC
41	1/2" NPT FUEL INLET	1	PC
42	1/2" NPT FUEL INLET	1	PC
43	1/2" NPT FUEL INLET	1	PC
44	1/2" NPT FUEL INLET	1	PC
45	1/2" NPT FUEL INLET	1	PC
46	1/2" NPT FUEL INLET	1	PC
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51	1/2" NPT FUEL INLET	1	PC
52	1/2" NPT FUEL INLET	1	PC
53	1/2" NPT FUEL INLET	1	PC
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61	1/2" NPT FUEL INLET	1	PC
62	1/2" NPT FUEL INLET	1	PC
63	1/2" NPT FUEL INLET	1	PC
64	1/2" NPT FUEL INLET	1	PC
65	1/2" NPT FUEL INLET	1	PC
66	1/2" NPT FUEL INLET	1	PC
67	1/2" NPT FUEL INLET	1	PC
68	1/2" NPT FUEL INLET	1	PC
69	1/2" NPT FUEL INLET	1	PC
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71	1/2" NPT FUEL INLET	1	PC
72	1/2" NPT FUEL INLET	1	PC
73	1/2" NPT FUEL INLET	1	PC
74	1/2" NPT FUEL INLET	1	PC
75	1/2" NPT FUEL INLET	1	PC
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82	1/2" NPT FUEL INLET	1	PC
83	1/2" NPT FUEL INLET	1	PC
84	1/2" NPT FUEL INLET	1	PC
85	1/2" NPT FUEL INLET	1	PC
86	1/2" NPT FUEL INLET	1	PC
87	1/2" NPT FUEL INLET	1	PC
88	1/2" NPT FUEL INLET	1	PC
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90	1/2" NPT FUEL INLET	1	PC
91	1/2" NPT FUEL INLET	1	PC
92	1/2" NPT FUEL INLET	1	PC
93	1/2" NPT FUEL INLET	1	PC
94	1/2" NPT FUEL INLET	1	PC
95	1/2" NPT FUEL INLET	1	PC
96	1/2" NPT FUEL INLET	1	PC
97	1/2" NPT FUEL INLET	1	PC
98	1/2" NPT FUEL INLET	1	PC
99	1/2" NPT FUEL INLET	1	PC
100	1/2" NPT FUEL INLET	1	PC



[illegible]

5

4. PREFERRED TAP POINT LOCATIONS  
3. FOR VERNIER ENGINE SCHEMATIC & TAP  
POINT LOCATIONS SEE DWG 350050  
2. SERVICE CONNECTIONS  
1. CUSTOMER CONNECTIONS  
NOTE: USE FOR OTHERS AS SPECIFIED

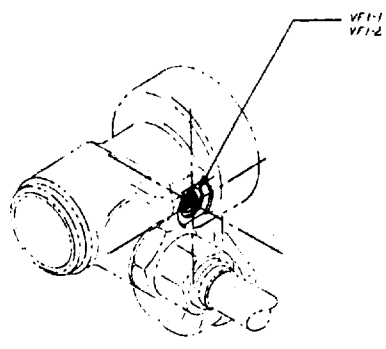
HEAT TREAT	UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES AND APPLY PRIOR TO FINISH	BY	DATE	SCHEMATIC INSTRUMENTATION \$TAP POINT LOCATION	A DIVISION OF NORTH AMERICAN AIRMAIL, INC. CANADA, PAID, CALIFORNIA
		ONE BY			
FINISH	1. ALL DIMENSIONS SHALL BE TOLERANCES (INCHES) (MM) .001 - .005 (0.025 - 0.127) .005 - .010 (0.127 - 0.254) .010 - .015 (0.254 - 0.381) .015 - .020 (0.381 - 0.508) .020 - .030 (0.508 - 0.762) .030 - .040 (0.762 - 1.016) .040 - .050 (1.016 - 1.270) .050 - .060 (1.270 - 1.524) .060 - .070 (1.524 - 1.778) .070 - .080 (1.778 - 2.032) .080 - .090 (2.032 - 2.286) .090 - .100 (2.286 - 2.540) .100 - .125 (2.540 - 3.175) .125 - .150 (3.175 - 3.810) .150 - .175 (3.810 - 4.445) .175 - .200 (4.445 - 5.080) .200 - .250 (5.080 - 6.350) .250 - .300 (6.350 - 7.620) .300 - .350 (7.620 - 8.890) .350 - .400 (8.890 - 10.160) .400 - .450 (10.160 - 11.430) .450 - .500 (11.430 - 12.700) .500 - .550 (12.700 - 13.970) .550 - .600 (13.970 - 15.240) .600 - .650 (15.240 - 16.510) .650 - .700 (16.510 - 17.780) .700 - .750 (17.780 - 19.050) .750 - .800 (19.050 - 20.320) .800 - .850 (20.320 - 21.590) .850 - .900 (21.590 - 22.860) .900 - .950 (22.860 - 24.130) .950 - 1.000 (24.130 - 25.400) 1.000 - 1.250 (25.400 - 31.750) 1.250 - 1.500 (31.750 - 38.100) 1.500 - 1.750 (38.100 - 44.450) 1.750 - 2.000 (44.450 - 50.800) 2.000 - 2.250 (50.800 - 57.150) 2.250 - 2.500 (57.150 - 63.500) 2.500 - 2.750 (63.500 - 69.850) 2.750 - 3.000 (69.850 - 76.200) 3.000 - 3.250 (76.200 - 82.550) 3.250 - 3.500 (82.550 - 88.900) 3.500 - 3.750 (88.900 - 95.250) 3.750 - 4.000 (95.250 - 101.600) 4.000 - 4.250 (101.600 - 107.950) 4.250 - 4.500 (107.950 - 114.300) 4.500 - 4.750 (114.300 - 120.650) 4.750 - 5.000 (120.650 - 127.000) 5.000 - 5.250 (127.000 - 133.350) 5.250 - 5.500 (133.350 - 139.700) 5.500 - 5.750 (139.700 - 146.050) 5.750 - 6.000 (146.050 - 152.400) 6.000 - 6.250 (152.400 - 158.750) 6.250 - 6.500 (158.750 - 165.100) 6.500 - 6.750 (165.100 - 171.450) 6.750 - 7.000 (171.450 - 177.800) 7.000 - 7.250 (177.800 - 184.150) 7.250 - 7.500 (184.150 - 190.500) 7.500 - 7.750 (190.500 - 196.850) 7.750 - 8.000 (196.850 - 203.200) 8.000 - 8.250 (203.200 - 209.550) 8.250 - 8.500 (209.550 - 215.900) 8.500 - 8.750 (215.900 - 222.250) 8.750 - 9.000 (222.250 - 228.600) 9.000 - 9.250 (228.600 - 234.950) 9.250 - 9.500 (234.950 - 241.300) 9.500 - 9.750 (241.300 - 247.650) 9.750 - 10.000 (247.650 - 254.000) 10.000 - 10.250 (254.000 - 260.350) 10.250 - 10.500 (260.350 - 266.700) 10.500 - 10.750 (266.700 - 273.050) 10.750 - 11.000 (273.050 - 279.400) 11.000 - 11.250 (279.400 - 285.750) 11.250 - 11.500 (285.750 - 292.100) 11.500 - 11.750 (292.100 - 298.450) 11.750 - 12.000 (298.450 - 304.800) 12.000 - 12.250 (304.800 - 311.150) 12.250 - 12.500 (311.150 - 317.500) 12.500 - 12.750 (317.500 - 323.850) 12.750 - 13.000 (323.850 - 330.200) 13.000 - 13.250 (330.200 - 336.550) 13.250 - 13.500 (336.550 - 342.900) 13.500 - 13.750 (342.900 - 349.250) 13.750 - 14.000 (349.250 - 355.600) 14.000 - 14.250 (355.600 - 361.950) 14.250 - 14.500 (361.950 - 368.300) 14.500 - 14.750 (368.300 - 374.650) 14.750 - 15.000 (374.650 - 381.000) 15.000 - 15.250 (381.000 - 387.350) 15.250 - 15.500 (387.350 - 393.700) 15.500 - 15.750 (393.700 - 400.050) 15.750 - 16.000 (400.050 - 406.400) 16.000 - 16.250 (406.400 - 412.750) 16.250 - 16.500 (412.750 - 419.100) 16.500 - 16.750 (419.100 - 425.450) 16.750 - 17.000 (425.450 - 431.800) 17.000 - 17.250 (431.800 - 438.150) 17.250 - 17.500 (438.150 - 444.500) 17.500 - 17.750 (444.500 - 450.850) 17.750 - 18.000 (450.850 - 457.200) 18.000 - 18.250 (457.200 - 463.550) 18.250 - 18.500 (463.550 - 469.900) 18.500 - 18.750 (469.900 - 476.250) 18.750 - 19.000 (476.250 - 482.600) 19.000 - 19.250 (482.600 - 488.950) 19.250 - 19.500 (488.950 - 495.300) 19.500 - 19.750 (495.300 - 501.650) 19.750 - 20.000 (501.650 - 508.000) 20.000 - 20.250 (508.000 - 514.350) 20.250 - 20.500 (514.350 - 520.700) 20.500 - 20.750 (520.700 - 527.050) 20.750 - 21.000 (527.050 - 533.400) 21.000 - 21.250 (533.400 - 539.750) 21.250 - 21.500 (539.750 - 546.100) 21.500 - 21.750 (546.100 - 552.450) 21.750 - 22.000				

1

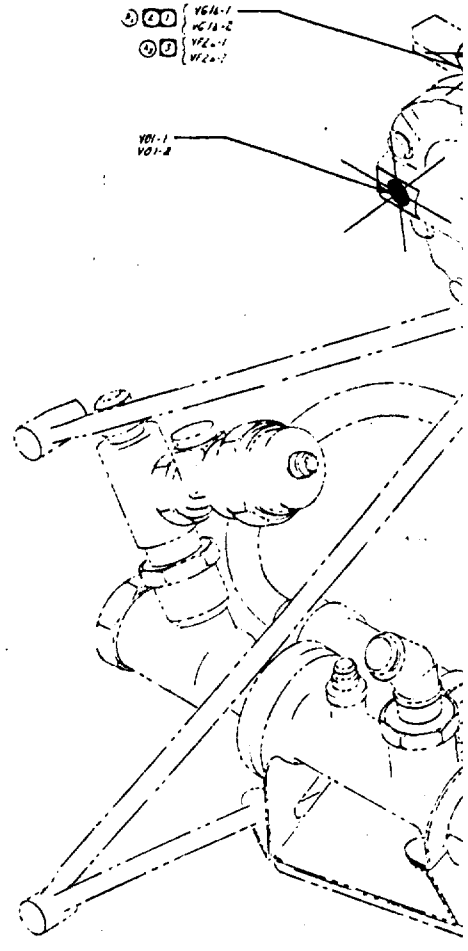
②  
②

② ② VGH-1  
② ② VGH-2  
② ② VGL-1  
② ② VGL-2

VGI-1  
VGI-2



VIEW **A** 4



2







**ROCKETDYNE**  
A DIVISION OF NORTH AMERICAN AVIATION, INC.

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**ELECTRICAL SYSTEM**

Twenty-five to 30 volts dc (to the main engine electrical relay box) will be maintained until 0.5 second after all starting sequences have been completed, and 20 to 30 volts dc thereafter. The power required is 800 watts maximum for starting, and 300 watts is required for flight operation. The command cutoff signal shall have a minimum current capacity of 0.30 ampere and shall be sustained for a minimum of 0.10 second. Electrical supply for the heaters during preflight is 115 volts ac at 60 to 400 cps. The maximum ground power supply shall be 3000 watts.

Nominal power requirement profile charts are presented in Fig. 3, 4, and 5. Drawing 900100 is the electrical system schematic for the LV-2A propulsion system.

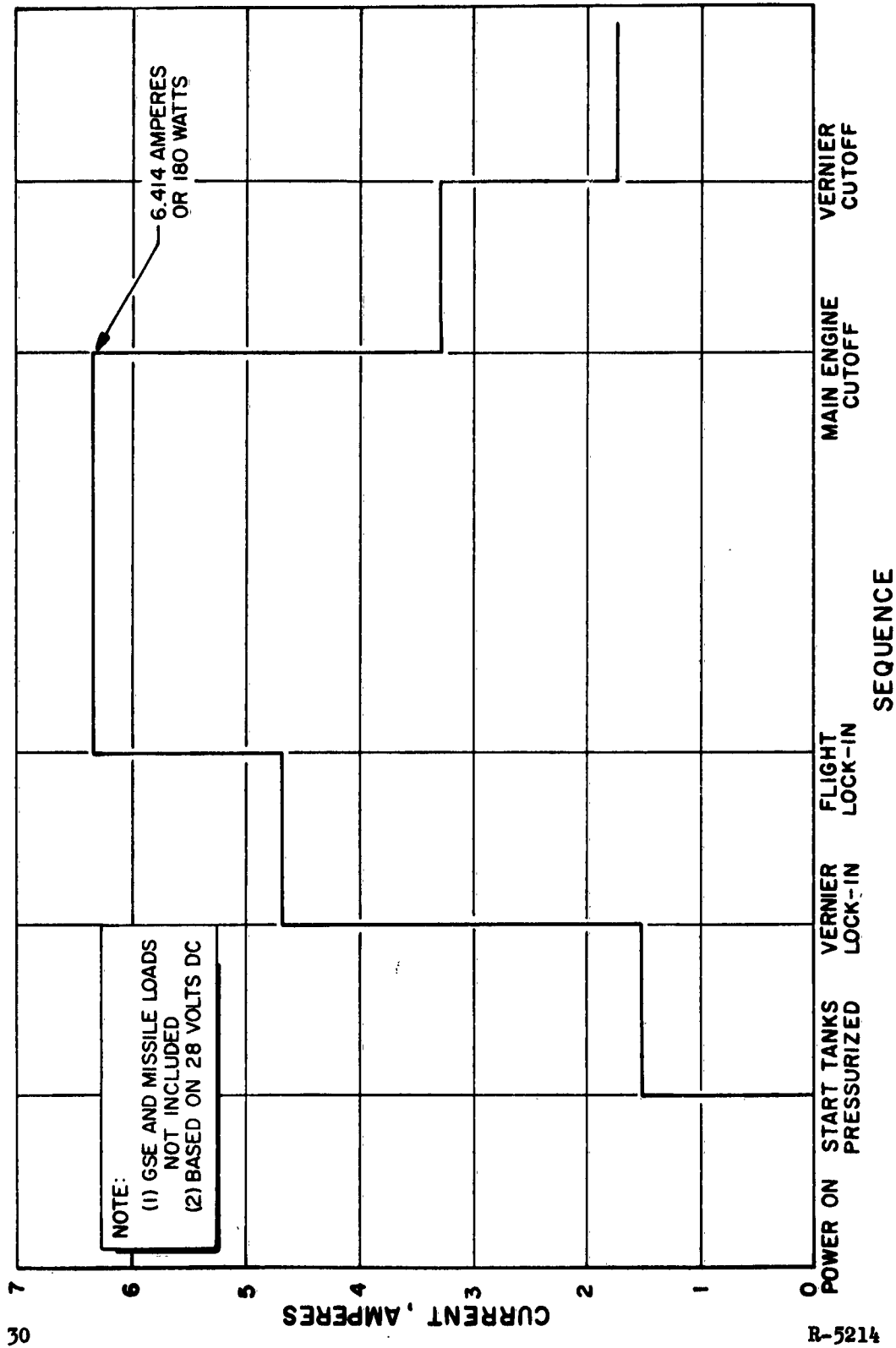


Figure 3 . Direct Current Requirements



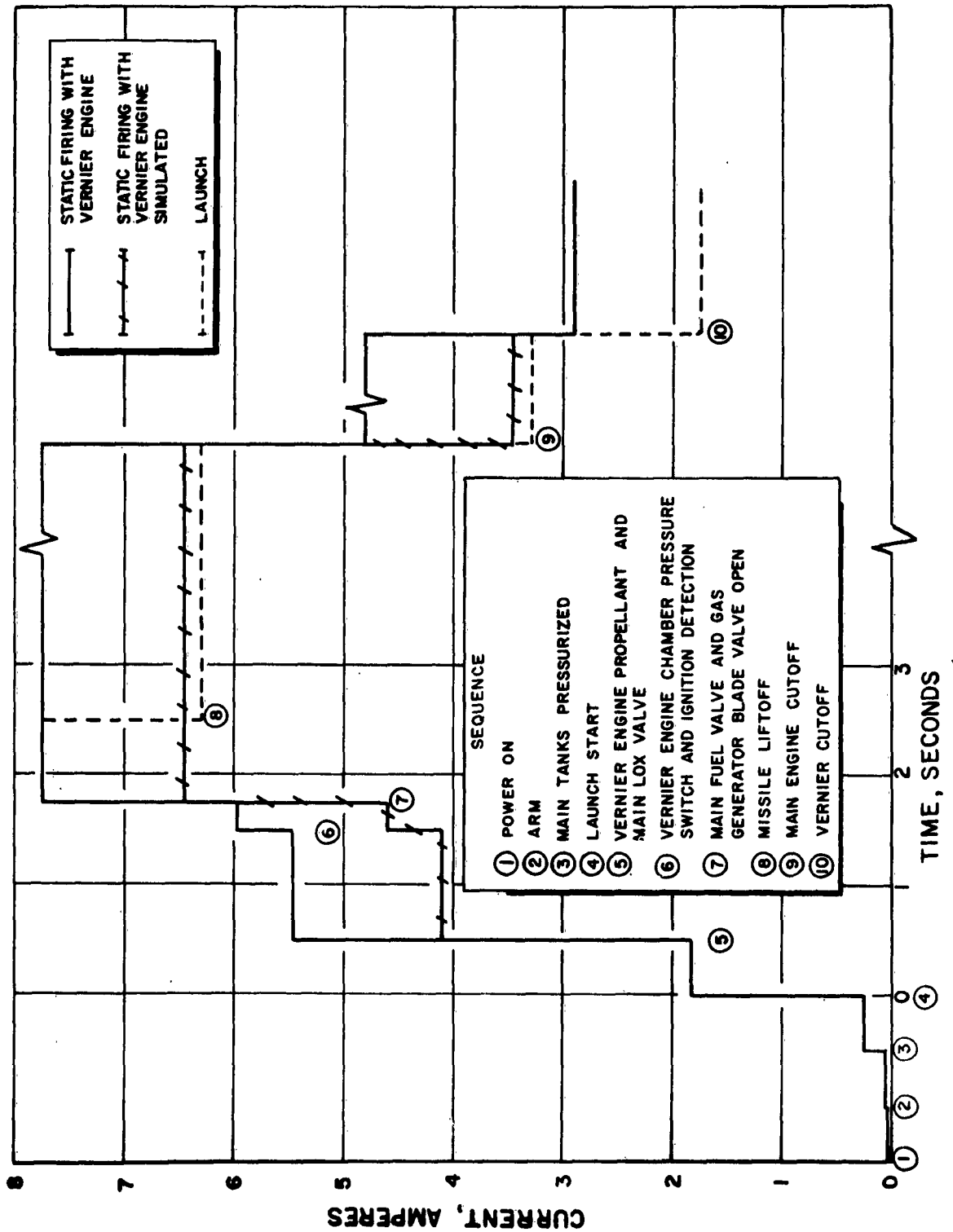
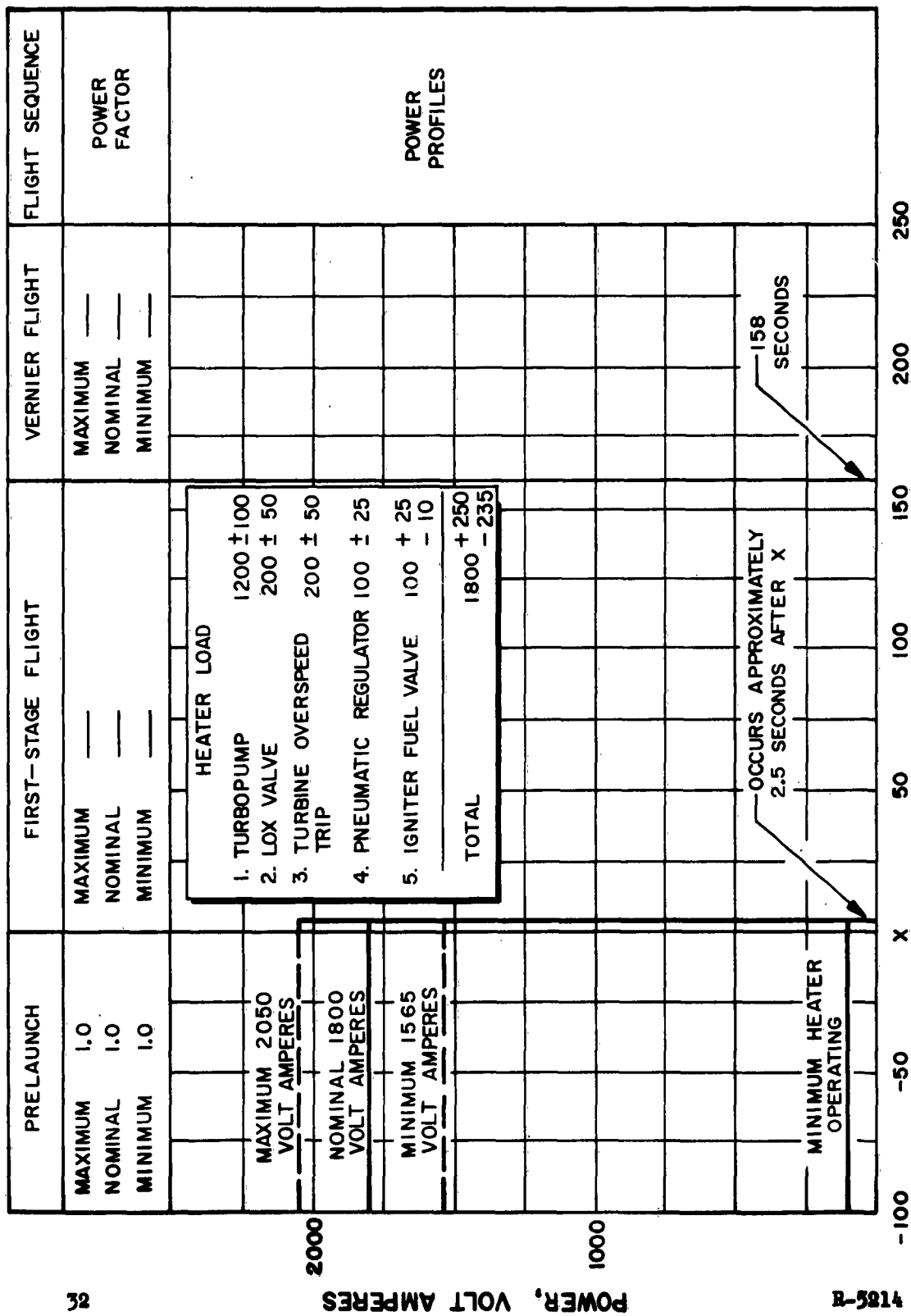


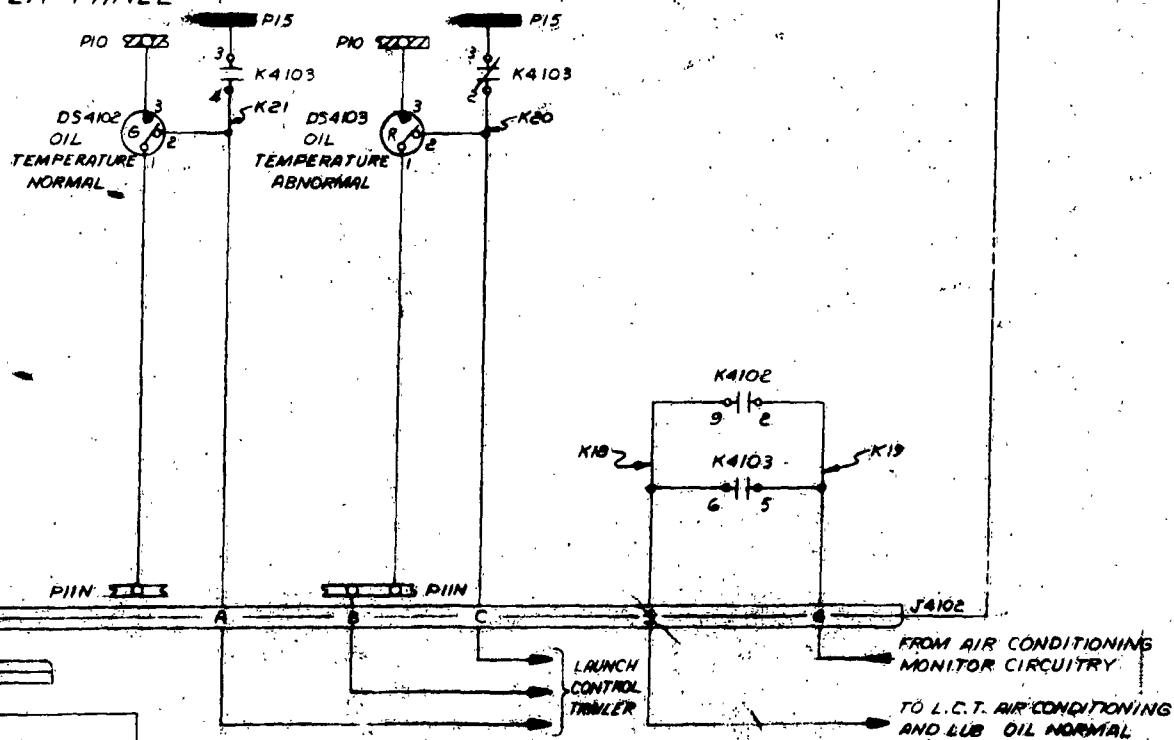
Figure 4. Direct Current Requirements (When Operated With R&D Ground Support Equipment)



**Figure 5 . Alternating Current Requirements**



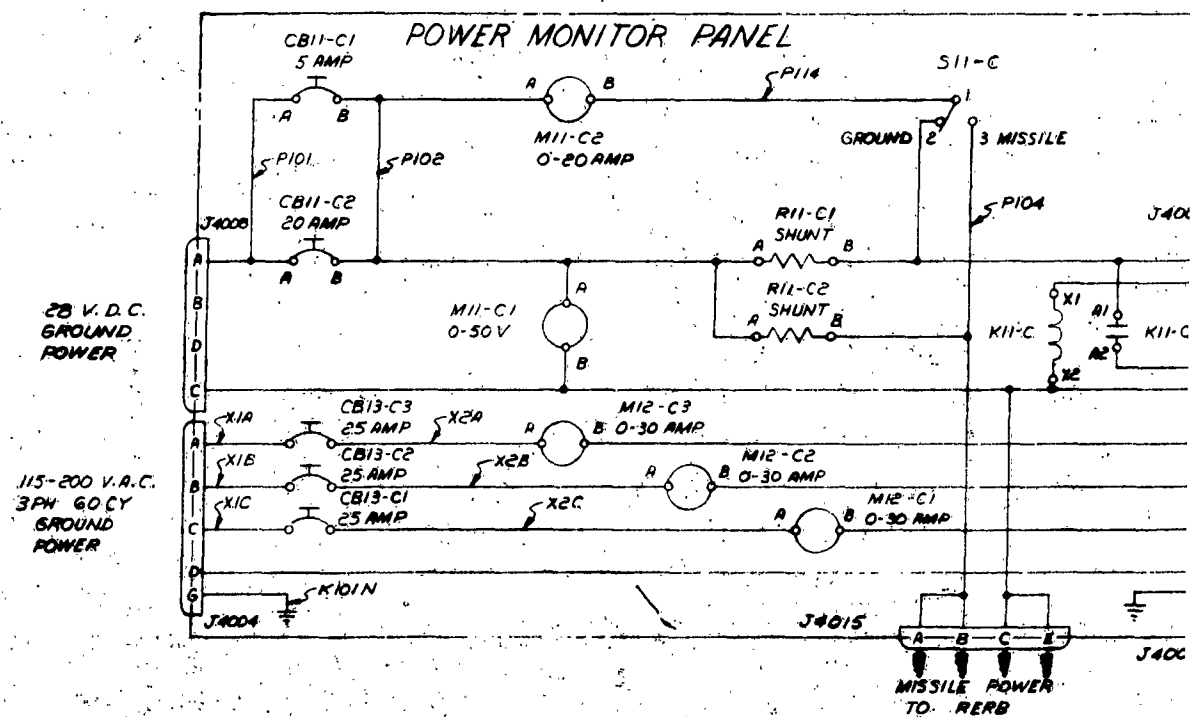
# HEATER PANEL



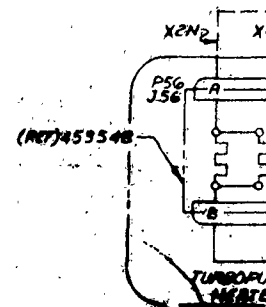
ISING  
AT LOW  
10°F ± 5°  
15°F ± 5°

TANK SENSING  
THERMOSTAT HIGH  
CLOSES 70°F ± 5°  
OPENS 45°F ± 5°

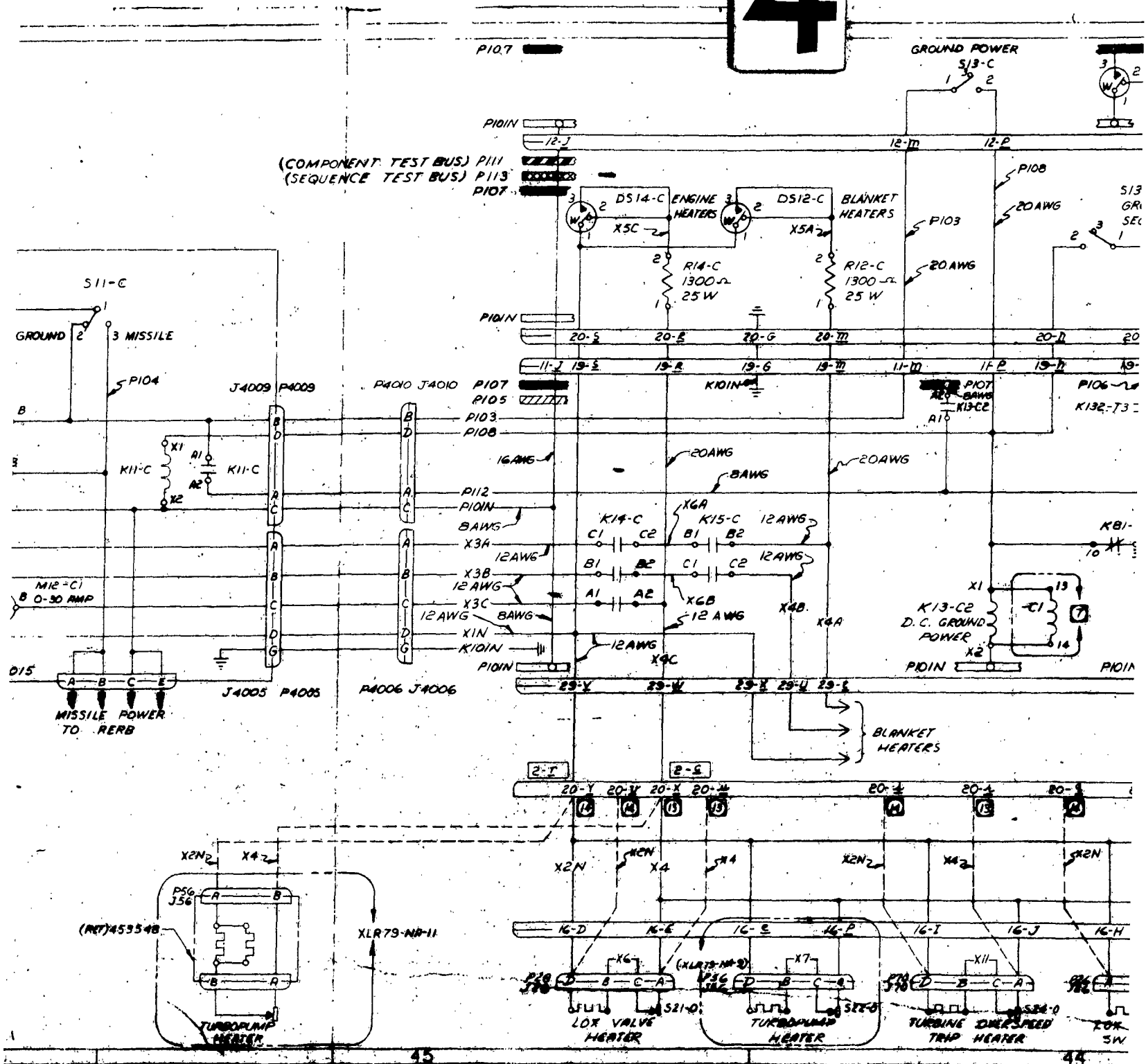
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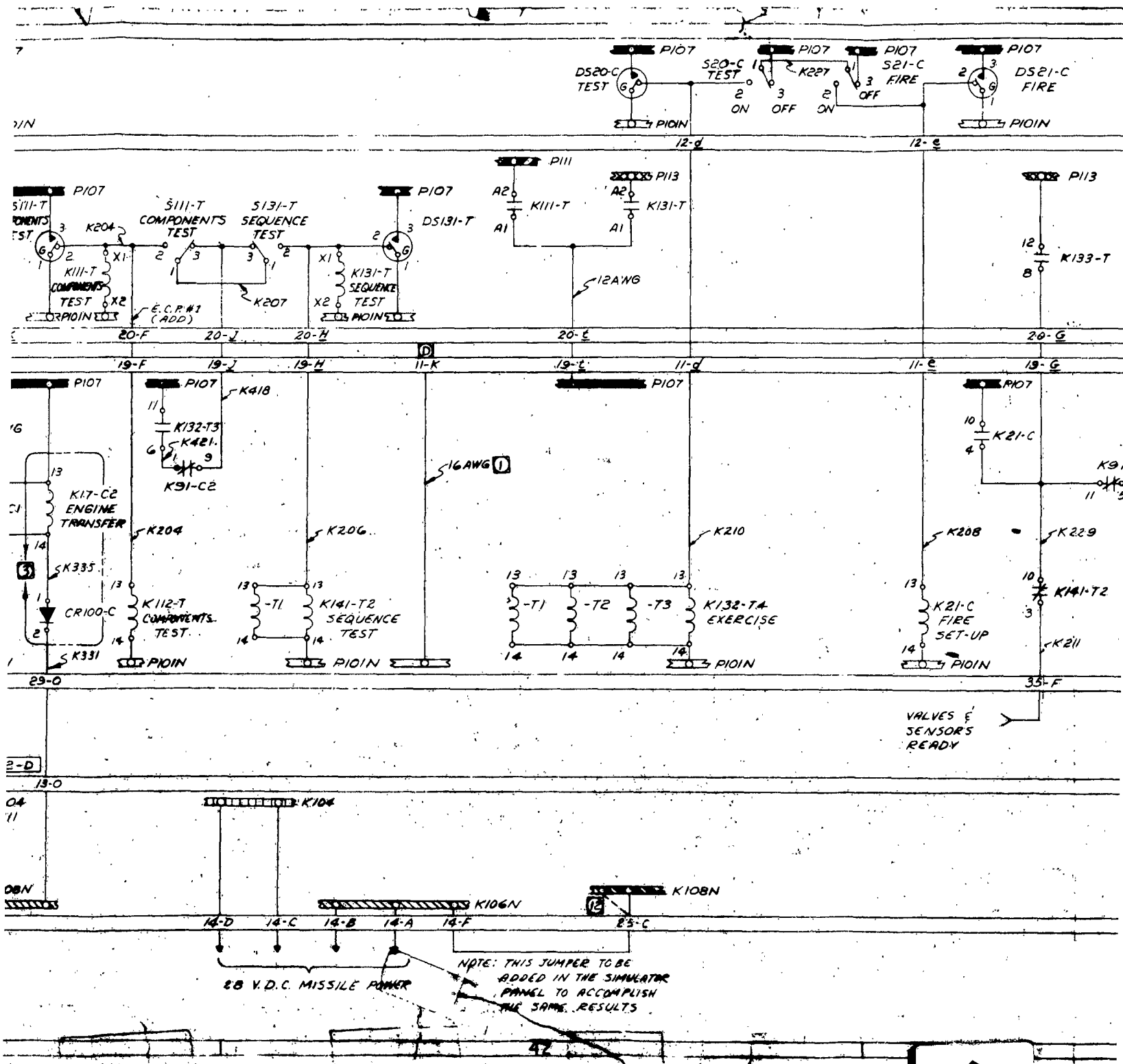
3



4



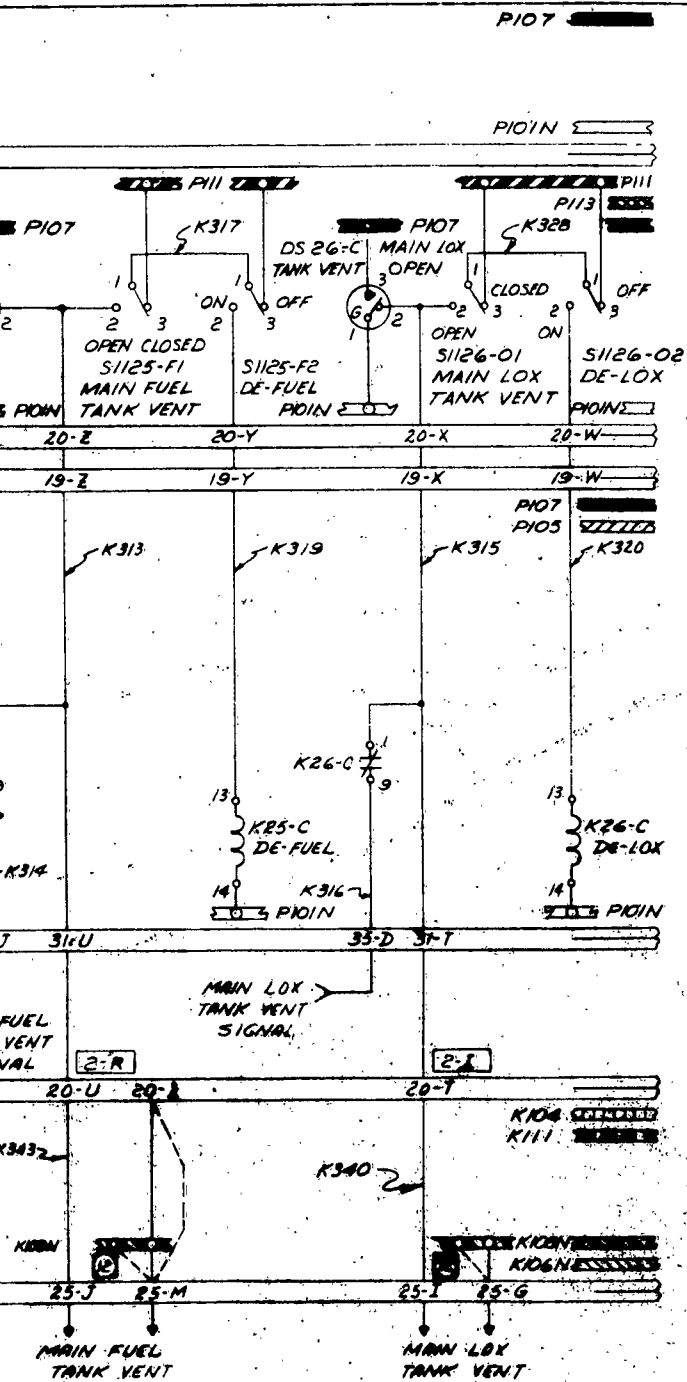




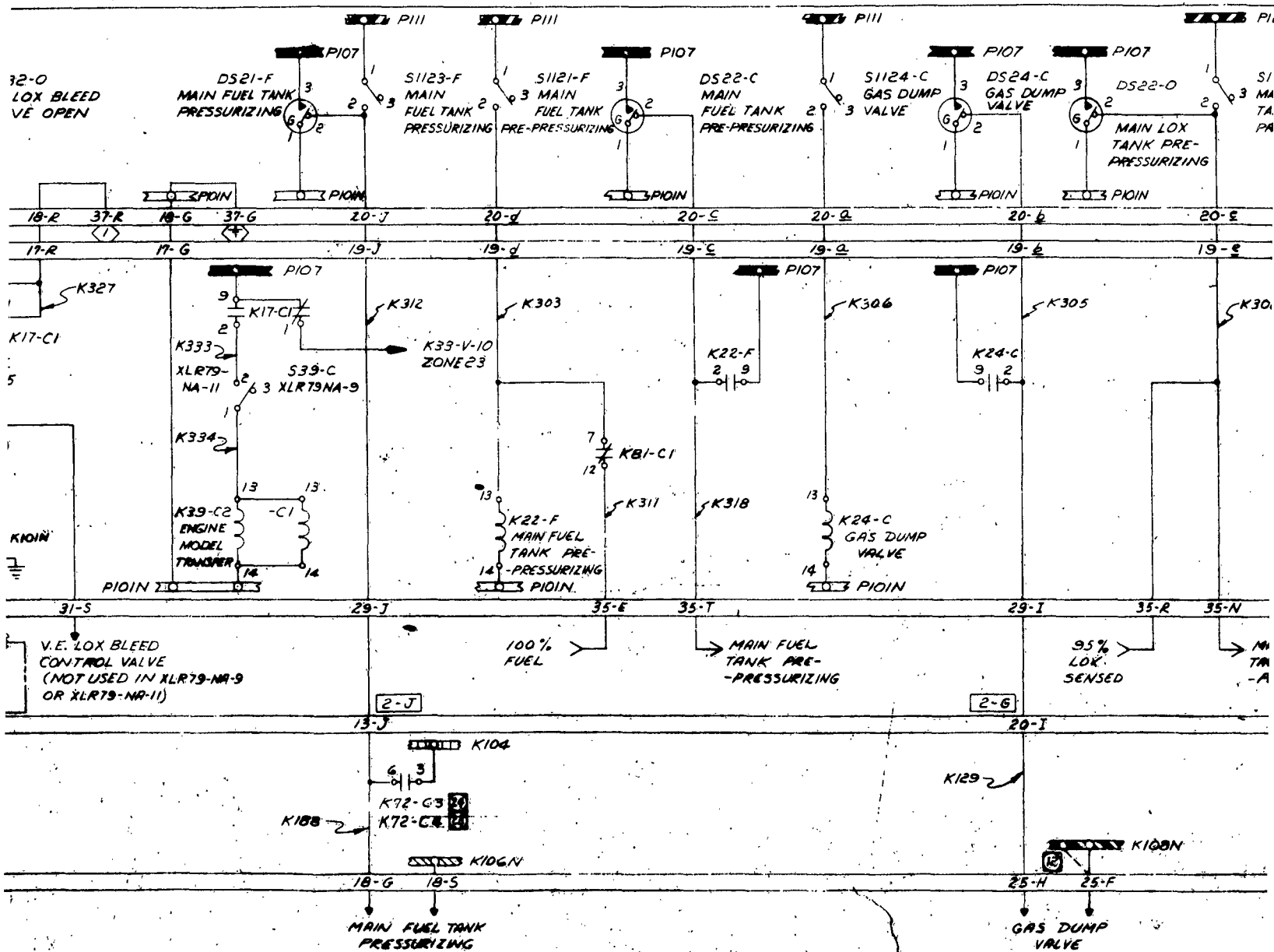
6







8





07 P107

DS34-C  
MISSILE  
COMPLETE

01 P10IN

11 P111  
13 P113  
07 P107

01 P10IN

P107  
P105

95-C  
K420  
K94-C  
PROP  
HOLD  
CUT-OFF  
P10IN  
35-H

K104  
K111

108N  
106N

KE  
S  
(NO)

P10IN

P111  
P113  
P107

P10IN

P107  
P105

DS42-F  
START TANKS  
PRESSURIZING  
3  
6  
2  
1  
P107  
P10IN  
18-2  
37-2  
20-V  
17-2  
19-V  
18-V  
37-V  
17-V  
11-11  
20-U  
19-U  
19-  
K406  
K41-C  
K132-T1  
K91-C2  
K430  
K426  
K61-C2  
K17-CE  
K427  
K17-CH4  
ZONE 39  
K44-C  
START TANKS  
PRESSURIZING  
T.D.P.U. 2.5 SEC.  
P10IN  
P10IN  
31-K  
31-G  
K407  
K132-T4  
K21-C  
K410  
K28-C1  
K419  
K35-C  
K425  
K28-C2  
MISSILE  
TANKS  
PRESSURIZED  
K411  
K81-C2  
K412  
K23-C  
ENGINE  
DISABLED  
P10IN  
P10IN  
31-A

K104  
K111

108N  
106N

15-M  
15-L  
A  
B  
P29  
J29  
L41-F  
START TANKS  
PRESSURIZING  
35

35

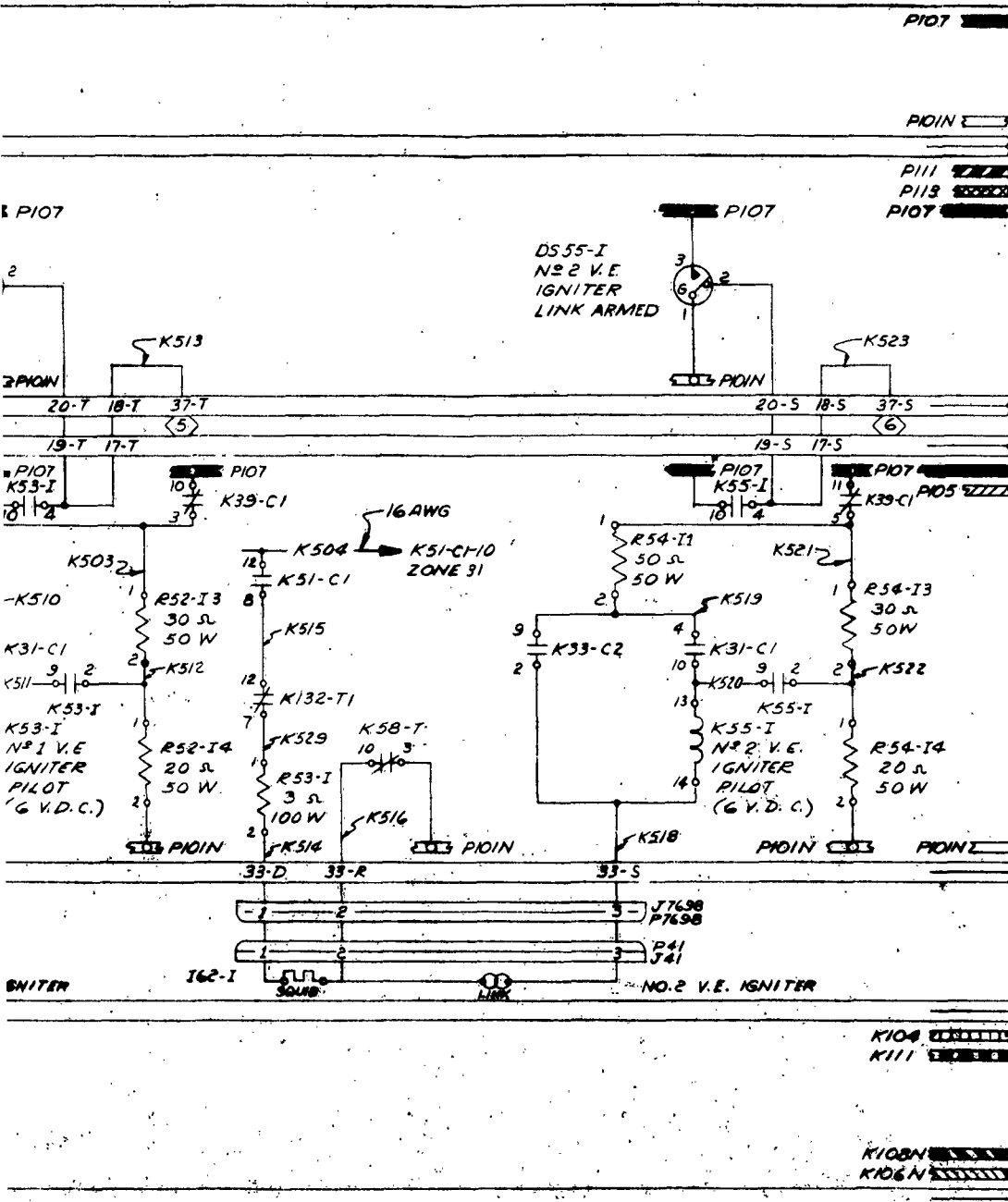
TO START TANKS  
PRESSURE SWITCHES  
(NOT USED IN XLR79-NA-9 OR XLR79-NA-11)

13-I  
2-L  
K391  
K42-C  
K307  
K43-C3  
K99-C2  
K104  
K301  
K42-C  
START TANKS  
PRESSURIZING  
K106N  
K106N  
15-M  
15-L  
A  
B  
P29  
J29  
L41-F  
START TANKS  
PRESSURIZING  
35

2-A  
20-F  
16-F  
C-A-B  
P45  
J45  
K356  
543-L  
LOX START TANK  
PRESS SWITCH  
54  
FL  
35

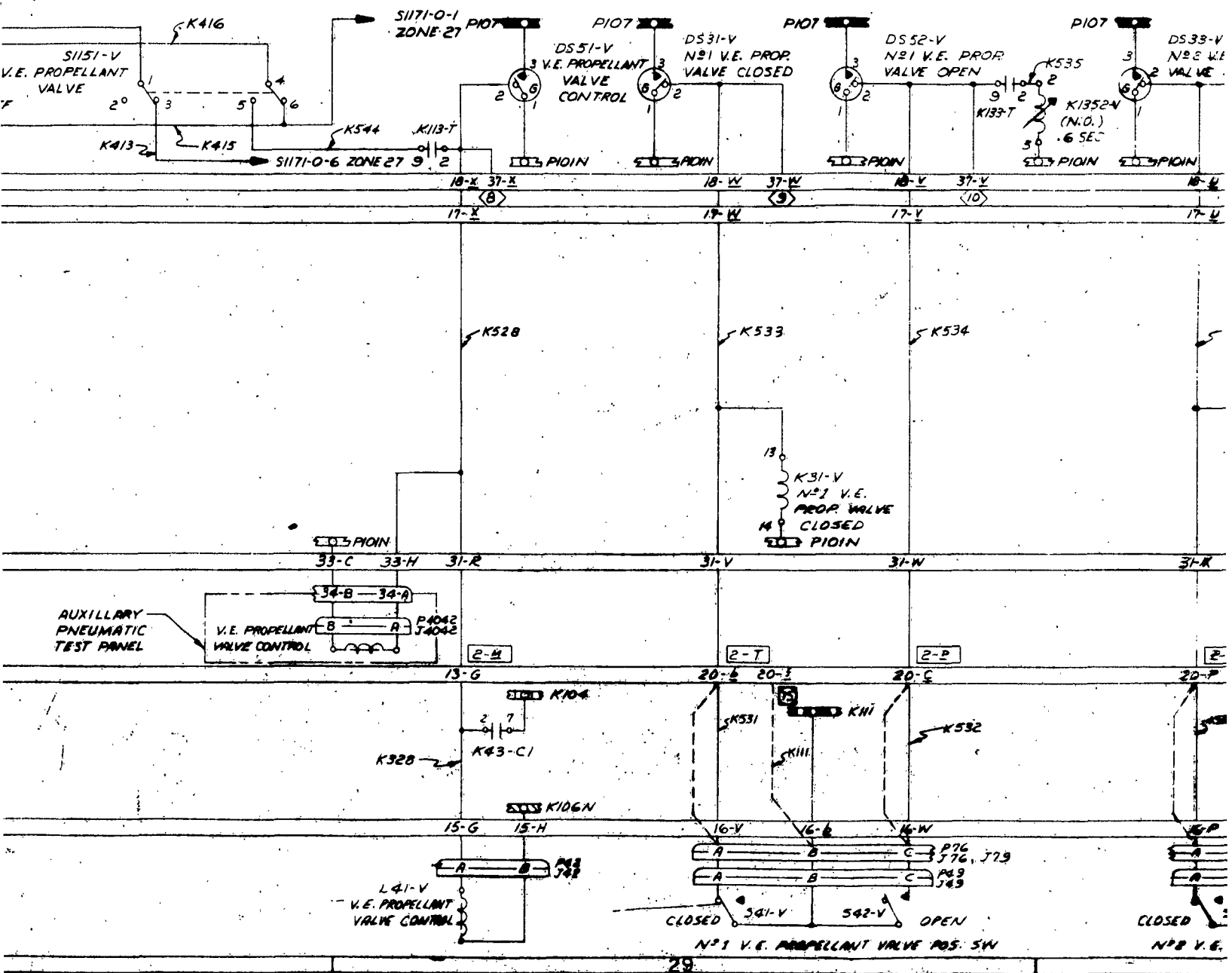
11





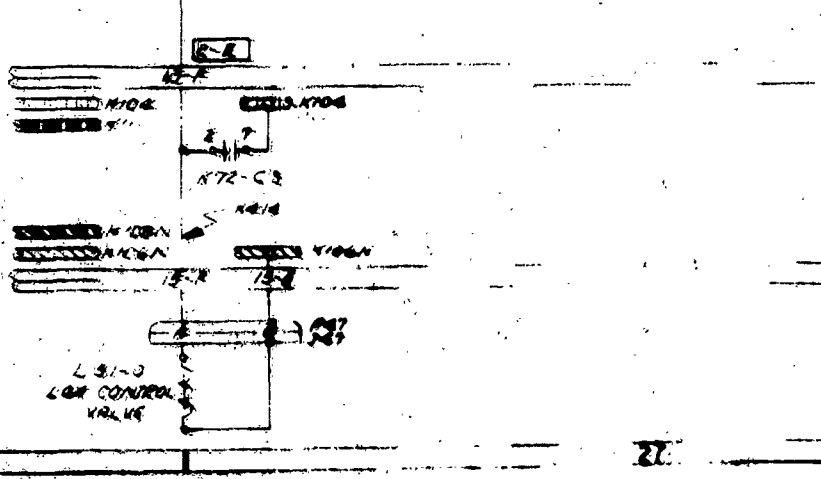
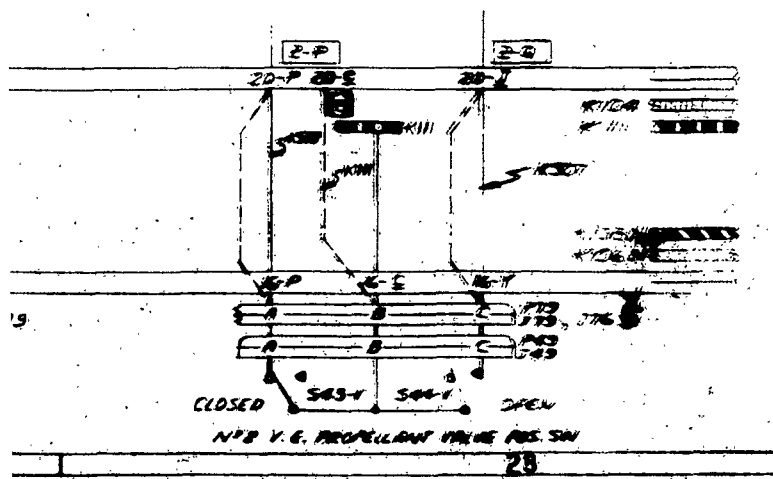
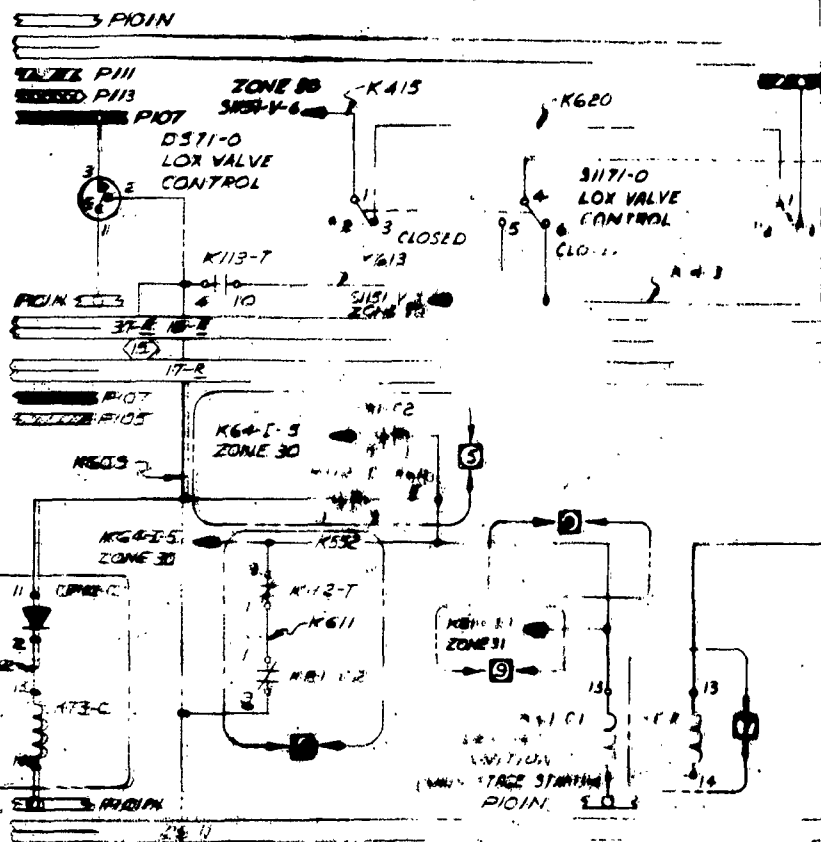
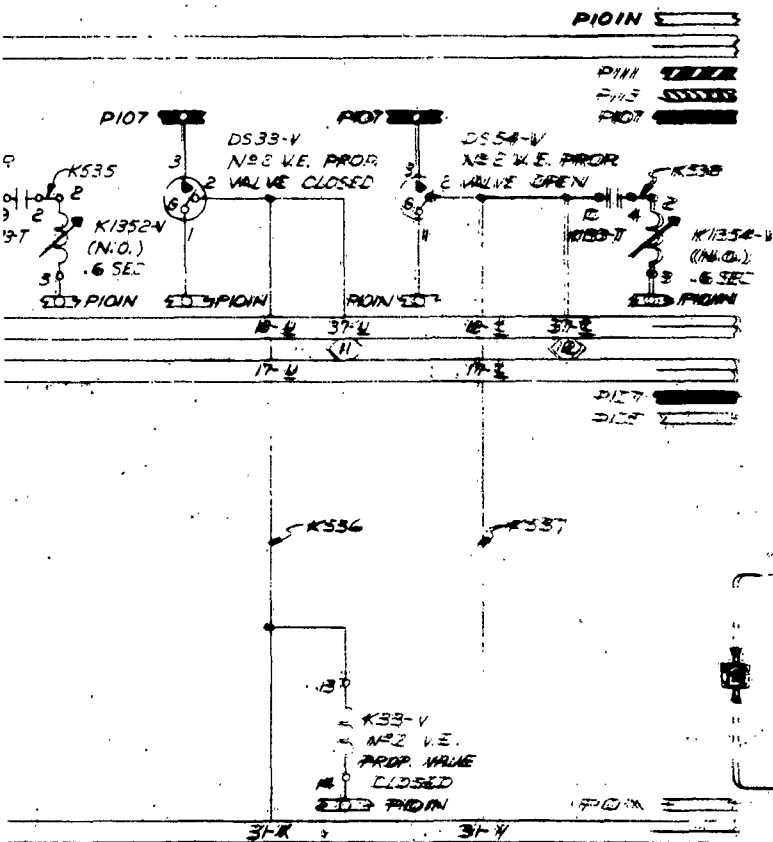




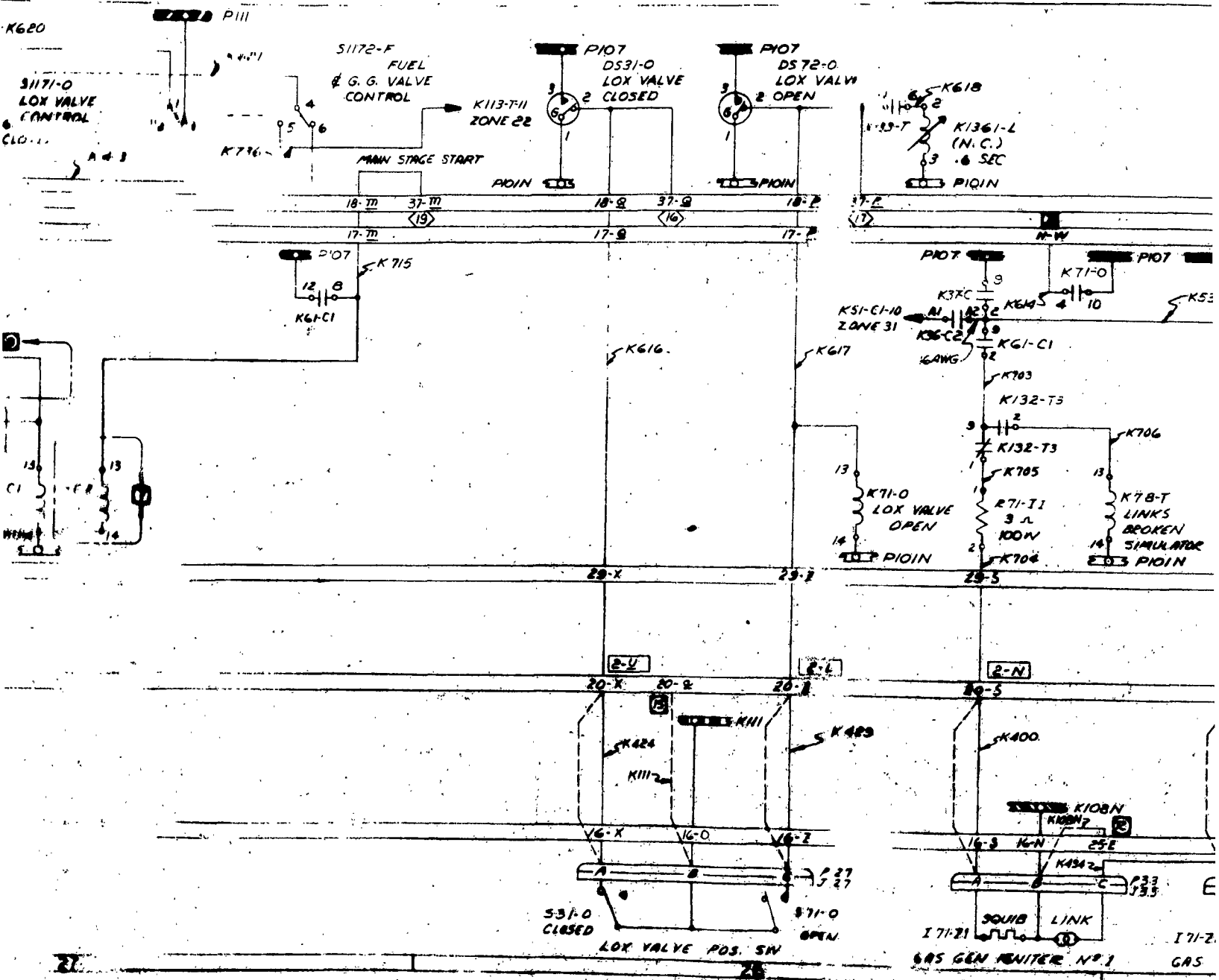


PI07

PI07



K620

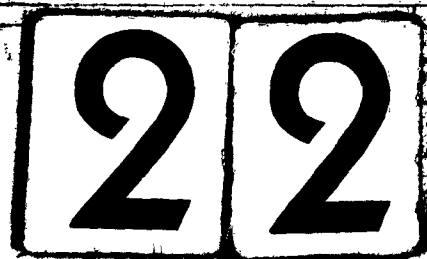






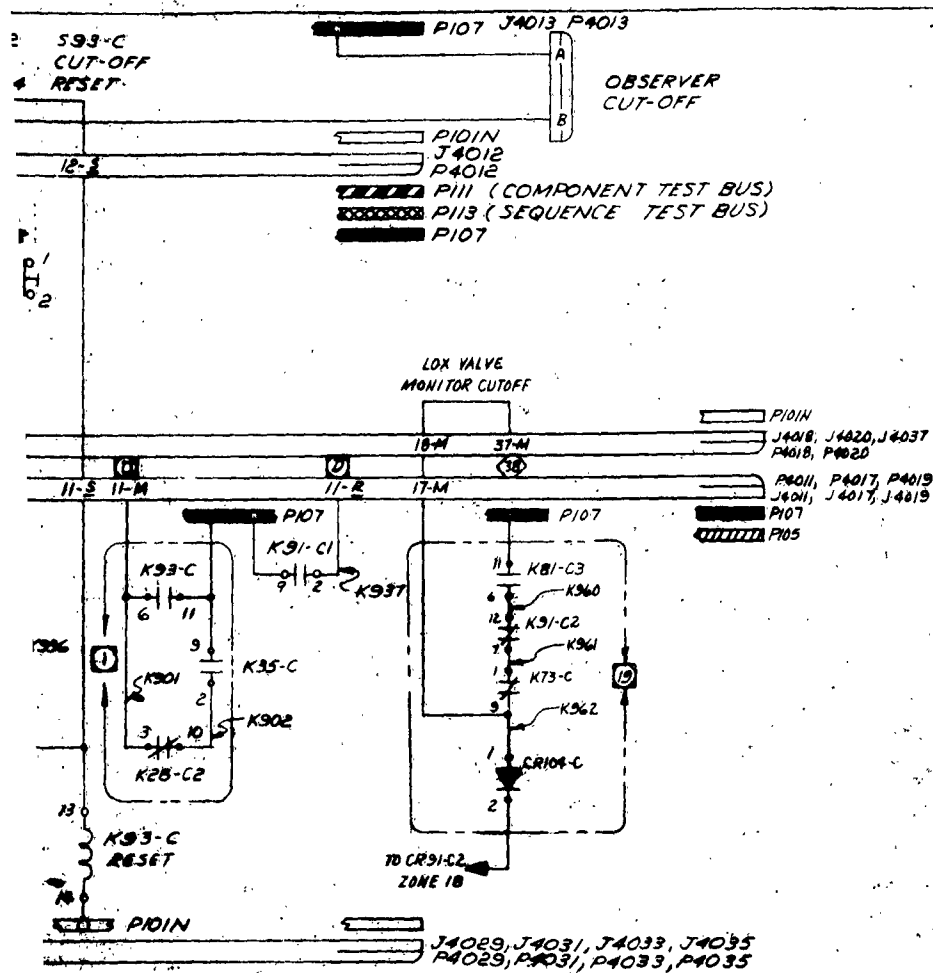












CONTROL PANEL

CONTROL-MONITOR

INTERCONNECTING BOX

GROUND & EXTERNAL EQUIPMENT

ENGINE RELAY BOX (REF)

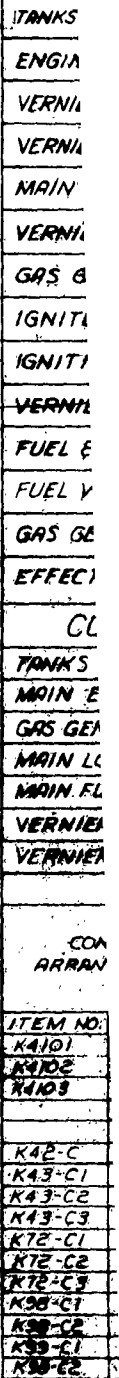
(REF WIRING DIAGRAM 500360)

ENGINE JUNCTION BOX (REF)

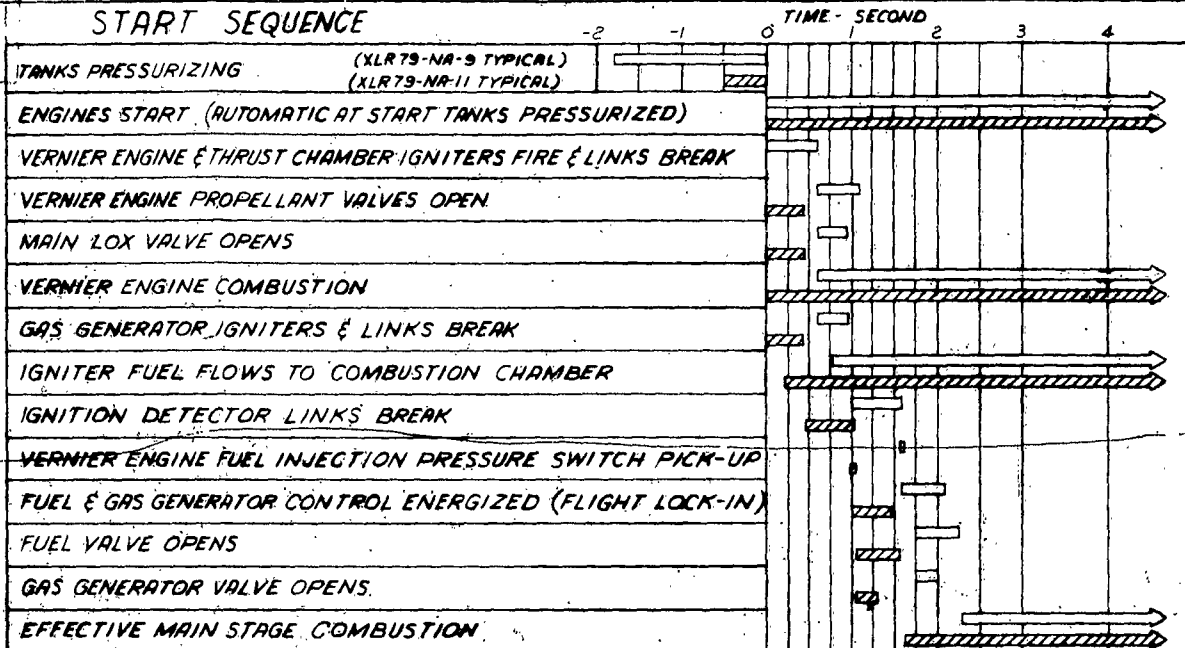
(REF WIRING DIAGRAM 500360)

ENGINE ACCESSORY SECTION (REF)

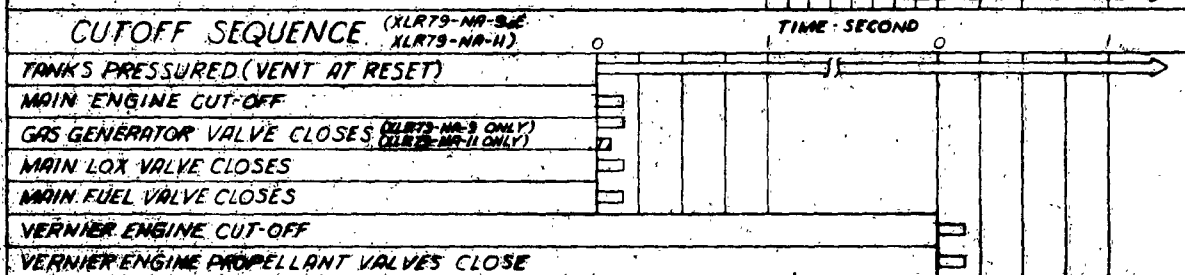




## START SEQUENCE



## CUTOFF SEQUENCE



IGNITER  
FUEL VALVE  
HEATER  
(XLR79-NA-9 ONLY)

RELAY						COIL	CONTACTS																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																										
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CONT  
ARRANG

ITEM NO.	
K11-C	4
K13-C1	4
K13-C2	4
K14-C	4
K15-C	4
K16-C	4
K17-C1	4
K17-C2	4
K21-C	4
K22-F	3
K23-C	3
K24-C	3
K25-C	4
K26-C	3
K28-C1	3
K28-C2	3
K31-C1	4
K31-C2	4
K31-F	2
K31-S	2
K31-V	2
K37-C	3
K38-O	3
K33-C1	4
K33-C2	4
K33-V	2
K39-C1	3
K39-C2	3
K35-C	3
K36-C1	3
K36-C2	3
K41-C	3
K44-C	3
K50-C	3
K51-C1	3
K51-C2	3
K53-I	3
K55-I	3
K58-T	3
K59-V	2
K61-C1	2
K61-C2	2

RELAYS				COIL		CONTACTS											
CONTACT ARRANGEMENT																	
MS24143-1				MIL-R-6106		13	9	9	10	10	11	11	12	12			
MS24140-1				MIL-R-6106		14	2	1	4	3	6	5	8	7			
MHYX-4003				ALLIED		13	9	9	10	10	11	11	12	12			
MHYX-4020				ALLIED		14	2	1	4	3	6	5	8	7			
2112-D-H3				AGASTAT		13	9	9	10	10	11	11	12	12			
HF-01 (N.C.)				G-V CONTROLS		14	2	1	4	3	6	5	8	7			
HF-01 (N.O.)				G-V CONTROLS		13	9	9	10	10	11	11	12	12			
ITEM NO.	COIL LOC	DESC	PART NO	MFGR	SPECIFICATION	NO	NC	NO	NC	NO	NC	NO	NC	NO	NC	NO	NC
K11-C	45	1P 1T	MS24140-1		MIL-R-6106	45											
K13-C1	44	4P 2T	MHXY-4003	ALLIED			43	19									
K14-C	44	3P 2T	MS24140-1		MIL-R-6106	44											
K15-C	43	3P 2T	MS24143-1			45		45		45							
K16-C	43	1P 1T	MS24140-1					45		45							
K17-C1	43	4P 2T	MHXY-4003	ALLIED	MIL-R-6106	44											
K17-C2	43					38	38	39	39	38	38	39	39				
K21-C	41					35		41		39							
K22-F	38					37											
K23-C	34						34	34									
K24-C	37																
K25-C	40																
K26-C	39						40										
							40										
K28-C1	34																
K28-C2	34						36	34		41	40	34					
							34		17								
K31-C1	41						33										
K31-C2	41						33	32		31		24					
K31-F	21						25										
K31-S	22							20	18								
K31-V	29						17										
K37-C	36																
K32-O	39						26		23								
K33-C1	40						39	39									
K33-C2	40																
K33-V	28						41	36		31		33					
K39-C1	38						32		25			34					
K39-C2	38																
K35-C	37	4P 2T	MHXY-4003	ALLIED			36	36		33		32		31			
K36-C1	36	1P 1T	MS24140-1				41										
K36-C2	36	1P 1T	MS24140-1		MIL-R-6106		17		36		36		34				
K41-C	36	4P 2T	MHXY-4003	ALLIED	MIL-R-6106		33										
K44-C	35	2P 2T	2112-D-H3	AGASTAT			36										
K50-C	35	4P 2T	MHXY-4003	ALLIED			36		35			39					
K51-C1	34		MHXY-4003														
K51-C2	34		MHXY-4003				18										
							34		31		33		32				
							30		33		23		17				
K53-I	33		MHXY-4020														
K55-I	32		MHXY-4020				33		33		41		30				
K58-T	33		MHXY-4003				32		32		41		30				
K59-V	23																
							33		32		31						
K61-C1	27						23		23			39					
K61-C2	27	4P 2T	MHXY-4003	ALLIED			26		25		20		27				
							38		18		49						

CONTACT ARRANGEMENT					
ITEM NO	COIL LOC	DESC	ITEM NO	COIL LOC	DESC
K62-I	34	2P 2T	K64-I	31	4P 2T
K66-I	24		K71-F	21	
K71-O	26		K71-S	21	
K73-C	28		K75-I	25	
K78-T	23		K81-C1	22	
K81-C2	22	4P 2T M	K81-C3	22	4P 2T M
K82-C	20	2P 2T M	K83-C	20	4P 2T M
K86-C	20		K91-C1	19	
K91-C2	19		K93-C	17	
K94-C	35		K95-C	36	4P 2T M
K96-C	19	4P 2T M	K111-T	43	1P 1T M
K112-T	43	4P 2T M	K113-T	41	4P 2T M
K131-T	42	1P 1T M	K132-T1	42	4P 2T M
K132-T2	42		K133-T3	42	
K132-T4	42		K133-T	41	
K141-T1	42		K141-T2	42	4P 2T M
K1352-V	23	1P 1T H	K1384-V	28	1P 1T H
K1361-L	26	1P 1T H			

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RELAYS					COIL	CONTACTS															
CONTACT ARRANGEMENT		MS24140-1			MIL-R-6106	X1	X2	X3													
		MHYX-4003			ALLIED	13	9	9	10	10	11	11	12	12							
		MHYX-4020				14	2	1	4	3	6	5	8	7							
		2112-D-H3			AGASTAT	A	H	B	A	B	C	E	F								
		HF-01 (N.C.)			G-V CONTROLS	2	3														
		HF-01 (N.O.)			G-V CONTROLS	3	3	4													
ITEM NO	COIL ID	DESC	PART NO	MFR	SPECIFICATION	NO	NC	NO	NC	NO	NC	NO	NC	NO	NC	NO	NC				
K62-I	34	2P 2T	2112-D-H3	AGASTAT		18		33													
K64-I	31	4P 2T	MHYX-4020	ALLIED		41		31				30	31								
K66-I	24		MHYX-4003			41				23	24		24								
K71-F	21							18						21							
K71-O	26					23		26				23									
K71-S	21		MHYX-4003					17		18				21							
K73-C	28		MHYX-4003					17						21							
K75-I	25		MHYX-4020			25		25	20	41		23	23								
K78-T	25		MHYX-4003					25													
K81-C1	22							44		36		21	38								
K81-C2	22	4P 2T	MHYX-4003	ALLIED				27		44		34	22								
K81-C3	22	4P 2T	MHYX-4003	ALLIED		17		30		43											
K82-C	20	2P 2T	2112-D-H3	AGASTAT				36		20											
K85-C	20	4P 2T	MHYX-4003	ALLIED				20													
K86-C	20							20		18											
K91-C1	19					17		44		36		41	19	34							
K91-C2	19							42	23	17		35									
K93-C	17							20		22	17	13	13								
K94-C	35					17				34		36									
K95-C	36	4P 2T	MHYX-4003	ALLIED		36		36		36		36									
K96-C	19	4P 2T	MHYX-4003	ALLIED		19	13	19		19											
K111-T	43	1P 1T	MS24140-1		MIL-R-6106	42															
K112-T	43	4P 2T	MHYX-4003	ALLIED				27													
K113-T	41	4P 2T	MHYX-4003	ALLIED		29		27		22											
K131-T	42	1P 1T	MS24140-1		MIL-R-6106	42															
K132-T1	42	4P 2T	MHYX-4003	ALLIED		44	44			33	33	33	32								
K132-T2	42					23				37	24	24	34								
K132-T3	42					26	26			23	43		44								
K132-T4	42					35				19						18					
K133-T	41					29		28		26		41									
K141-T1	42											40	36								
K141-T2	42	4P 2T	MHYX-4003	ALLIED				39		41											
K1352-V	23	1P 1T	HF-01	G-V CONTROLS		23															
K1354-V	28	1P 1T	HF-01			23															
K1361-L	26	1P 1T	HF-01	G-V CONTROLS		24															

(REB)	RESERVED			
X4	PI01	K201	K301	K401
X6	PI02	K202	K302	K402
X7	PI03	K203	K303	K403
X11	PI04	K204	K304	K404
X12	PI05	K205	K305	K405
X2N	PI06	K206	K306	K406
K104	PI07	K207	K307	K407
K106N	PI08	K208	K308	K408
K108N	PI09		K309	K409
K111	K110	K210	K310	K410
K100	PI11	K211	K311	K411
K218	PI12	K212	K312	K412
K219	PI13	K213	K313	K413
K301	PI14		K314	K414
K306	PI15		K315	K415
K307	K116		K316	K416
K317			K317	K417
K318			K318	K418
K328		K219	K319	K419
V303		K220	K320	K420
K340		K221	K321	K421
K349		K222	K322	K422
K356		K223	K323	K423
K358		K224	K324	K424
K360		K225	K325	K425
K391		K226	K326	K426
K400		K227	K327	K427
K404		K228	K328	
K414		K229	K329	
K424			K330	K430
K429		K231	K331	
K433			K332	
K434			K333	
K507			K334	
K511			K335	
K514				
K516				
K524				
K531				
K532				
K533				
K535				
K536				
K538				
K601				
K603				
K704				
K711				
K715				
K716				
K721				

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RELAYS				COIL	CONTACTS																	
MS24140-1 MIL-R-6106				X1	X2	X3																
MHYX-4003 ALLIED				13	9	9	10	10	11	11	12	12										
MHYX-4020				14	2	1	4	3	6	5	8	7										
2112-D-H3 AGASTAT				A	H	B	C	F														
HF-01 (N.C.) G-V CONTROLS				2	3	5																
HF-01 (N.O.) G-V CONTROLS				3	3	5																
LOC	DESC	PART NO	MFR	SPECIFICATION	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N		
4	2P 2T	2112-D-H3	AGASTAT		18	33																
1	4P 2T	MHYX-4020	ALLIED		41	31					30	31										
4		MHYX-4003			41					23	24			24								
1						18								21								
6					23	26					25											
1		MHYX-4003				17					18			21								
8		MHYX-4003				17								21								
5		MHYX-4020			25	25	20	41					25	23								
3		MHYX-4003				25																
2						44	36					23			38							
2	4P 2T	MHYX-4003	ALLIED			27	44					34	22									
2	4P 2T	MHYX-4003	ALLIED		17	30	43															
0	2P 2T	2112-D-H3	AGASTAT			36	20															
0	4P 2T	MHYX-4003	ALLIED			20																
2						20	18															
9						17	44	36					41	19	34							
9						42	23	17					35									
7						20	22	17	19	19												
3						17		36					36									
6	4P 2T	MHYX-4003	ALLIED		36	34					36											
1	4P 2T	MHYX-4003	ALLIED		19	19	19					19										
1	1P 1T	MS24140-1		MIL-R-6106	42																	
1	4P 2T	MHYX-4003	ALLIED			27																
1	4P 2T	MHYX-4003	ALLIED		29	27	22															
	1P 1T	MS24140-1		MIL-R-6106	42																	
	4P 2T	MHYX-4003	ALLIED		44	44	35	33	33					32								
					23		31	24	24	34												
					26	26	25	43	44													
					35	19																
					29	28	26	41														
											40	36										
	4P 2T	MHYX-4003	ALLIED		39	41																
	1P 1T	HF-01	BY CONTROLS		23																	
	1P 1T	HF-01			23																	
	1P 1T	HF-01	BY CONTROLS		24																	

[illegible]



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## RESERVED WIRE NUMBERS

K301	K401	K501	K601	K701	K101N	K901	X1A
K302	K402	K502	K602	K702	P101N	K902	X1B
K303	K403	K503	K603	K703		K903	X1C
K304	K404	K504	K604	K704		K904	X1N
K305	K405	K505		K705		K905	X2A
K306	K406	K506	K606	K706		K906	X2B
K307	K407	K507	K607	K707		K907	X2C
K308	K408	K508	K608			K908	X3A
K309	K409	K509	K609	K709		K909	X3B
K310	K410	K510		K710		K910	X3C
K311	K411	K511	K611	K711		K911	X4A
K312	K412	K512	K612	K712		K912	X4B
K313	K413	K513	K613			K913	X4C
K314	K414	K514	K614	K714		K914	X5A
K315	K415	K515	K615	K715		K915	
K316	K416	K516	K616	K716		K916	X5C
K317	K417	K517	K617	K717		K917	X6A
K318	K418	K518	K618	K718		K918	X6B
K319	K419	K519	K619	K719		K919	
K320	K420	K520	K620	K720		K920	
K321	K421	K521	K621	K721		K921	
K322	K422	K522	K622	K722		K922	P10
K323	K423	K523		K723		K923	P11N
K324	K424	K524	K624	K724		K924	X12
K325	K425	K525	K625	K725		K925	X13N
K326	K426	K526	K626			K926	X14N
K327	K427	K527	K627	K727		K927	P15
K328		K528				K928	X16
K329		K529				K929	X17N
K330	K430	K530				K930	K16
K331		K531				K931	K19
K332		K532		K732		K932	K20
K333		K533				K933	K21
K334		K534		K734		K934	X22N
K335		K535				K935	X23N
		K536		K736		K936	P24
		K537		K737		K937	
		K538		K738		K938	
		K539		K739		K939	
		K540		K740			
		K541		K741		K941	
		K542				K942	
		K543					
		K544					
				K745			
				K746			
		K547		K747			
		K548		K748	K954		
		K549		K749			
				K750			
		K552					
						K960	
						K961	
						K962	
						K963	
						K964	
						K965	

## SWITCHES

ITEM NO.	LOC.	DESC.	PART NO.	MFGR.	SPEC.
S11-C	46	1P 2T	AN3021-3		MIL-S-6745
S13-C	44		AN3021-3		
S20-C	42		AN3021-3		
S21-C	41	1P 2T	AN3021-3		
S33-C	38	1P 2T	AN3022-3		MIL-S-6745
S91-C1	18	2 CIRCUIT	W103L5-ALR	HETHERINGTON	
S91-C2	18	1 CIRCUIT	MS25089-3FB		MIL-S-6743
S92-C	19	2 CIRCUIT	MS25089-3FR		MIL-S-6743
S93-C	17	1 CIRCUIT	MS25089-3FB		MIL-S-6743
S111-T	43	1P 2T	AN3021-3		MIL-S-6745
S131-C	44		AN3021-3		
S131-T	42		AN3021-3		
S1121-F	38		AN3021-3		
S1122-C	37		AN3021-3		
S1123-F	38		AN3021-3		
S1124-C	37		AN3021-3		
S1125-F1	40		AN3021-3		
S1125-F2	40		AN3021-3		
S1126-D1	39		AN3021-3		
S1126-D2	39		AN3021-3		
S1127-C	34		AN3021-3		
S1128-D	39	1P 2T	AN3021-3		
S1135-C	37	1P 1T	AN3021-11		
S1141-O	30	2P 2T	AN3027-3		
S1151-V	30				
S1177-O	27				
S1178-F	27	2P 2T	AN3027-3		
S1185-C	20	1P 2T	AN3021-3		MIL-S-6745
S1193-C	17	1 CIRCUIT	MS25089-3FR		MIL-S-6743
S4101	49	1P 2T	MS25089-3FR		MIL-S-6743

ITEM M
DS12-C
DS13-C
DS14-C
DS15-C
DS20-C
DS21-C
DS21-A
DS22-C
DS22-L
DS24-C
DS25-C
DS26-C
DS28-C
DS31-A
DS31-C
DS31-S
DS31-Y
DS32-O
DS33-C
DS33-V
DS34-C
DS42-F
DS51-V
DS52-V
DS53-J
DS54-V
DS55-T
DS59-V
DS64-T
DS66-T
DS71-C
DS71-F
DS71-O
DS72-C
DS72-F
DS72-O
DS75-S
DS91-C1
DS91-C2
DS92-C1
DS92-C2
DS111-T
DS131-T
DS4101
DS4102
DS4103



ELLANEOUS

PART NO.	MFGR	SPEC
07271-1-5	SPEK'D-TERMINOIT	
07271-1-20		
07271-1-25		
07271-1-25		
07271-1-25	SPEK'D-TERMINOIT	
3DTI	INTERNATIONAL	
3DTI	INTERNATIONAL	
3HTI	INTERNATIONAL	
3HTI	INTERNATIONAL	
REC NO 2004		INTL-M-2004
REC NO 2004		
REC NO 2004		
REC NO 2004		INTL-M-2004

## RESISTORS

[illegible]

CONNECTOR:

CONNECTOR			
ITEM NO	LOC	DESC	PART NO
J4002	15	4 CONTACTS	MS3102E20-4P
P4002	15	4	MS3106E20-4P
J37	15	4	
P37	15	4	MS3108EMS-25W
J4004	15	7	MS3102E24-10
P4004	15	7	MS3106E24-10
J4005	15	7	MS3102E24-10
P4005	15	7	MS3106E24-10
J4006	15	7	MS3102E24-10
P4006	15	7	MS3106E24-10
J4007	15	6	MS3102E20-22
P4007	15	6	MS3106E20-22
J4008	15	6	MS3102E20-22
P4008	15	6	MS3106E20-22
J4009	15	6	MS3102E20-22
P4009	15	6	MS3106E20-22
J4010	15	6	GP3102E20-22
P4010	15	6	MS3106E20-22
J4011	15	37	GP3102E20-213
P4011	15	37	MS3106E20-211
J4012	15	37	MS3102E20-211
P4012	15	37	MS3106E20-211
J4013	14	3	MS3102E145-75
P4013	14	3	MS3106E145-75
J186			
P186	19	3	MS3102E145-75
J4015	15	6	MS3102E22-15
P4015	15	6	MS3106E22-15
J4017	14	48	GP3102E36-101
P4017	14	48	MS3106E36-101
J4018	14	48	GP3102E36-101
P4018	14	48	MS3106E36-101
J4019	14	47	GP3102E36-75
P4019	14	47	MS3106E36-75
J4020	14	47	GP3102E36-75
P4020	14	47	MS3106E36-75
J4029	15	47	GP3102E36-75
P4029	15	47	MS3106E36-75
J4031	15	24	GP3102E24-205
P4031	15	24	MS3106E24-205
J4033	15	19	GP3102E22-145
P4033	15	19	MS3106E22-14P
J4034	15	5	MS3102E45-5P
P4034	15	5	MS3106EMS-53
J4035	14	17	GP3102E20-293
P4035	14	17	MS3106E20-293
J4042			
P4042	39	2	MS3106E125-35
J4047	14	48	GP3102E36-105
P4047	14	48	MS3106E36-10P
J4078			
P4078	30	2	MS3106E1031-45
P4080	33	8	MS3106E20-75
P4081	18	8	MS3106E20-75
P4082	20	8 CONTACTS	MS3102E20-75

## CONNECTORS



LOC	DESC	PART NO	MFGR	SPEC
15 4	CONTACT	MS3106E20-4P	BENDIX	MIL-C-5015
15 4		MS3106E20-4S		
15 4		MS3106E20-4S		
15 4		MS3106E20-4S		
15 7		MS3106E24-10P		
15 7		MS3106E24-10S		
15 7		MS3106E24-10S		
15 7		MS3106E24-10P		
15 7		MS3106E24-10P		
15 7		MS3106E24-10S		
15 6		MS3106E20-22S		
15 6		MS3106E20-22P		
15 6		MS3106E20-22P		
15 6		MS3106E20-22S		
15 6		MS3106E20-22S		
15 6		MS3106E20-22P		
15 6		GP3102E20-22P		
15 6		MS3106E20-22S		
15 37		GP3102E20-21S		
15 37		MS3106E20-21P		
15 37		MS3106E20-21P		
15 37		MS3106E20-21S		
14 3		MS3106E14S-7S		
14 3		MS3106E14S-7S		
19 3		MS3106E14S-7S		
15 6		MS3106E22-15S		
15 6		MS3106E22-15P		
14 48		GP3102E36-10S		
14 48		MS3106E36-10P		
14 48		GP3102E36-10P		
14 48		MS3106E36-10S		
14 47		GP3102E36-7S		
14 47		MS3106E36-7P		
14 47		GP3102E36-7P		
14 47		MS3106E36-7S		
15 47		GP3102E36-7S		
15 47		MS3106E36-7P		
15 24		GP3102E20-20S		
15 24		MS3106E24-20P		
15 18		GP3102E22-14S		
15 19		MS3106E22-14P		
15 5		MS3106E14S-5P		
15 5		MS3106E14S-5S		
14 17		GP3102E20-20S		
14 17		MS3106E20-20P		
39 2		MS3106E12S-3S		
14 48		GP3102E36-10S		
14 48		MS3106E36-10P		
30 2		MS3106E10SL-4S		
35 8		MS3106E20-7S		
18 8		MS3106E20-7S		
20 8	CONTACT	MS3106E20-7S	BENDIX	MIL-C-5015

## CONNECTORS

ITEM NO	LOC	DESC	PART NO	MFGR	SPEC
J13	15	16 CONTACT	1672-74124-TP	500709-61	MIL-S-5015
P13	15	16	MS3106E24-7S		
J14	15	6	1672-74120-17P	500709	
P14	15	6	MS3106E20-17S		
J15	15	14	1672-74120-27S	500709-11	
P15	15	14	MS3106E20-27P		
J16	14	47	MS3106E36-7S		
P16	14	47	MS3106E36-7P		
J18	15	19	1672-74122-14S	500709-51	
P18	15	19	MS3106E22-14P		
J20	14	47	MS3106E36-7P		
P20	14	47	MS3106E36-7S		
J25	14	14	MS3106E20-27S		
P25	14	14	MS3106E20-27P		
J26		2			
P26	14	2	MS3106E10SL-4S		
J27		3			
P27	14	3	MS3106E10SL-3S		
J28		4			
P28	14	4	MS3106E10SL-3S		
J29		2			
P29	15	2	MS3106E12S-3S		
J30		4			
P30	14	4	MS3106E14S-2S		
J31		2			
P31	15	2	MS3106E12S-3S		
J32		3			
P32	13	3	MS3106E10SL-3S		
J33		3			
P33	14	3	SC06E10SL-3S		
J35		3			
P35	14	3	MS3106E14S-7S		
J38		3			
P38	14	3	SC06E10SL-3S		
J42		2			
P42	15	2	MS3106E12S-3S		
J44		3			
P44	13	3	MS3106E14S-7S		
J45		3			
P45	13	3	MS3106E14S-7S		
J47		2			
P47	15	2	MS3106E12S-3S		
J49		3			
P49	13	3	MS3106E10SL-3S		
J50		4			
P50	14	4	MS3106E14S-2S		
J56		4			
P56	14	4	MS3106E16-9S		
J70		4			
P70	14	4	MS3106E16-9S		
P76	14	10	MS3106E18-1P		
P76	14	10	MS3106E18-1S		
P79	14	10	MS3106E18-1P		
P79	14	10	MS3106E18-1S		
J92		3			
P92	13	3	MS3106E10SL-3S		
J401	49	5	MS3106E10-11P		
P401	49	5	MS3106E10-11S		
J402	49	31	MS3106E36-9S		
P402	49	31	MS3106E36-9P		
49	3	CONTACT	MS3106E10SL-4S		MIL-S-5015

33. CI  
32. CI  
31. PI  
30. AI  
29. CII  
28. CII  
27. CII  
26. CM  
25. M  
24. CC  
23. PI  
22. PI  
21. PI  
20. PI  
19. CA  
18. CI  
17. CA  
16. CA

ZONE	F
3, 17, 28	
3, 4, 11	G
3, 10, 23	H
17, 22, 38	J
21	K

33. CIRCUITRY TO BE ADDED FOR MB3-151 (G1000 MD 6)  
 32. CIRCUITRY TO BE ADDED FOR MB3-150 (G1000 MD 15)  
 31. REMOVED PER MB3-149  
 30. ADDED PER MB3-149  
 29. CIRCUITRY TO BE ADDED FOR MB3-144 (G1000 MD 14)  
 28. CIRCUITRY TO BE REMOVED FOR MB3-144 (G1000 MD 14)  
 27. CIRCUITRY TO BE INSTALLED FOR HYBRID ENGINE FIRING (G1000 MD 13 & G3000 MD 17)  
 26. CIRCUITRY TO BE INSTALLED FOR LOX VALVE MONITOR CUT-OFF (G1000 MD 12 & G3000 MD 5)  
 25. MY7002 RELAYS REPLACED ON ALL ENGINE RELAY BOXES BY NAB-27103 TYPE I RELAYS  
 24. CONNECTORS CODED 16 REPLACED ON ALL ENGINE RELAY BOXES BY CONNECTORS CODED 17  
 23. PINS 1, 15, 2, 16 ARE BUSSED TOGETHER IN J20 INTERNALLY  
 22. PINS 3, 17, 4, 18 ARE BUSSED TOGETHER IN J20 INTERNALLY  
 21. PINS 5, 19, 6, 20 ARE BUSSED TOGETHER IN J20 INTERNALLY  
 20. PINS 7, 21, 8, 22 ARE BUSSED TOGETHER IN J25 INTERNALLY  
 19. CIRCUITRY TO BE ADDED FOR MB3-19 (G1000 MD 11)  
 18. CIRCUITRY TO BE REMOVED FOR MB3-19 (G1000 MD 11)  
 17. CIRCUITRY TO BE ADDED FOR MB3-24 (G1000 MD 11)  
 16. CIRCUITRY TO BE REMOVED FOR MB3-24 (G1000 MD 11)  
 15. CIRCUITRY TO BE ADDED FOR START TANKS PRESSURIZING CUT-OFF, GROUND POWER FAILURE CUT-OFF & SEPARATION OF MISSILE (G1000 MD 11)  
 14. CIRCUITRY TO BE REMOVED FOR START TANKS PRESSURIZING CUT-OFF, GROUND POWER FAILURE CUT-OFF & SEPARATION OF MISSILE (G1000 MD 11)  
 13. CIRCUITRY TO BE ADDED FOR LAUNCH LOCKOUT (G1000 MD 6 (UP))  
 12. CIRCUITRY TO BE REMOVED FOR LAUNCH LOCKOUT (G1000 MD 6 (UP))  
 11. CIRCUITRY TO BE ADDED FOR RESET OF XLR 19-NAT (G1000 MD 4 (UP))  
 10. CIRCUITRY TO BE REMOVED FOR STATIC FIRING (G1000 MD 5)  
 9. CIRCUITRY TO BE INSTALLED FOR STATIC FIRING (G1000 MD 5, G3000 MD 5)  
 8. UNDERLINED CONNECTOR PIN LETTERS DENOTE LOWER CASE.  
 7. REF DWG 900040 SCHEMATIC.  
 6. REF DWG 900075 BLOCK DIAGRAM  
 5. SYMBOL  INDICATES RECORDER CONNECTIONS  
 4. REF DWG SCHEMATIC NO. 902500 FOR ENGINE SIMULATOR  
 3. SYMBOL  DENOTES DOUGLAS AIRCRAFT COMPANY CONNECTIONS.  
 2. WIRES ARE #20 AWG FOR ALL PANELS & WIRES ARE #16 AWG FOR ALL CABLES  
 1. THE COMPLETE REFERENCE SYMBOL DESIGNATION FOR CONNECTORS IS IN 4000 SERIES (EXAMPLE: J37 IS J 4037) EXCEPT THOSE IN ENGINE RELAY BOX, ENGINE JUNCTION BOX, & ENGINE ACCESSORY SECTION.

NOTE: UNLESS OTHERWISE SPECIFIED

DRILL	TOL
.0156 TO .156	
.156 TO .316	
.316 TO .476	
.476 TO .636	
.636 TO .796	

# 36

ZONE	F		
3,174 28		1. ADDED NOTE 26 & CIRCUITRY FOR LOX VALVE MONITOR CUTOFF	3 ECP MB3-67 4-16-60 J. C. Smith
3,4 41	G	1. ADDED NOTE 27 & CIRCUITRY FOR HYBRID ENGINE FIRING	3 ECP MB3-103 3-22-61 J. C. Smith
3,10 23	H	1. ADDED NOTE 28 & 29 & CIRCUITRY FOR FLIGHT LOCK-IN CIRCUIT	3 ECP MB3-144 8-13-62 J. C. Smith
17,22 38	J	1. ADDED NOTE 30 & 31, CODE & CIRCUITRY FOR FLIGHT LOCK-IN CIRCUIT	3 ECP MB3-119 B.J. LUCAS 11-14-62
21	K	1. ADDED NOTE 32 & 33, CODE & RECORDING CIRCUIT THROUGH CONTROL MONITOR	3 ECP MB3-160 ECP MB3-161 12/13/62 SVOREN

		REVISIONS		PARTS MADE OF	
ZONE	SYM	1 MAY BE REWORKED	2 RECORD CHANGE	3 DATE	SIGNATURE
17,18 35 19	A	1. ADDED PROP TRANSFER HOLD CUT-OFF CIRCUITRY	3		
		2. ADDED K91-C2 CONTACTS	3		
		3. ADDED PROP DEPLETION CUT-OFF, SLOW BUILD-UP CUT-OFF, HIGH TEMPERATURE CUT-OFF	3	11-1-58	B. BEATTIE
19,20 27	B	1. ADDED RESET CIRCUITRY	3		
		2. ADDED RELAY K17-C2, NOTE 11	3		
		3. CHANGED LAUNCH LOCKOUT CIRCUITRY	3		
		4. ADDED NOTES 12 & 13	3		
		5. RELAY K44-C T.D.P.U. 2.5 SEC. WAS 1.5 SEC.	3	1-5-59	B. BEATTIE
19,20 35	C	1. ADDED NOTES 14 & 15	3		
		2. ADDED COMPONENTS LIST FOR ENGINE RELAY & JUNCTION BOX	3		
		3. ADDED CONTROL-INDICATOR LUB. TANK HEATER CIRCUITRY	3		
		4. ADDED AUXILIARY PNEUMATIC TEST PNL CIRCUITRY	3	5-22-59	B. BEATTIE
19,20 35	D	1. ADDED NOTES 16 & 17, & RELATED CIRCUITRY	3		
		2. ADDED NOTES 18 & 19, & RELATED CIRCUITRY	3	9-30-59	B. BEATTIE
19,20 35	E	1. ADDED NOTES 20, 21, 22 & 23, & RELATED CIRCUITRY	3		
		2. SOIC 81 WAS 500396	3		
		3. ADDED NOTES 24 & 25	3		
		4. 500352-11 WAS 500852	3		
		5. ADDED SEQUENCE CHART	3	11-23-59	B. BEATTIE

TO BE ADDED FOR START TANKS PRESSURIZING  
AND POWER FAILURE CUT-OFF & SEPARATION OF MISSILE & G1000 BUSES (G1000MD7 & UP)  
TO BE REMOVED FOR START TANKS PRESSURIZING  
AND POWER FAILURE CUT-OFF & SEPARATION OF MISSILE & G1000 BUSES (G1000MD7 & UP)  
TO BE ADDED FOR LAUNCH LOCKOUT (G1000MD6 & UP)  
TO BE REMOVED FOR LAUNCH LOCKOUT (G1000MD6 & UP)  
TO BE ADDED FOR RESET OF XLR 79-NA-7 (G1000MD4 & UP)  
TO BE REMOVED FOR STATIC FIRING (G1000MD3)  
TO BE INSTALLED FOR STATIC FIRING (G1000MD5, G3002MD2)  
CONNECTOR PIN LETTERS  
POWER CASE.

00040 SCHEMATIC,  
00075 BLOCK DIAGRAM  
INDICATES RECORDER CONNECTIONS  
SCHEMATIC NO. 902500 FOR  
MULATOR  
ENOTES DOUGLAS AIRCRAFT  
CONNECTIONS.  
200 AWS FOR ALL PANELS &  
116 AWS FOR ALL CABLES  
REFERENCE SYMBOL DESIGN-  
CONNECTORS IS IN 4000 SERIES  
37 IS J 4037) EXCEPT THOSE IN  
Y BOX, ENGINE JUNCTION BOX,  
CESSARY SECTION.  
OTHERWISE SPECIFIED

## FOR REFERENCE ONLY

<b>DRILLED HOLE TOLERANCES</b> .0136 TO .1286 +.002, -.001 .136 TO .286 +.003, -.001 .286 TO .436 +.004, -.001 .436 TO .586 +.005, -.001 .586 TO .736 +.007, -.001 .736 TO .886 +.010, -.001	<b>DISPOSITIONS PRIOR TO FINISH</b> TOLERANCES EXCEPT AS NOTED UNLESS SPECIFIED OTHERWISE 1. FINISH SURF. ROUNDED TO RCP 2. FINISH SURF. ROUNDED TO RCP 3. FINISH SURF. ROUNDED TO RCP 4. FINISH SURF. ROUNDED TO RCP 5. FINISH SURF. ROUNDED TO RCP 6. FINISH SURF. ROUNDED TO RCP 7. FINISH SURF. ROUNDED TO RCP 8. FINISH SURF. ROUNDED TO RCP 9. FINISH SURF. ROUNDED TO RCP 10. FINISH SURF. ROUNDED TO RCP	<b>DATE: 2-3-58</b> DRAWN: <u>W. J. MAT</u> CHECKED: <u>W. J. MAT</u> BY: <u>W. J. MAT</u> MATL	<b>SCHEMATIC-ENGINE ELEC SYSTEM</b> SCALE: <u>None</u> WT	<b>ROCKETDYNE</b> A DIVISION OF NORTH AMERICAN AVIATION, INC. 6665 CANBON AVE. CANBON PARK, CALIFORNIA DWG NO. <b>900100</b>
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001006

3

## OPERATING REQUIREMENTS AND LIMITATIONS

Frequently reviewed specifications and limitations applicable to operation of the LV-2A propulsion system are contained in this section.

### FUEL PUMP INLET (RJ-1)

The minimum required NPSH for starting at 0 to 120 F is 80 feet. The minimum required NPSH for nominal rated thrust operation at 0 to 120 F is 34 feet. The maximum allowable surge pressure at 0 to 120 F is 160 psig.

### OXIDIZER PUMP INLET

At saturation temperature, (1) the minimum required net positive suction head (NPSH) for starting is 55 feet, (2) the minimum NPSH required for nominal rated thrust operation is 55 feet, and (3) the maximum allowable surge pressure is 160 psig.

## GROUND AND FLIGHT LOADING CONDITIONS

### Handling Load

The main and vernier engines shall withstand a maximum of 4 g handling loads applied in any direction.

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Flight Operation

The engine system shall operate satisfactorily without permanent deformation or failure under the following specified loads:

1. Load of 15 g parallel to the direction of flight and 1 g perpendicular to the direction of flight
2. Load of 12 g parallel to the direction of flight and 1.25 g perpendicular to the direction of flight
3. Load of 10 g parallel to the direction of flight and 1.5 g perpendicular to the direction of flight
4. Load of 2.5 g parallel to the direction of flight and 3 g perpendicular to the direction of flight



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Critical Customer Connect Point Maximum Loading

The customer connect point maximum loading is as follows:

<u>Attach Point*</u>	<u>Allowable Loads</u>
Mount Attach to Missile (Pt. 1)	$F_y = 63,000$ lb 5930-lb side load
Mount Attach to Missile (Pt. 2)	$F_y = 63,000$ lb 5930-lb side load
Mount Attach to Missile (Pt. 3)	$F_y = 63,000$ lb 5930-lb side load
LOX Inlet Duct	$F_y = 3,200$ lb
Fuel Inlet Duct	$F_y = 7,200$ lb
Actuator Attach Point	$\pm 10,000$ lb axial force
Aft End of Heat Exchanger	300 lb any direction
Forward Attach Lug Heat Exchanger	380 lb any direction
Aft Attach Lug Heat Exchanger	$F_y = \pm 380$ lb
	$F_x = \pm 50$ lb
	$F_z = \pm 380$ lb
Main Oil Discharge	100 lb any direction
LOX Seal Drain	50 lb any direction
Oil Seal Drain	50 lb any direction

\*Refer to coordinate system

## PNEUMATIC SUPPLY

The pneumatic supply as delivered to the main engine manifold will be MIL-N-6011 nitrogen, liquid and gas. The flows quoted are for the propulsion system requirements only. No allowance has been made for other applications.

1. Standby: high-pressure nitrogen, 0.150 lb/min maximum is required at 3000 to 1000 psi for oxidizer pump seal purge and the engine control system bleed and leakage. Nitrogen temperature range is -65 to +160 F.
2. Starting: high-pressure nitrogen, 4.0 lb maximum is supplied at 3000 to 1500 psi and at a temperature range of -65 to +160 F for oxidizer pump seal purge, engine start tank pressurization, and pneumatic control.
3. Flight operation: high-pressure nitrogen, 2.0 lb maximum is supplied at 3000 to 800 psia and at a temperature range of -65 to +160 F for oxidizer pump seal purge, controls, and engine lubrication tank pressurization. Maximum flowrate is 0.0115 lb/sec.
4. Vernier engine solo flight: high-pressure nitrogen, 8.0 lb maximum is supplied at 3000 to 800 psia and at a temperature range of -65 to +160 F for vernier tank pressurization and pneumatic control. Maximum flowrate is 0.89 lb/sec.

The regulated pneumatic pressure at the customer supply connect-point is 660 psia.

A nitrogen supply temperature of 70 F was assumed for the above computations.

SECTION II: PROPULSION SYSTEM PERFORMANCE

STEADY-STATE PERFORMANCE

Steady-state performance values presented in this section were obtained from production engine test results. Run-to-run deviations include random instrumentation errors and run-to-run nonrepeatability. The actual component differences are depicted in the engine-to-engine deviations.

#### RATED MAIN ENGINE PERFORMANCE

The main engine nominal performance values and attendant variations at sea-level standard temperature and pressure, rated thrust and rated mixture ratio appear in Table 5 . The vernier performance values were analytically determined using a typical vernier system downstream of the customer connect points. Since vernier performance depends upon the pressure supplied by the main engine, it will not exactly agree with rated values obtained from vernier production testing. A performance schematic depicting relative positions of flow and pressure data is presented in Fig. 6 .

Run-to-run deviations in engine thrust and mixture ratio, and run-to-run and engine-to-engine deviations in specific impulse for the main engine are presented in Table 6 .

Information regarding effects of nitrogen dilution on engine performance is included for application for analysis in the event of a suspected occurrence. Performance shifts of sea-level engine specific impulse and thrust due to nitrogen dilution of LOX presented in Fig. 7 and 8 were based on test results conducted on an engine system other than, but considered sufficiently descriptive of, the Thor. Empirically determined effects on  $c^*$ ,  $C_F$ , gas generator temperature and LOX density due to nitrogen dilution were imposed on nominal engine data to generate the figures.

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TABLE 5

NOMINAL MAIN ENGINE PERFORMANCE VALUES  
AT SEA-LEVEL RATED THRUST AND MIXTURE RATIO

Parameter	Nominal Value	Standard Deviation	
		Engine-to-Engine (S <sub>EE</sub> )	Run-to-Run (S <sub>RR</sub> )
Engine			
Oxidizer (LOX) Density, lb/cu ft	71.38*		
Fuel (RJ-1) Density, lb/cu ft	53.17*		
Thrust, pounds	170,000*	---	---
Specific Impulse, seconds	252.4	0.62	0.30
Mixture Ratio (o/f), including vernier flow	2.15*	---	---
Thrust Chamber			
Thrust, pounds	169,500	---	---
Specific Impulse, seconds	257.5	0.62	0.31
Characteristic Velocity (c*), injector end, ft/sec	5958	15.4	9.5
Thrust Coefficient (C <sub>F</sub> ), injector end	1.391	0.0038	0.0021
Chamber Pressure, injector end,psia	594.3	1.53	0.92
Characteristic Velocity, nozzle stagnation, ft/sec	5517.	---	---
Thrust Coefficient, nozzle stagnation	1.502	---	---
Chamber Pressure, nozzle stagnation, psia	550.3	---	---
c* Efficiency, %	95.5	0.25	0.15
C <sub>F</sub> Efficiency, %	101.2	0.25	0.15
Propellant Flowrates, lb/sec			
Oxidizer	456.3	1.11	0.54
Fuel	201.9	0.48	0.26
Mixture Ratio (o/f)	2.260	0.0016	0.0008
Main Fuel Orifice Pressure Drop,psi	55.6		
at 190 lb/sec and 53.17 lb/cu ft	49.2	10.3	1.8
Orifice Diameter, inches	2.74		

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TABLE 5  
(Continued)

Parameter	Nominal Value	Standard Deviation	
		Engine-to-Engine (S <sub>EE</sub> )	Run-to-Run (S <sub>RR</sub> )
Propellant Pumps			
LOX Pump			
Inlet Pressure (total), psia	53.0*	---	---
Discharge Pressure (total),psia	862.	14.8	2.9
Developed Head, feet	1641.	11.8	6.7
Weight Flow, lb/sec	469.9	1.14	0.56
Volume Flow, gpm	2955.	7.2	3.5
Speed, rpm	6252.	26.8	8.4
Shaft Power, bhp	1772.	16.2	8.6
Efficiency, %	79.1	---	---
Fuel Pump			
Inlet Pressure (total), psia	48.0*	---	---
Discharge Pressure (total), psia	902.	14.8	2.9
Developed Head, feet	2307.	39.8	7.8
Weight Flow, lb/sec	217.2	0.53	0.26
Volume Flow, gpm	1833	4.50	2.18
Speed, rpm	6252.	26.8	8.4
Shaft Power, bhp	1272.	22.0	5.24
Efficiency, %	71.6	---	---
Turbine			
Turbine Shaft Power, bhp	3136.	31.	13
Turbine Inlet Temperature, F	1203.	10.6	3.0
Turbine Gas Flow, lb/sec	15.21	0.16	0.05
Turbine Exhaust Pressure (static), psia	23.6	1.69	0.25
Turbine Inlet Pressure (total),psia	515.6	4.8	2.3
Turbine Pressure Ratio (total psia inlet/static exhaust)	21.8	---	---

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TABLE 5  
(Continued)

Parameter	Nominal Value	Standard Deviation	
		Engine-to-Engine (S <sub>EE</sub> )	Run-to-Run (S <sub>RR</sub> )
Gas Generator			
Gas Generator Chamber Pressure, injector end, psia	541.4	5.5	1.6
LOX Bleed Pressure, psia	788.	----	----
Fuel Bleed Pressure, psia	888.	----	----
Total Propellant Flow **, lb/sec	15.21	0.16	0.05
LOX Flow**, lb/sec	3.73	0.04	0.01
Fuel Flow**, lb/sec	11.48	0.14	0.04
Mixture Ratio (o/f)	0.325	0.004	0.001
Fuel Orifice Pressure Drop, psi at 10.5 lb/sec and 53.17 lb/cu ft	167.3	----	----
Orifice Diameter, inch	139.9	----	----
LOX Orifice Pressure Drop, psi at 3.5 lb/sec and 71.38 lb/cu ft	86.3	---	----
Orifice Diameter, inch	75.9	14.5	1.3
Verniers (Pump-Fed)			
LOX Flow, lb/sec	6.56	0.054	0.019
Fuel Flow, lb/sec	3.61	0.035	0.011
Vernier Total Flow, lb/sec	10.17	0.070	0.026
Mixture Ratio (o/f)	1.82	0.019	0.006
LOX Customer Connect Pressure, psia	762.	9.0	3.3
Fuel Customer Connect Pressure, psia	701.	7.9	2.6
Heat Exchanger LOX Flow, lb/sec	3.17	0.045	0.046

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TABLE 5  
(Continued)

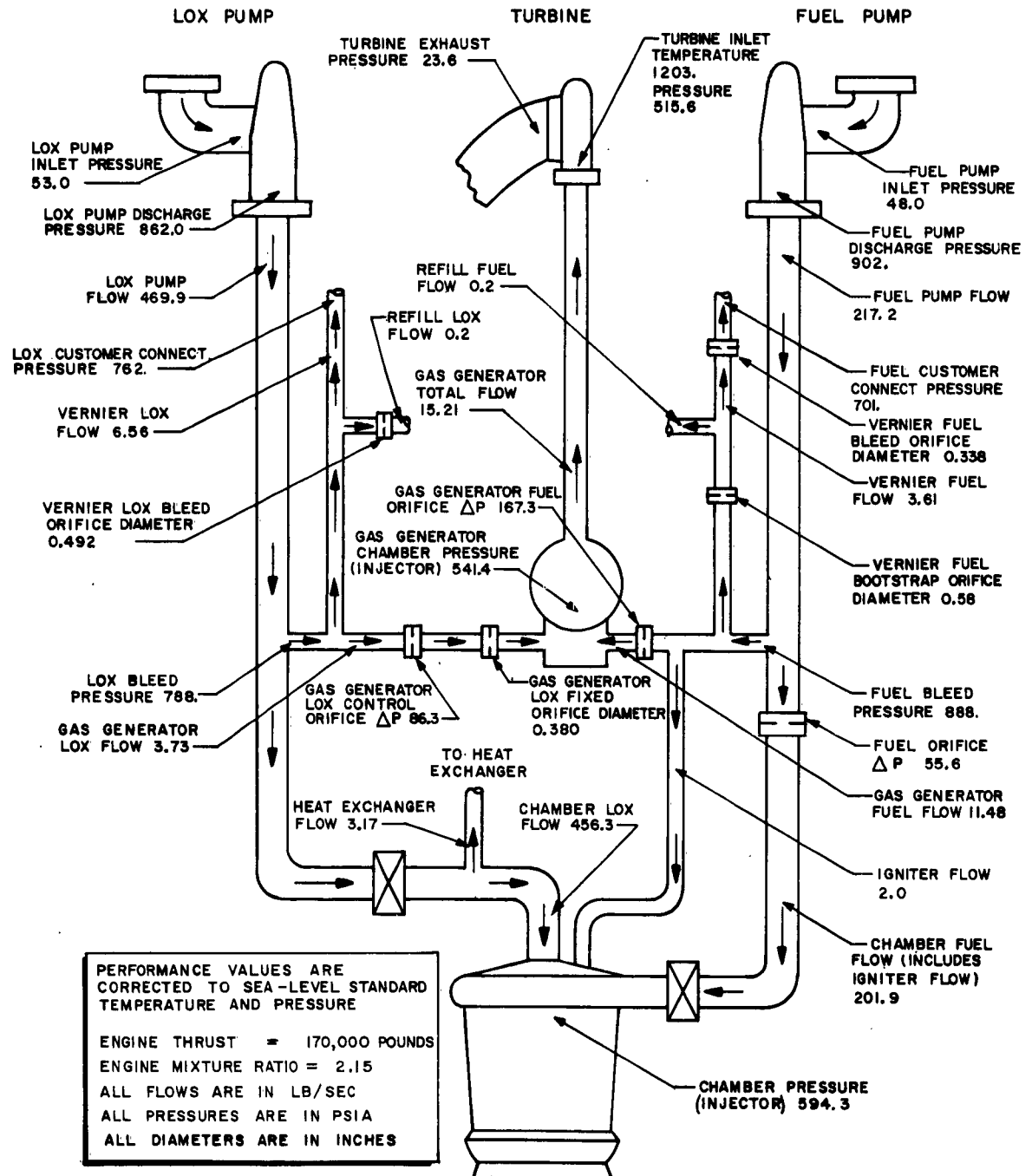
Parameter	Nominal Value	Standard Deviation	
		Engine-to-Engine (S <sub>EE</sub> )	Run-to-Run (S <sub>RR</sub> )
Verniers (Solo)			
LOX Flow, lb/sec	5.38	0.028	0.014
Fuel Flow, lb/sec	3.01	0.018	0.006
Vernier Total Flow, lb/sec	8.39	0.046	0.020
Mixture Ratio (o/f)	1.78	0.007	0.006
LOX Customer Connect Pressure, psia	575.	4.40	2.1
Fuel Customer Connect Pressure, psia	530.	4.20	1.20
Engine Regulator Pressure Setting, psia	660.	----	----

NOTE: All pressures were measured with a static tap, unless designated as total. Pressure designated as total were calculated from a static measurement.

\* Rated value

\*\*Calculated from turbine inlet temperature and pressure





**Figure 6. Main Engine Performance Schematic**

TABLE 6

**PERFORMANCE DEVIATIONS, YLR79-NA-13 THOR MAIN ENGINES**  
(Data Based on 47 Runs Involving 23 Engines)

Parameter	Specified or Mean Value	Deviation, %
<u>Engine Thrust</u>		
Specified, pounds	170,000. $\pm 3\%$	
Run-to-Run Deviation*		0.25
Run-to-Run, 95% Tolerance		0.61
<u>Mixture Ratio</u>		
Specified	2.15 $\pm 1.02\%$	
Run-to-Run Deviation*		0.23
Run-to-Run, 95% Tolerance		0.56
<u>Specific Impulse**</u>		
Specified Minimum, seconds	249.	
Mean	252.4	
Run-to-Run Deviation*		0.12
Run-to-Run, 95% Tolerance		0.29
Engine-to-Engine Deviation		0.25
Engine-to-Engine, 95% Tolerance		0.61
Over-all Standard Deviation***		0.27
Over-all, 95% Tolerance		0.63

\* Run-to-run standard deviation

\*\* Specific impulse values are quoted at rated thrust and mixture ratio

\*\*\* Run-to-run and engine-to-engine standard deviation. This method of combination allows a conservative estimation.

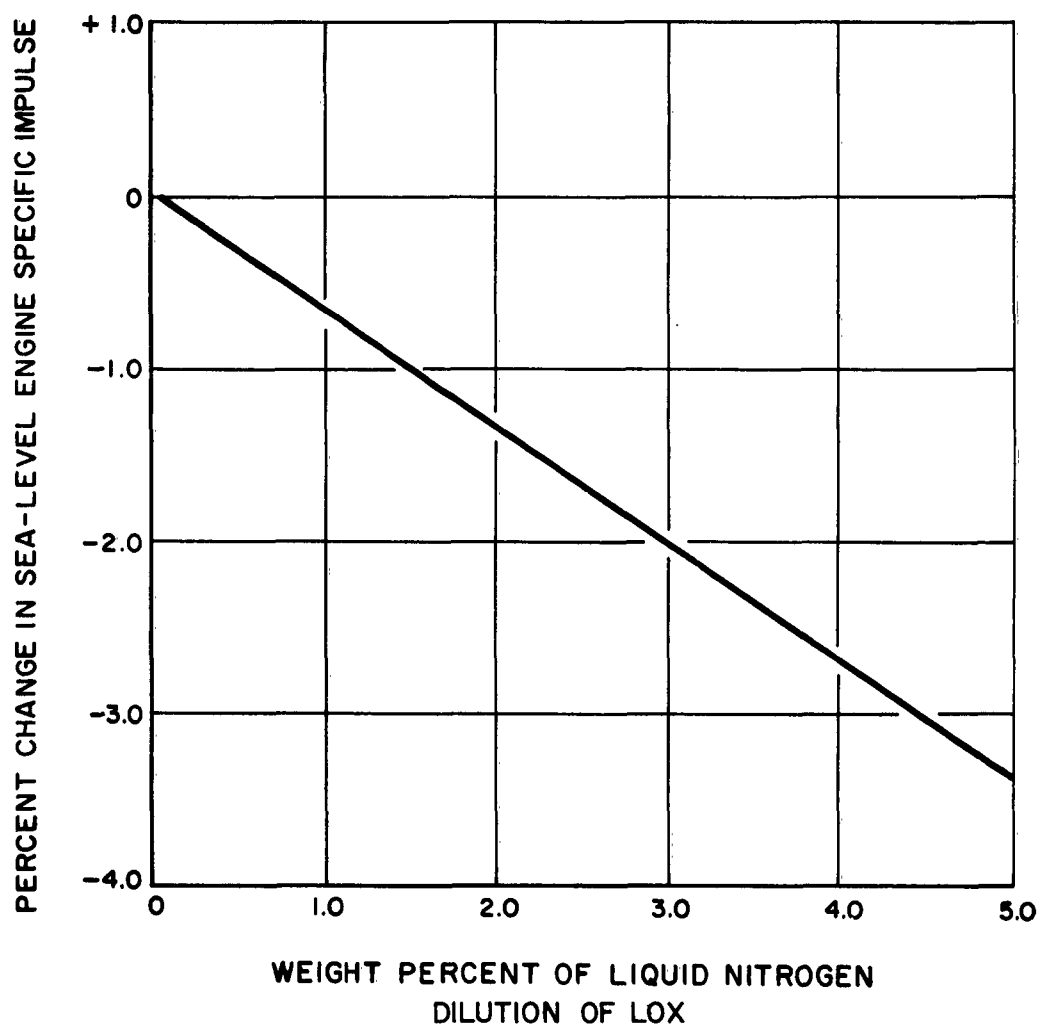


Figure 7. Effects of Liquid Nitrogen Dilution on Sea Level Engine Specific Impulse

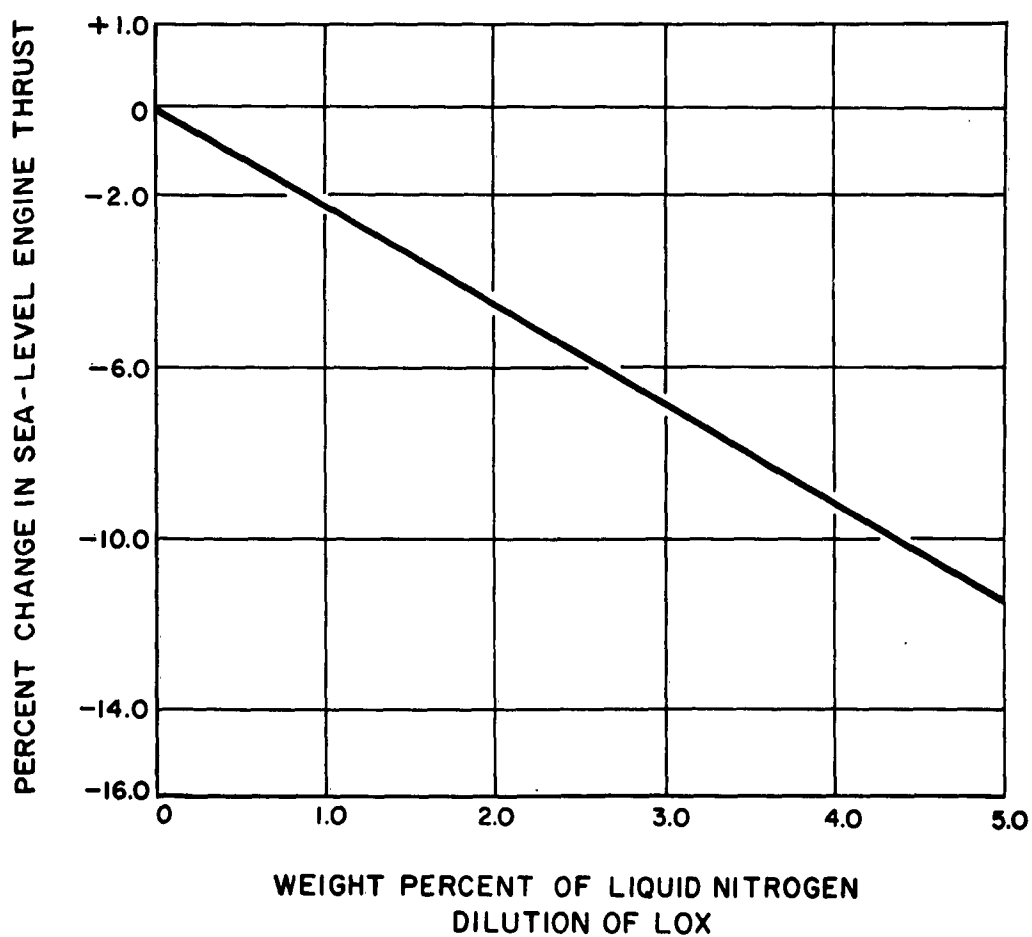


Figure 8. Effects of Liquid Nitrogen Dilution on Sea-Level Engine Thrust

### RATED VERNIER ENGINE PERFORMANCE

Statistical analyses of LR101-NA-11 vernier engine data are presented in Table 7, covering mean performance, run-to-run, and engine-to-engine variations. The data are based on 94 tests on 47 acceptance engines. RP-1 was used for all tests. Data were reduced to sea-level standard temperature and pressure rated thrust, mixture ratio, and propellant inlet pressures prior to statistical analysis. The data reduction program computes orifices required to give rated thrust and mixture ratio at tank-fed conditions. With these orifices, the program then computes what thrust and mixture ratio would be under pump-fed conditions.

The following standard conditions are used by the data reduction program:

<u>Rated Parameter</u>	<u>Tank-Fed</u>	<u>Pump-Fed</u>
Thrust, pounds	830	---
Mixture Ratio	1.80	---
LOX Inlet Pressure, psia	540	660
Fuel Inlet Pressure, psia	510	636
LOX Specific Gravity, lb/cu ft	66.27	70.73
Fuel Specific Gravity, lb/cu ft	50.48	50.48

A schematic of vernier operation under pump-fed conditions (with RJ-1 fuel) appears in Fig. 9.

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TABLE 7

NOMINAL LR101-NA-11 VERNIER ENGINE PERFORMANCE  
AND PERFORMANCE DEVIATIONS

Parameter	Mean Value	S <sub>EE</sub>	C <sub>VEE</sub>	S <sub>RR</sub>	C <sub>VRR</sub>
<u>Tank-Fed</u>					
Specific Impulse, seconds	198.7	1.92	0.97	1.12	0.56
Characteristic Velocity (c*), Injector End, ft/sec	4942	69.9	1.41	29.1	0.59
Thrust Coefficient (C <sub>F</sub> ), Injector End	1.294	0.007	0.55	0.005	0.35
Chamber Pressure, Injector End, psia	305.4	2.64	0.86	0.85	0.28
Chamber Pressure, Nozzle, psia	298.	--	--	--	--
LOX Weight Flow, lb/sec	2.68	--	--	--	--
Fuel Weight Flow, lb/sec	1.49	--	--	--	--
LOX Orifice Differential Pressure, psi	39.8	7.96	20.0	2.97	7.44
Fuel Orifice Differential Pressure, psi	27.6	7.68	27.8	3.33	12.05
<u>Pump-Fed</u>					
Thrust, pounds	1017	5.64	0.55	4.19	0.41
Mixture Ratio	1.803	0.010	0.54	0.011	0.61
Specific Impulse, seconds	209.8	2.21	1.05	0.83	0.39
c*, Injector End, ft/sec	5054.	51.5	1.02	21.0	0.42
C <sub>F</sub> , Injector End	1.336	0.005	0.39	0.005	0.37

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TABLE 7  
(Continued)

Parameter	Mean Value	S <sub>EE</sub>	C <sub>VEE</sub>	S <sub>RR</sub>	C <sub>VRR</sub>
Chamber Pressure, Injector End, psia	362.5	3.39	0.93	1.70	0.47
Chamber Pressure, Nozzle, psia	353.	- -	- -	- -	- -
LOX Weight Flow, lb/sec	3.12	- -	- -	- -	- -
Fuel Weight Flow, lb/sec	1.73	- -	- -	- -	- -

S<sub>EE</sub> Engine-to-engine standard deviation

C<sub>VEE</sub> Engine-to-engine coefficient of variation (standard deviation expressed as percentage of the mean)

S<sub>RR</sub> Run-to-run standard deviation

C<sub>VRR</sub> Engine-to-engine coefficient of variation (standard deviation expressed as percentage of the mean)

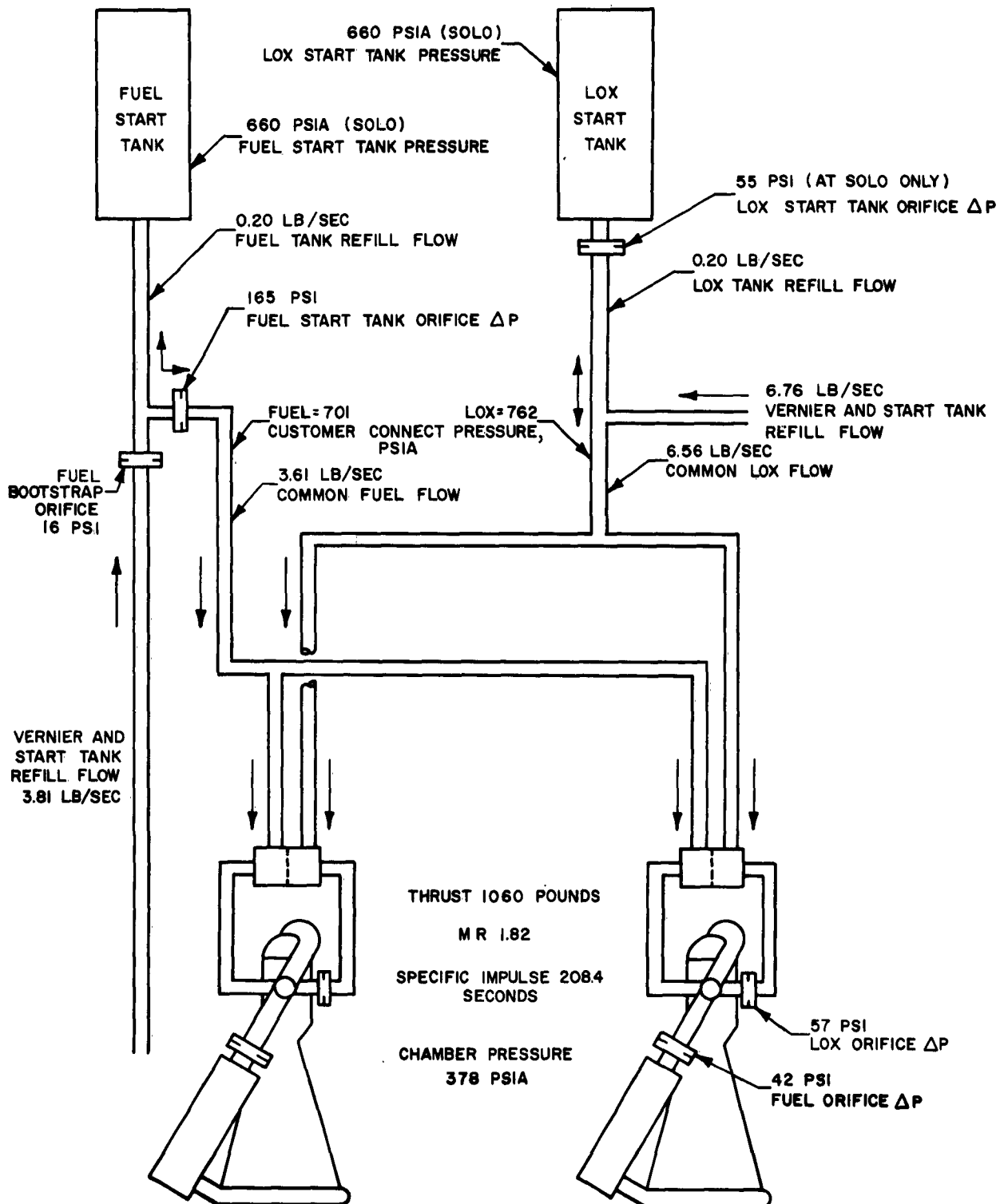


Figure 9. LR79-NA-11 Vernier Pump-Fed Performance Schematic



## INFLUENCE COEFFICIENTS

### LINEARIZED SOLUTIONS

Engine influence coefficients result from a linearized solution of a set of steady-state equations which describe the operation of an engine. Each influence coefficient is expressed in percentage form, and represents the effect that a 1% increase in an engine independent variable will have on an engine dependent variable. A coefficient preceded by a positive (+) sign (or no sign) indicates that an increase in the independent variable results in an increase in the dependent variable; a coefficient preceded by a negative (-) sign indicates that an increase in the independent variable results in a decrease in the dependent variable.

### ILLUSTRATION

Figure 10 is a portion of a typical table of engine influence coefficients. This table is in the form as printed by a high-speed digital computer. The symbols E 01, E 04, etc., placed after the nominal values in the table represent powers of 10. Hence 1.4696E 01 is equivalent to 14.696; 6.0000E 04 is equivalent to 60,000; etc.

### APPLICATION

These influence coefficients may be applied to two different situations; (1) calculations involving an engine type, or (2) calculations involving a specific engine.

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A ONE-PERCENT INCREASE IN ANY ONE OF THE INDEPENDENT VARIABLES CAUSES THE FOLLOWING PERCENTAGE CHANGE IN ANY ONE OF THE DEPENDENT VARIABLES.

-INDEPENDENT VARIABLES-

1. ATMOSPHERIC PRES - - - - -	1.4696E 01
2. FUEL DENSITY - - - - -	5.0450E 01
3. OXID DENSITY - - - - -	7.1380E 01
4. FUEL PUMP INLET PRES - - - -	7.7000E 01
5. OXID PUMP INLET PRES - - - -	5.3000E 01
6. C* CORRECTION - - - - -	-

1-            2-            3-            4-            5-            6-

-DEPENDENT VARIABLES-

ENGINE THRUST - - 6.0000E 04						
	-0.4556	0.5326	0.0703	0.0576	0	0.6494
ENGINE ISP - - - 2.3000E 02						
	-0.4426	0.1462	0.0341	0.0182	0	1.1677
ENGINE MR - - - - 2.2700E 00						
	-0.0039	-0.4054	0.3016	0.0200	0	-0.4134
ENGINE FUEL FLOW- 7.9770E 01						
	-0.0096	0.6588	-0.1688	0.0243	0	-0.2268
ENGINE OXID FLOW- 1.8110E 02						
	-0.0145	0.2674	0.1256	0.0461	0	-0.6462

Figure 10 . Sample Table of Influence Coefficients  
as Printed by High-Speed Digital Computer

### Calculations Involving an Engine Type

Suppose it were desired to determine the thrust of the engine described by the sample table of influence coefficients when operated under the following conditions:

- |                                 |                  |
|---------------------------------|------------------|
| 1. Atmospheric pressure         | = 1.40 psia      |
| 2. Fuel density                 | = 50.45 lb/cu ft |
| 3. Oxidizer density             | = 69.55 lb/cu ft |
| 4. Fuel pump inlet pressure     | = 69.30 psia     |
| 5. Oxidizer pump inlet pressure | = 59.55 psia     |

Because the influence coefficients are linear, the total effect of several influences acting simultaneously on an engine can be determined by adding the individual effects of each influence. The change in engine thrust would be

$$\begin{aligned}
 \frac{F_E - F_{E_i}}{F_{E_N}} = & \frac{P_a - P_{a_i}}{P_{a_N}} (F_{P_a}) + \frac{\rho_F - \rho_{F_i}}{\rho_{F_N}} (F_{\rho_F}) \\
 & + \frac{\rho_o - \rho_{o_i}}{\rho_{o_N}} (F_{\rho_o}) + \frac{P_F - P_{F_i}}{P_{F_N}} (F_{P_F}) \\
 & + \frac{P_o - P_{o_i}}{P_{o_N}} (F_{P_o}), \quad (1)
 \end{aligned}$$

Where  $F_E$ ,  $P_a$ ,  $\rho_F$ ,  $\rho_o$ , etc., are the actual values of these parameters for the problems considered.

$F_{E_i}$ ,  $P_{a_i}$ ,  $\rho_{F_i}$ ,  $\rho_{o_i}$ , etc., are the initial or base values of these parameters.

$F_{E_N}$ ,  $P_{a_N}$ ,  $\rho_{F_N}$ ,  $\rho_{o_N}$ , etc., are the nominal values of these parameters, listed in the table of influence coefficients.

$F_{P_a}$ ,  $F_{\rho_F}$ ,  $F_{\rho_o}$ , etc., are the influence coefficients for engine thrust found in the appropriate columns of the table of influence coefficients.

For calculations involving an engine type, the initial values would be the same as the nominal values, and  $F_{E_i} = F_{E_N}$ ,  $P_{a_i} = P_{a_N}$ ,  $\rho_{F_i} = \rho_{F_N}$ ,  $\rho_{o_i} = \rho_{o_N}$ , etc.

The calculation for the example stated above would be as follows:

$$\begin{aligned} \frac{F_E - 60,000}{60,000} &= \left( \frac{1.40 - 14.696}{14.696} \right) (-0.4556) + \left( \frac{50.45 - 50.45}{50.45} \right) (+0.5326) \\ &+ \left( \frac{69.55 - 71.38}{71.38} \right) (+0.0703) + \left( \frac{69.30 - 77.00}{77.00} \right) (+0.0576) \\ &+ \left( \frac{59.55 - 53.00}{53.00} \right) (0) \end{aligned}$$

$$\begin{aligned} \frac{F_E - 60,000}{60,000} &= -0.9047 (-0.4556) + 0(+0.5326) \\ &-0.0256 (+0.0703) - 0.1000 (+0.0576) \\ &+0.1236 (0) = +0.4046 \text{ or } +40.46\% \end{aligned}$$

Therefore:

$$F_E = +0.4046 (60,000) + 60,000$$

$$F_E = +24,276 + 60,000 = 84,276 \text{ pounds}$$

The incremental thrust change has been found to be +24,276 pounds for the conditions stated, yielding a final engine thrust of 84,276 pounds.

#### Calculations Involving a Specific Engine.

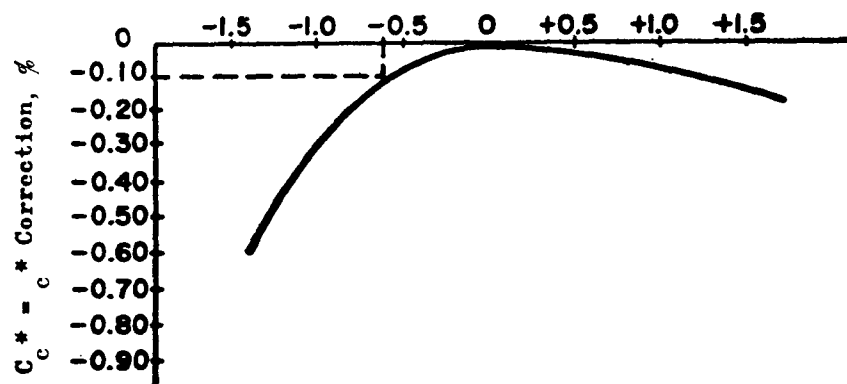
When the values of actual engine parameters differ from those used as nominal values in the table of influence coefficients, the "delta method" of application of influence coefficients is used. This procedure consists of computing an incremental change of variables rather than a percentage change of these variables. The incremental change is then applied to the actual engine value. This effect can be accomplished by using Eq. (1) if the quantities  $F_{E_i}$ ,  $P_{a_i}$ ,  $\rho_{F_i}$ ,  $\rho_{O_i}$ , etc., are defined as the actual engine values of these parameters. All other quantities are as defined previously.

#### NONLINEAR CORRECTIONS

A special computational procedure has been devised to extend the usefulness of engine influence coefficients. This technique is used to allow nonlinear corrections to be made for certain parameters where the linear approximation is not sufficiently accurate. An example of this method is the  $c^*$  correction ( $C_{c*}$ ). In this case, a plot of  $C_{c*}$  vs the change in engine mixture ratio is included with the table of influence coefficients. Similarly, other nonlinear corrections would be applied as additional terms in the summation of effects.

A typical plot of these parameters is shown below:

$$\left( \frac{\mu_E - \mu_{EN}}{\mu_{EN}} \right) 100 = \left( \frac{\text{Change in Engine Mixture Ratio}}{\text{Nominal Engine Mixture Ratio}} \right) 100\%$$



The change in engine mixture ratio is computed for the changes in atmospheric pressure, propellant densities, etc., and with the assumption that the  $c^*$  correction is zero. With this change in engine mixture ratio, the  $c^*$  correction is read from the curve. This value of  $c^*$  correction is used with the other independent variables to compute the changes in the remaining dependent variables.

For example, if the change in engine mixture ratio accompanying the +40.46% thrust change in the preceding example were -0.62%, then the  $c^*$  correction from the curve is -0.10%. The true change in engine thrust is therefore:

$$(\% \text{ change in } F_E = +40.46 - 0.10 (+0.6494) = +40.40\%)$$

Similarly, other nonlinear corrections would be applied as additional terms in the summation of effects.

#### LV-2A INFLUENCE COEFFICIENTS

Current influence coefficients for the LV-2A propulsion system are presented in Tables 8 and 9. Table 8 includes the additional effect of fuel temperature on system performance while considering fuel density a constant. Any density change, therefore, is considered independently.

The effects of engine mixture ratio on  $c^*$  in terms of a correction appear in Fig. 11.

TABLE 8

INFLUENCE COEFFICIENTS FOR THE YLR79-N/  
AND LR101-NA-11 VERNIER ENGINE

A 1% increase in any one of the independent variables  
following percentage change in any one

		<u>Independent Variables</u>	
		1. Atmospheric Pressure, psia	14.696
		2. Fuel Density, lb/cu ft	53.170
		3. Oxidizer Density, lb/cu ft	71.380
		4. Fuel Pump Inlet Pressure, psia	48.000
<u>Dependent Variables</u>		<u>Nominal Values</u>	<u>1</u>
Engine Thrust Without Verniers, pounds		170,000.	-0.1472
Engine Specific Impulse Without Verniers, seconds		252.26	-0.1404
Engine Mixture Ratio With Verniers		2.1500	-0.0001
Engine Fuel Flow With Verniers, lb/sec		217.13	-0.0067
Engine Oxidizer Flow With Verniers, lb/sec		466.83	-0.0068
Vernier Oxidizer Flow, lb/sec		6.4860	-0.0056
Vernier Fuel Flow, lb/sec		3.5637	-0.0058
Vernier Thrust, pounds		2112.0	-0.1702
Thrust Chamber Nozzle Stagnation Pressure, psia		551.53	-0.0069
Fuel Pump Outlet Pressure, psia		901.35	-0.0091
Oxidizer Pump Outlet Pressure, psia		861.27	-0.0089
Pump Speed, rpm		6260.8	-0.0051





TABLE 8

FOR THE YLR79-NA-13 THOR MAIN ENGINE  
11 VERNIER ENGINES (PUMP-FED)

by one of the independent variables causes the  
change in any one of the dependent variables

Independent Variables

14.696	5. Oxidizer Pump Inlet Pressure, psia	53.000
53.170	6. c* Correction	1.0000
71.380	7. Fuel Temperature (at constant density), F	60.000
48.000		

ial ies	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>	<u>7</u>
000.	-0.1472	-0.6862	1.8030	-0.0178	0.0685	1.0844	-0.0039
06	-0.1404	-0.0736	0.2228	-0.0017	0.0085	1.1346	-0.0001
00	-0.0001	-1.6245	1.6197	-0.0533	0.0614	-0.0374	-0.0256
03	-0.0067	0.5003	0.4707	0.0204	0.0179	-0.0178	0.0138
03	-0.0068	-1.1242	2.0903	-0.0329	0.0794	-0.0552	-0.0119
00	-0.0056	-0.7031	1.6793	-0.0193	0.0563	0.4534	-0.0060
07	-0.0058	0.3569	0.6199	0.0085	0.0256	0.3638	0.0076
00	-0.1702	-0.6315	1.7772	-0.0176	0.0604	0.5157	-0.0046
03	-0.0069	-0.5675	1.5463	-0.0145	0.0588	0.9510	-0.0029
05	-0.0091	-0.3755	1.3415	0.0044	0.0509	0.5976	0.0077
07	-0.0089	-1.0884	2.0517	-0.0304	0.0897	0.6184	-0.0093
08	-0.0051	-0.6687	0.6730	-0.0189	0.0256	0.2659	-0.0061



TABLE 9

INFLUENCE COEFFICIENTS FOR THE IR101-NA-11 VERNIER ENGINE OPERATING AT SOLO CONDITIONS

A 1% increase in any one of the independent variables causes the following percentage change in any one of the dependent variables.

		<u>Independent Variables</u>			
		<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>
		<u>Nominal Values</u>			
<u>Dependent Variables</u>					
1. Atmospheric Pressure, psia	14.696	4. Fuel Propellant Supply Pressure, psia	510.00		
2. Fuel Density, lb/cu ft	50.480	5. Oxidizer Propellant Supply Pressure, psia	540.00		
3. Oxidizer Density, lb/cu ft	66.270				
Vernier Thrust, pounds	830.00	-0.2082	0.0358	0.3285	0.7599
Vernier Specific Impulse, seconds	198.27	-0.2082	-0.1051	0.1767	-0.2635
Vernier Mixture Ratio	1.8000	0.	-0.4947	0.5237	-1.2400
Vernier Fuel Flow, lb/sec	1.4951	0.	0.4589	-0.1848	1.1503
Vernier Oxidizer Flow, lb/sec	2.6912	0.	-0.0358	0.3389	-0.4275
					0.7839

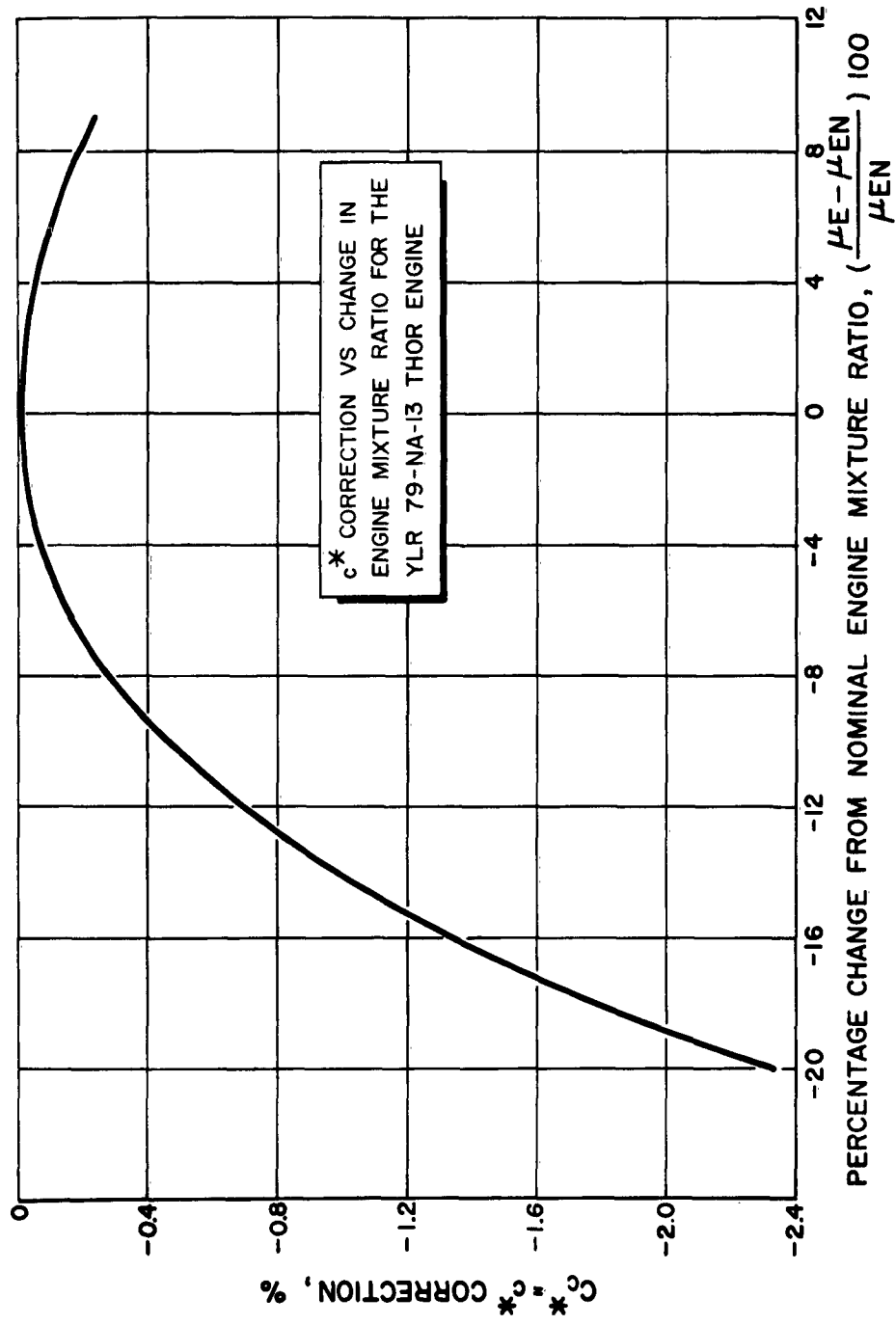


Figure 11. c\* Correction vs Change in Engine Mixture Ratio for the YLR79-NA-13 Thor Main Engine

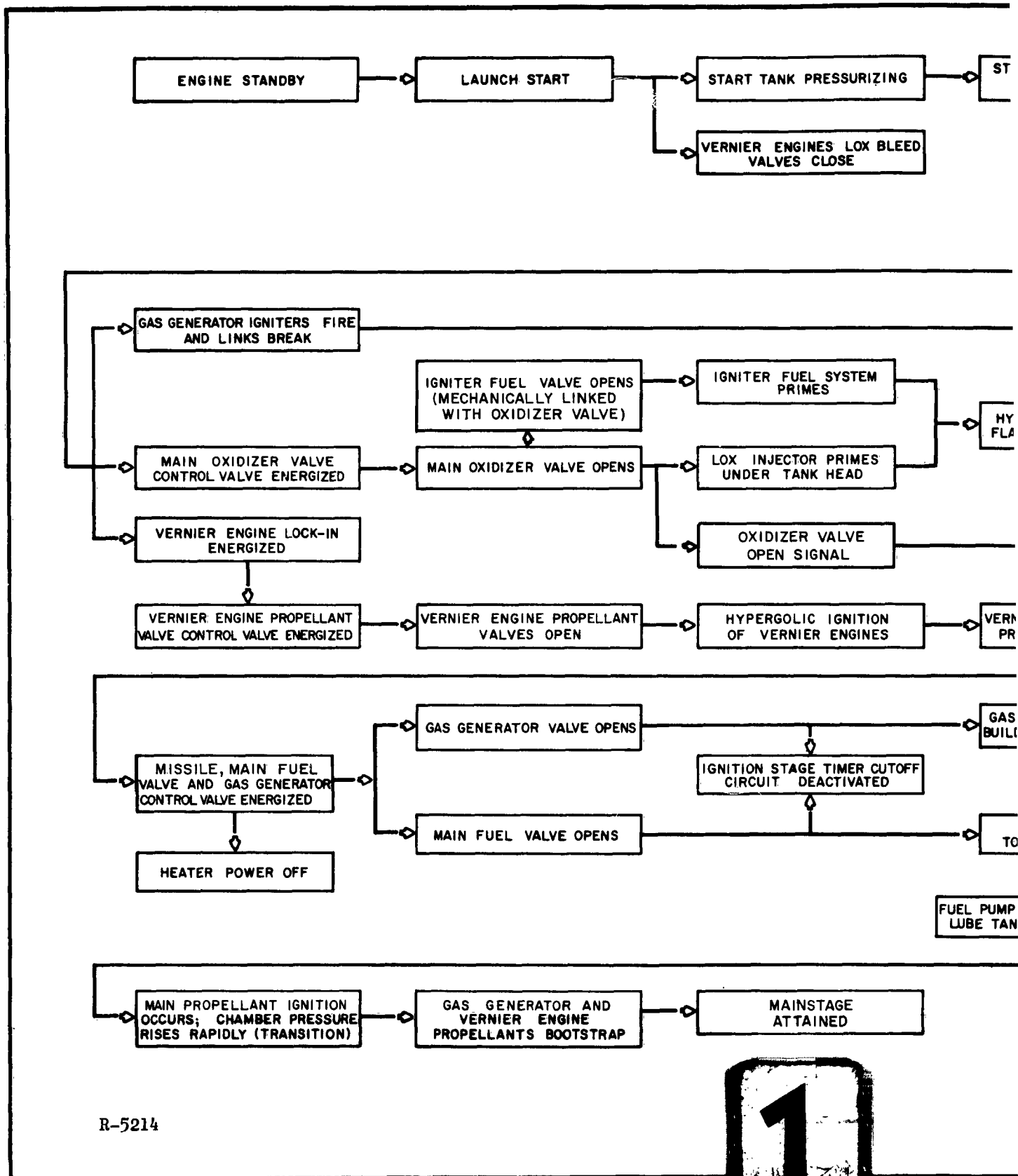
### TRANSIENT CHARACTERISTICS

The following portion of this report is devoted to a detailed description of YLR79-NA-13 main engine and LR101-NA-11 vernier engines transient operating characteristics during starting, stabilization, and cutoff. Considered are electromechanical sequencing, engine systems major flows and pressures, and start tanks refill operation. It should be noted that all relationships are typical of static firing operation but are considered good approximations of missile launching conditions as well. Data from simulated missile starts were used where available.

## START AND CUTOFF SEQUENCE

The YLR79-NA-13 main engine and LR101-NA-11 vernier engines are electrically sequenced for appropriate start and cutoff operation. All valves are pneumatically operated with a 660 psia regulated gaseous nitrogen supply. Pneumatic restrictors (orifices) are used in conjunction with the valves to provide desired actuation delay and movement times.

Figures 12 and 13 schematically represent electromechanical start and cutoff sequence requirements. Figure 14 displays the average time function of the sequence of events during start and cutoff.



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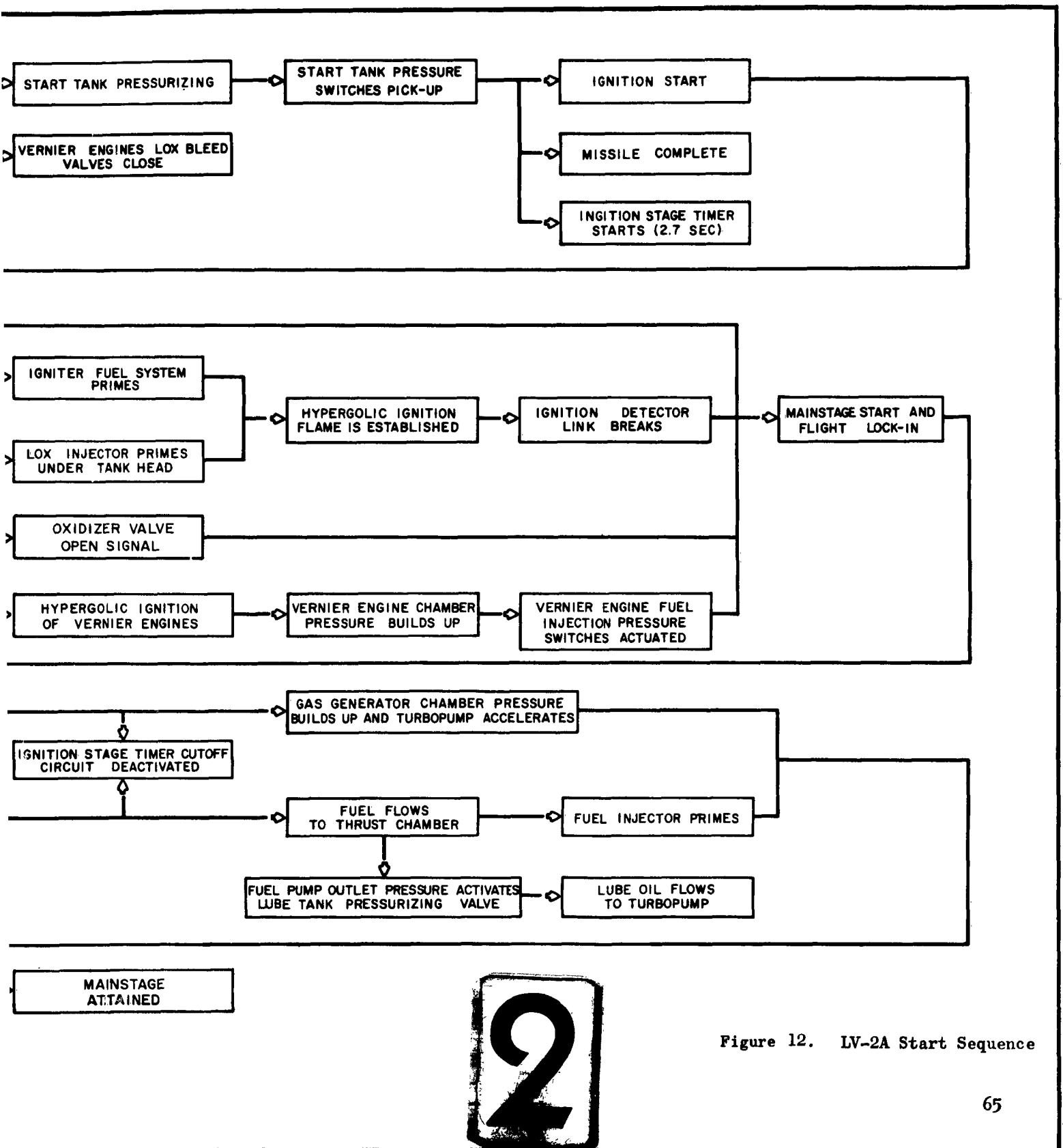


Figure 12. LV-2A Start Sequence

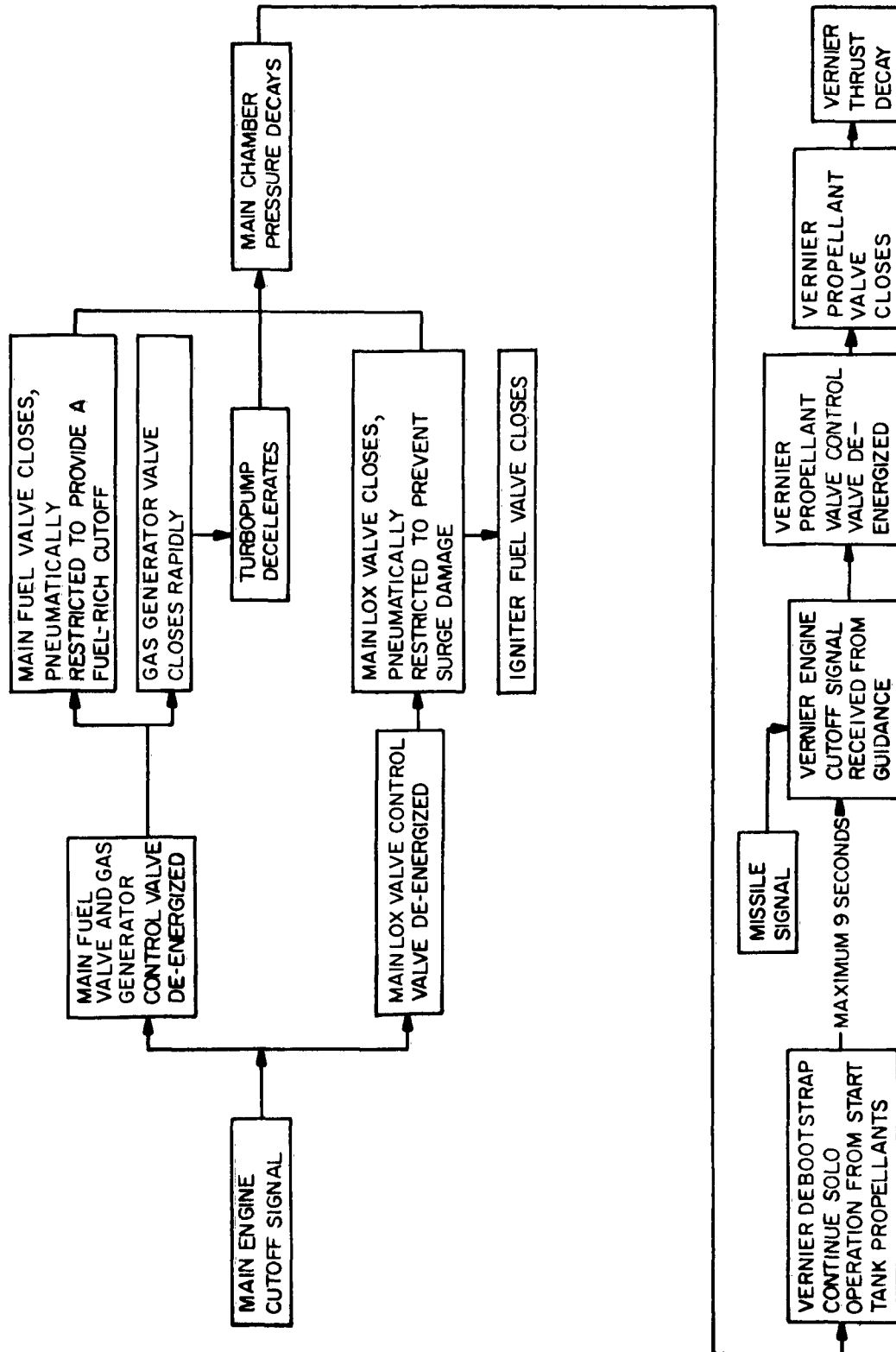


Figure 13. LV-2A Cutoff Sequence



# START SEQUENCE

△ LAUNCH START

△ START TANKS PRESSURIZED

△ IGNITION START

■ MAIN LOX VALVE IGNITION AND FUEL VALVE OPEN

■ VERNIER ENGINE PROPELLANT VALVES OPEN, HYPER

△ GAS GENERATOR IGNITERS FIRE

△ MAIN CHAMBER HYPERGOLIC IGNITION OCCURS

△ GAS GENERATOR LINKS BREAK

△ IGNITION DETECTOR LINK BRE

△ VERNIER ENGINES FUEL

△ MAINSTAGE START

■ GAS GENERATOR B

MAIN

# CUTOFF SEQUENCE

△ MAIN ENGINE CUTOFF SIGNAL

■ GAS GENERATOR BLADE VALVE CLOSES

■ MAIN LOX VALVE CLOSES

■ MAIN FUEL VALVE CLOSES

△ 90% CHAMBER PRESSURE

0 0.2 0.4 0.6 0.8 1.0 1.2 1.4 1.6

TIME, SECOND



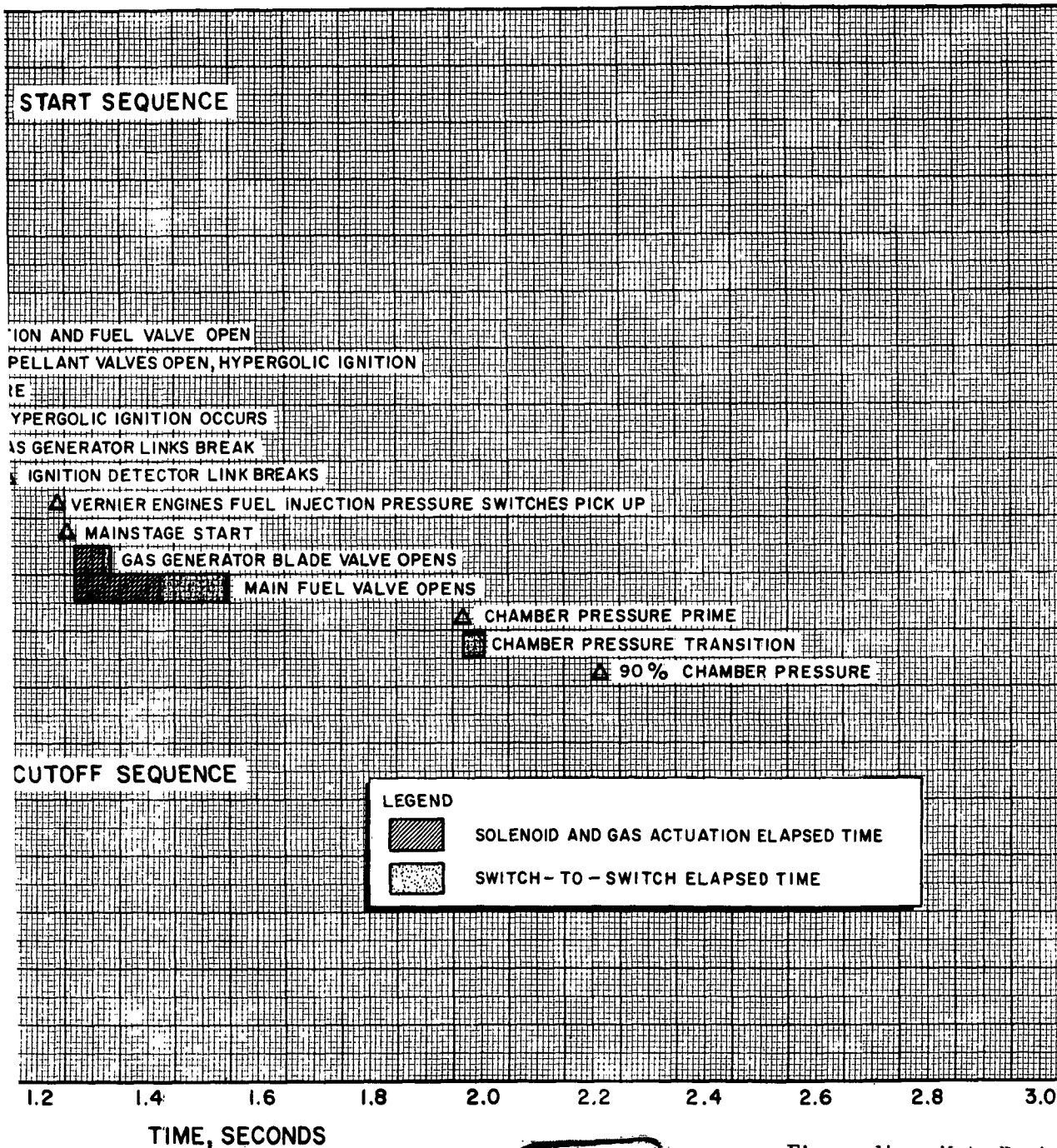


Figure 14. Main Engine Electromechanical Start and Cutoff Time Sequence



#### START AND CUTOFF TRANSIENT CHARACTERISTICS

The YLR79-NA-13 main engine and LR101-NA-11 vernier engines are ignited by pyrophoric cartridges with an integrated start-vernier solo tank system. Main chamber ignition flame is established by LOX supplied to the injector under tank head, along with start-tank-supplied igniter fuel to spray disks located in each of the six baffled compartments. No chamber fuel jacket prefill is used. Gas generator ignitors are pyrotechnic.

Figures 15 through 17 portray typical start characteristics (primarily propellant flows) of the pump main chamber, and auxilliary systems. Figures 18 and 19 are typical oscillographic recordings (primarily pressures) of an engine start and cutoff, respectively. Vernier engines were simulated during this test. Estimated prelaunch propellant consumption (ignition start to 90% chamber pressure) and start tank refill operation are presented in Tables 10 and 11.

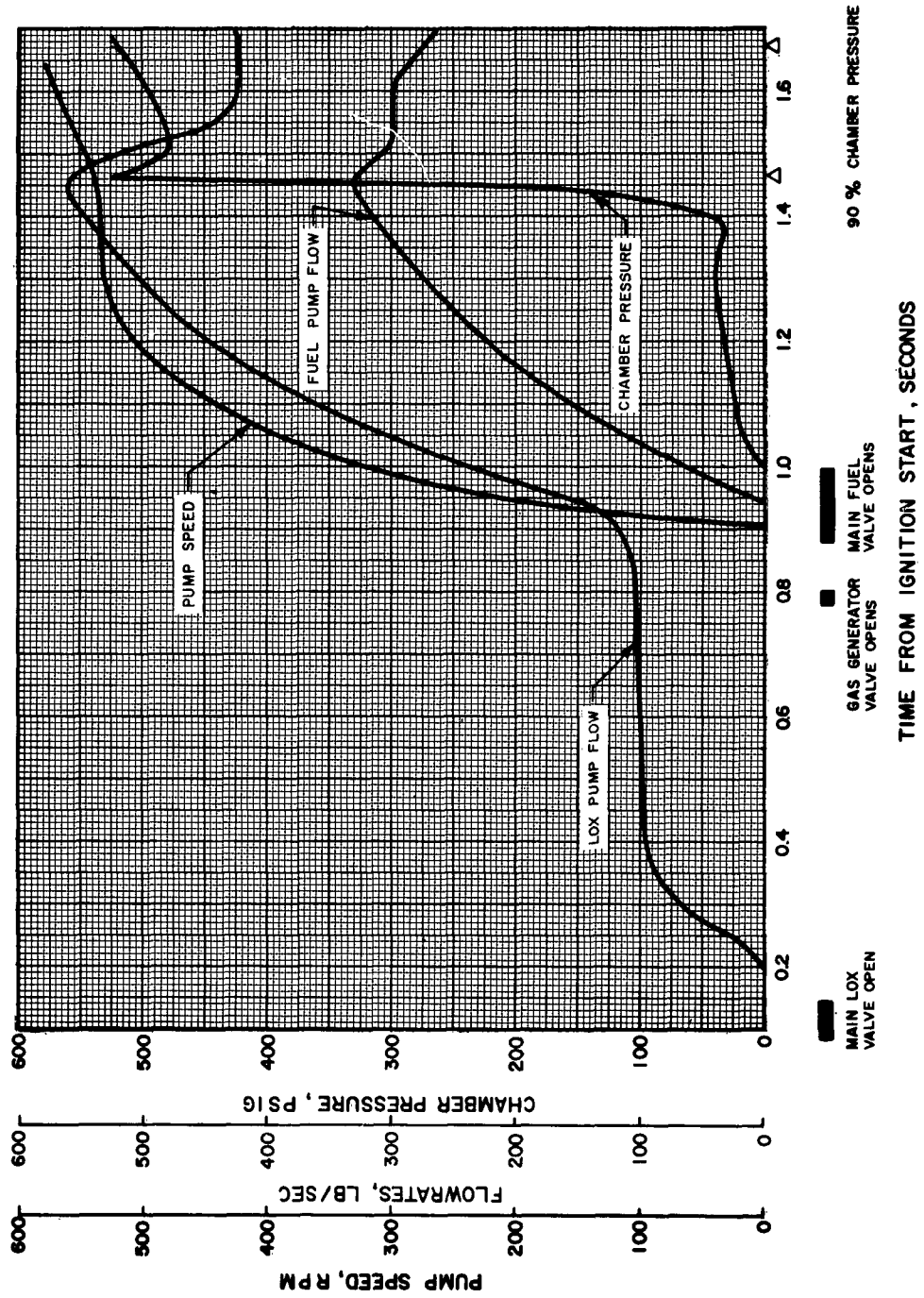
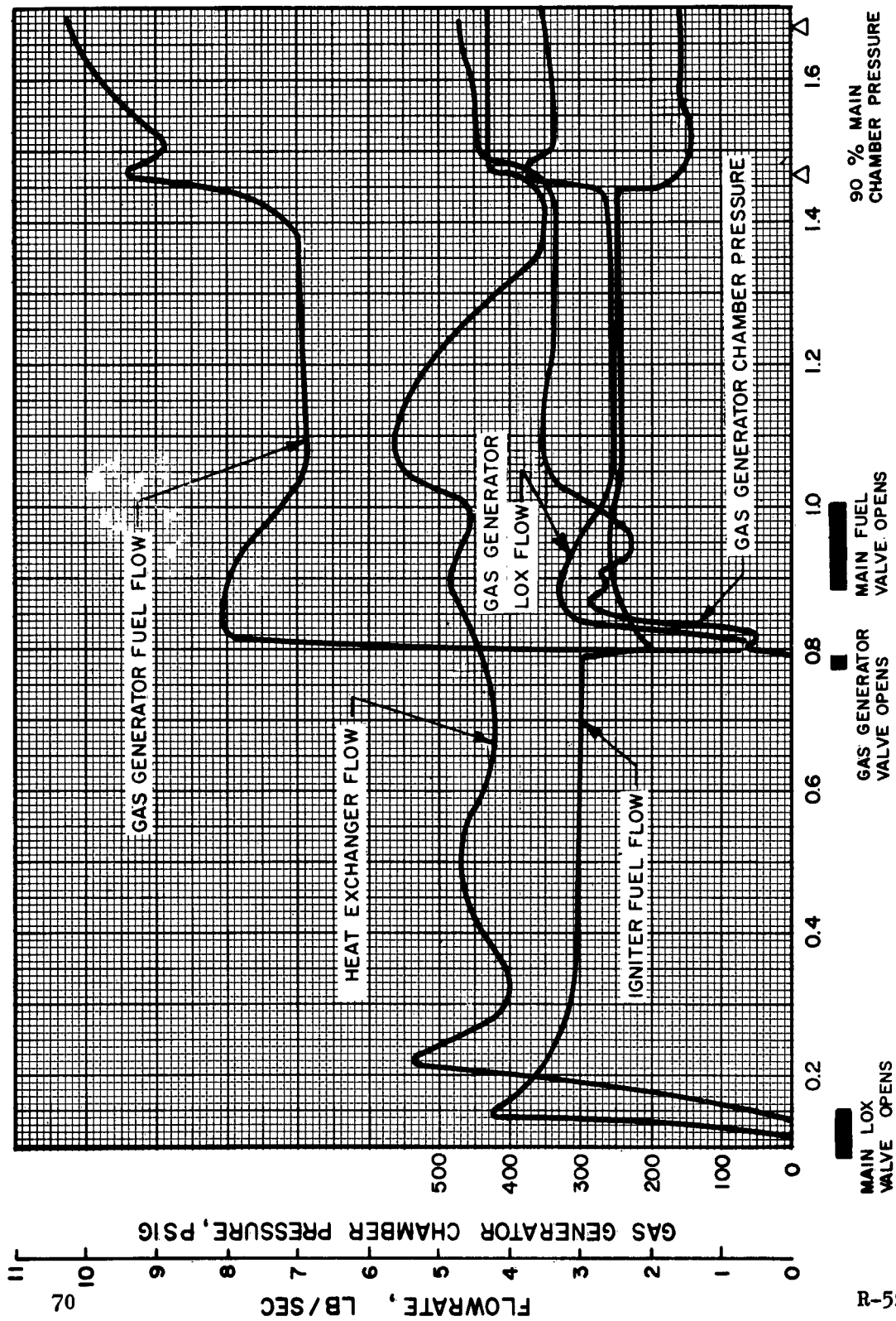


Figure 15. Main Engine System Start Characteristics



TIME FROM IGNITION START, SECONDS

Figure 16. Gas Generator and Auxiliary Flows Start Characteristics

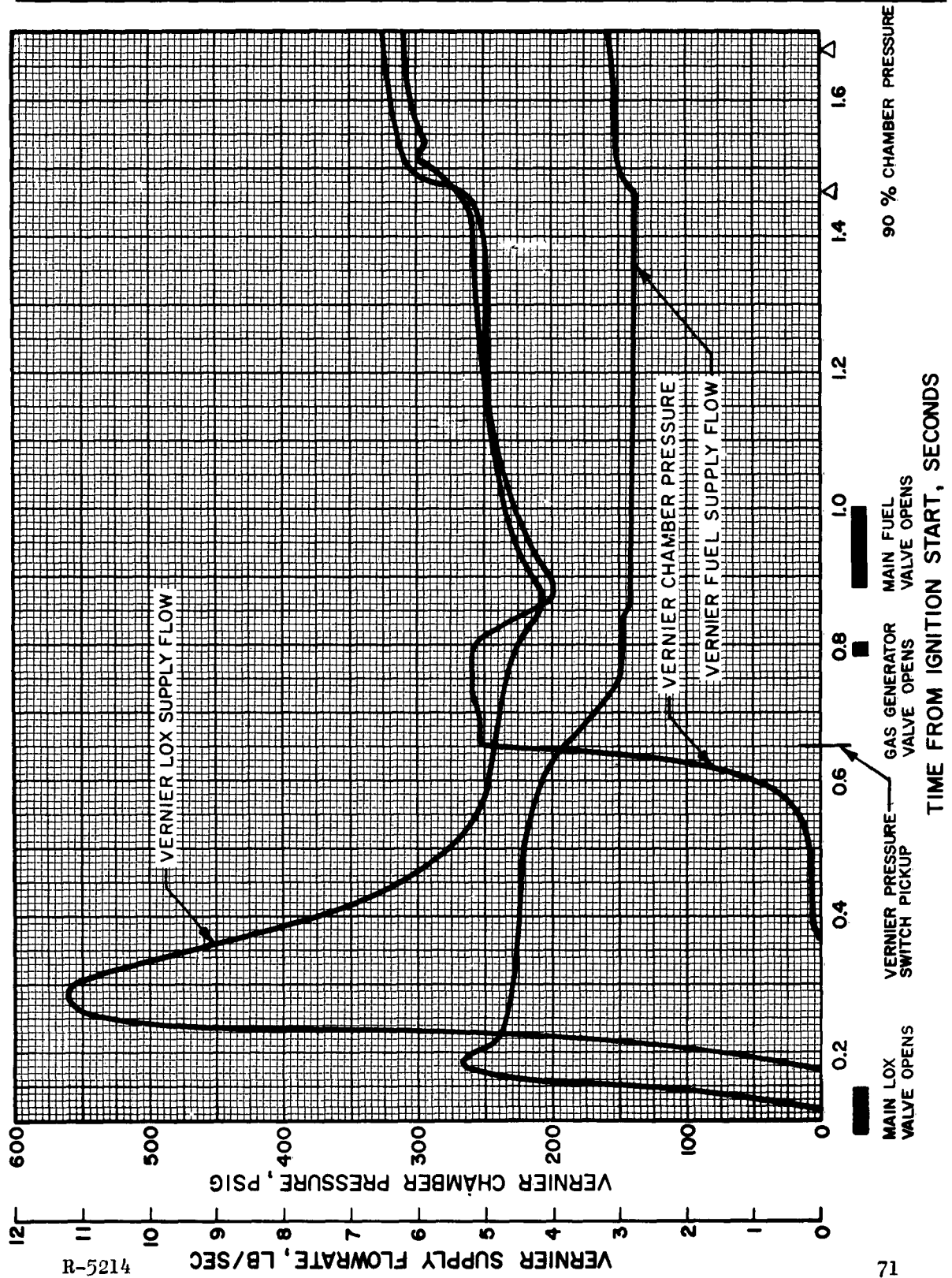
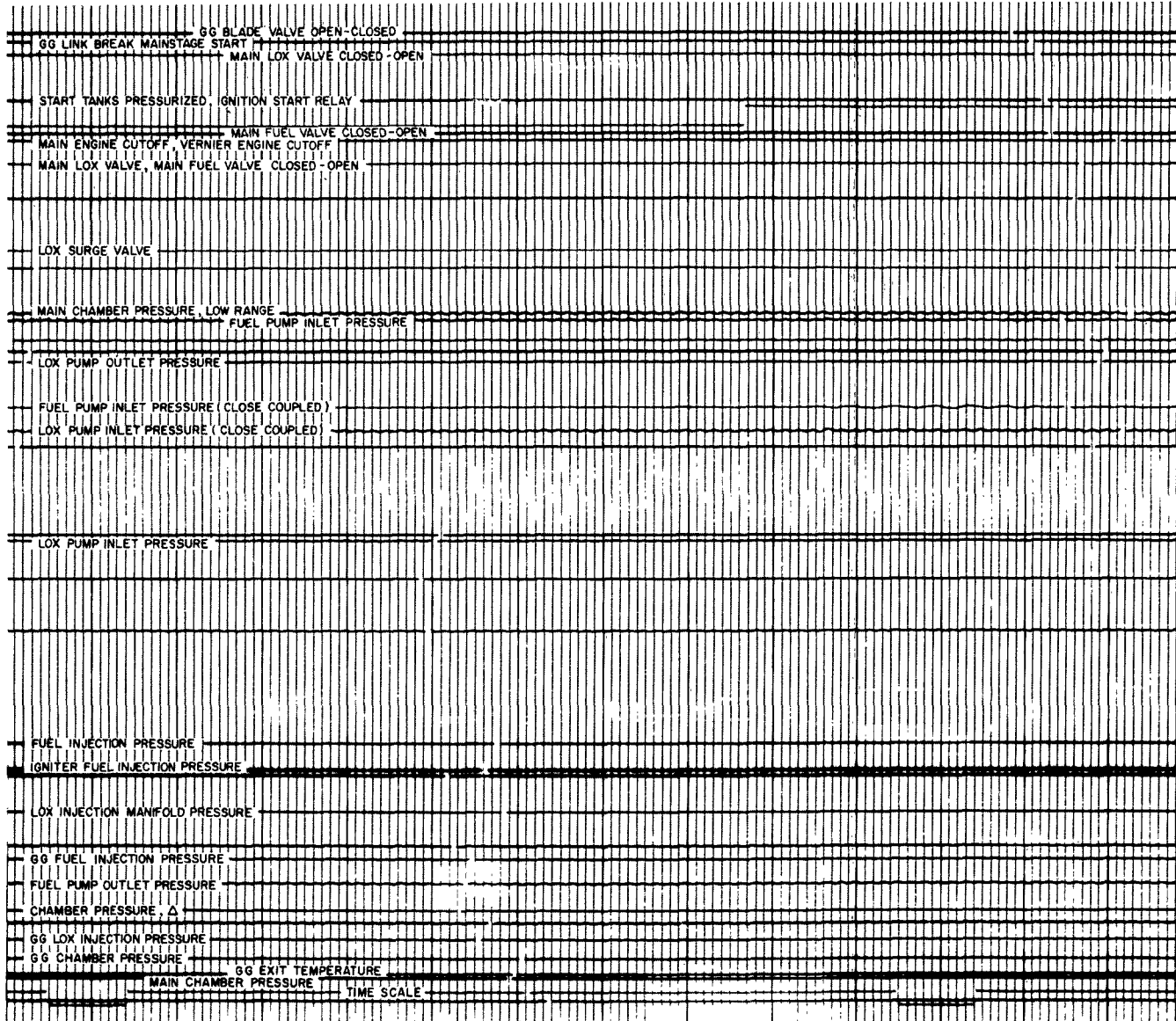
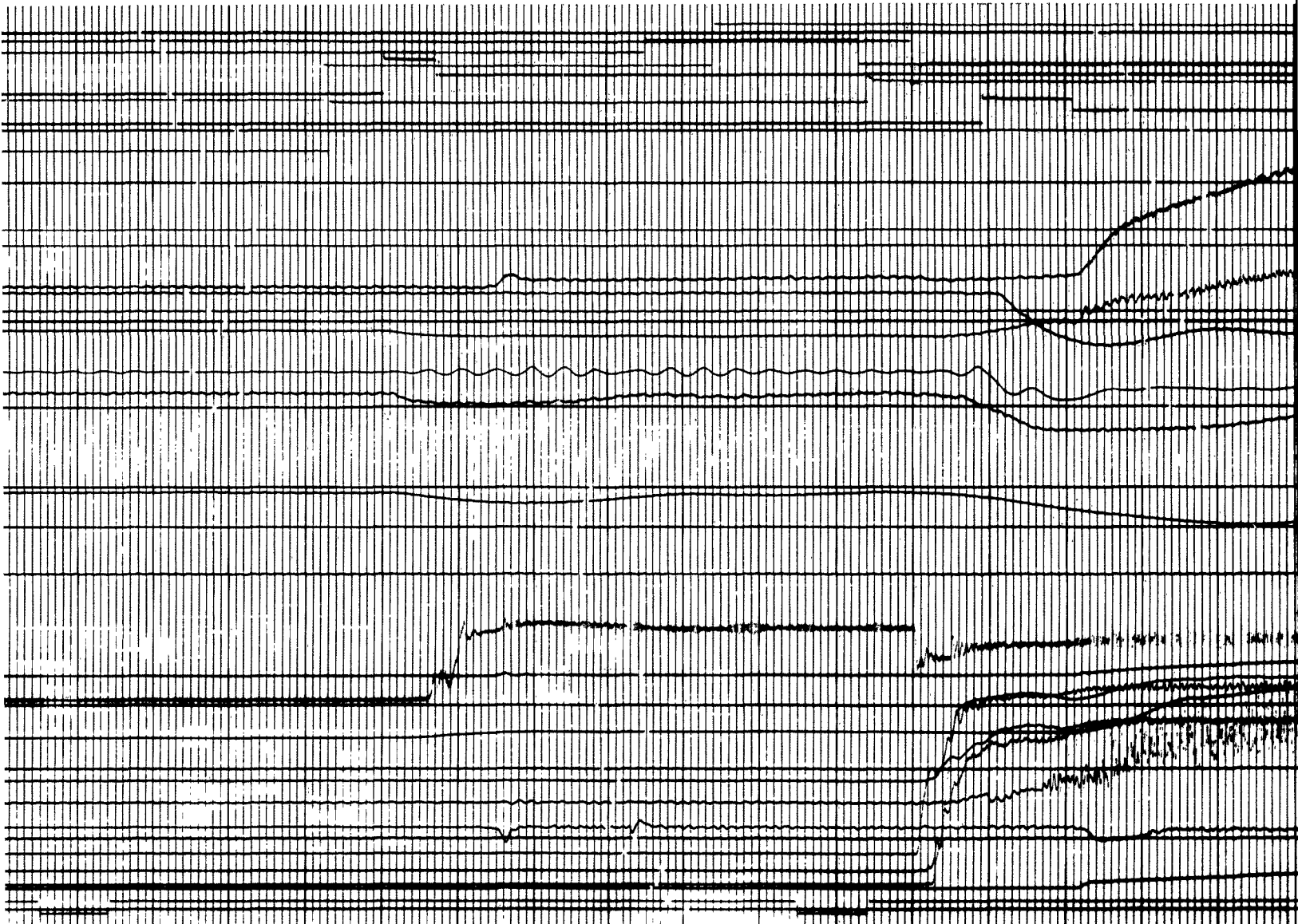


Figure 17. Vernier System Start Characteristics

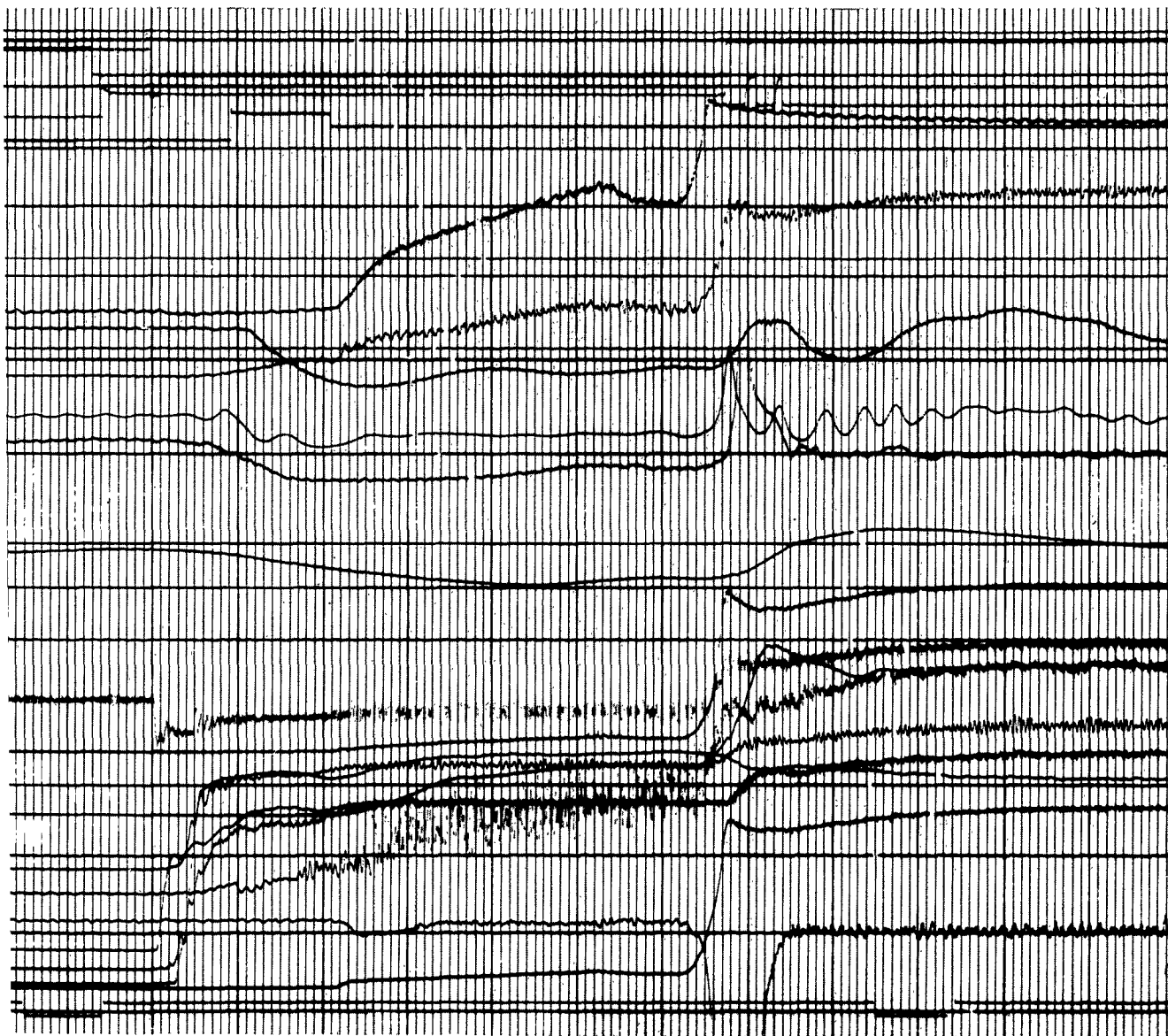






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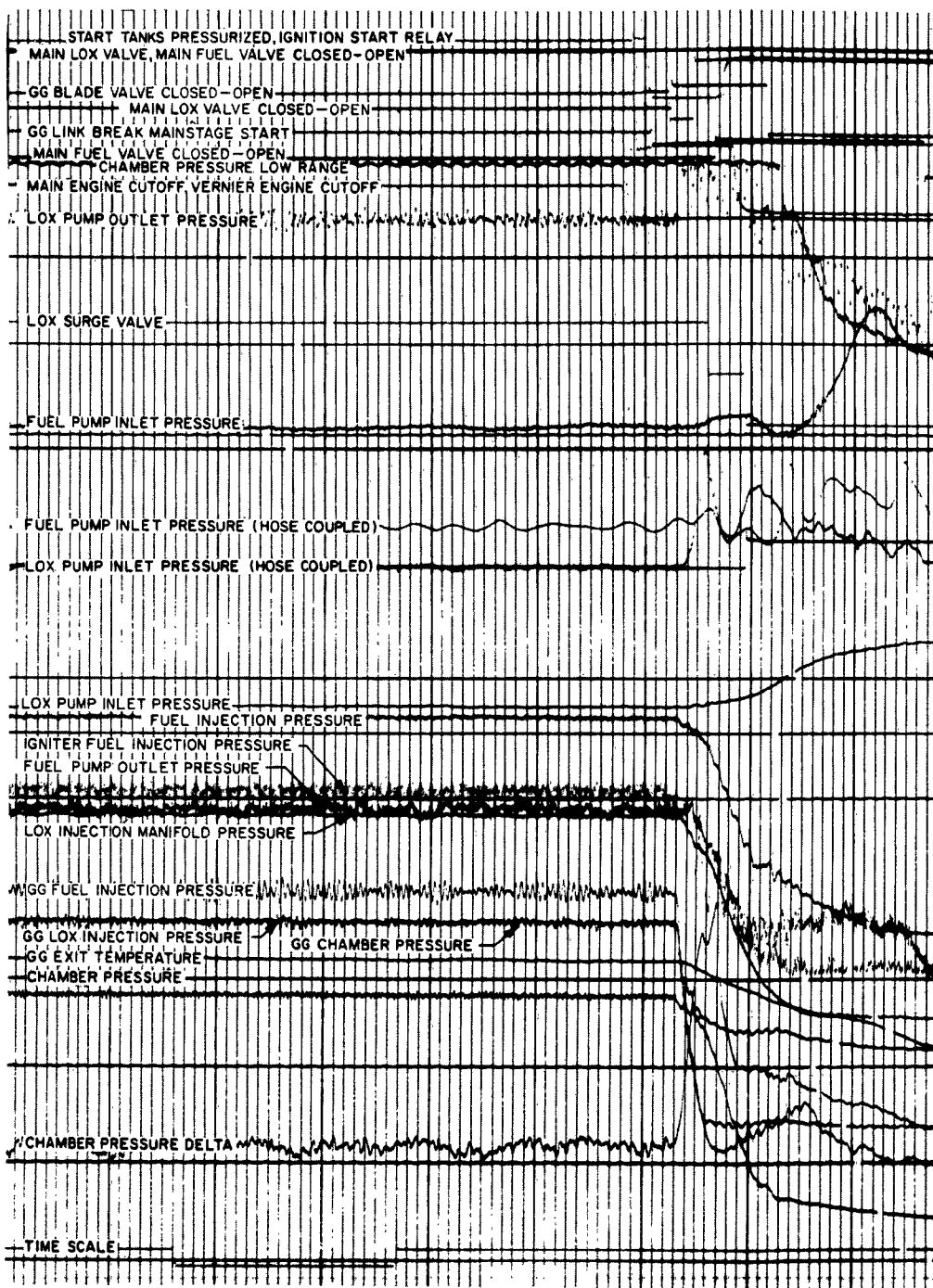


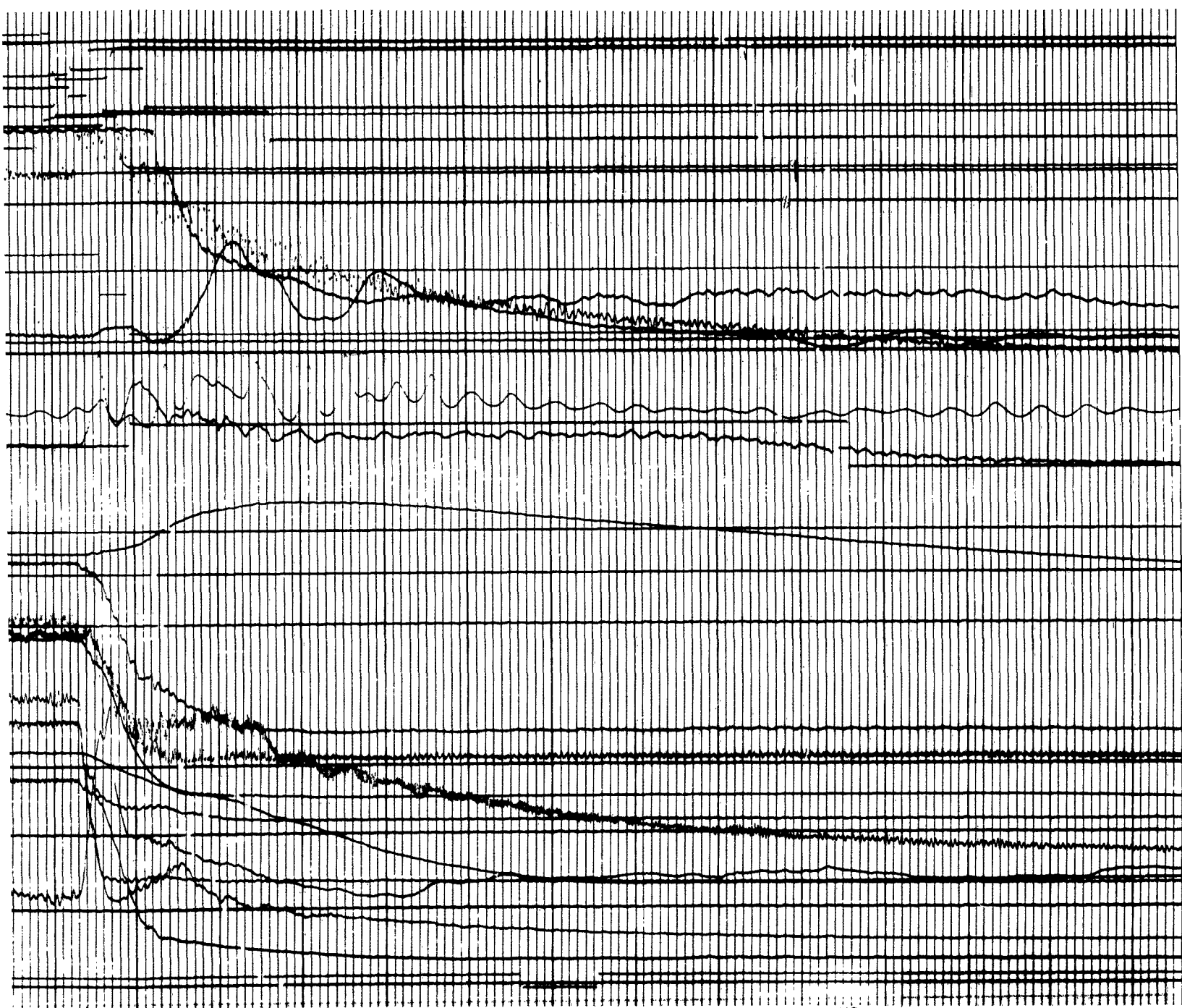


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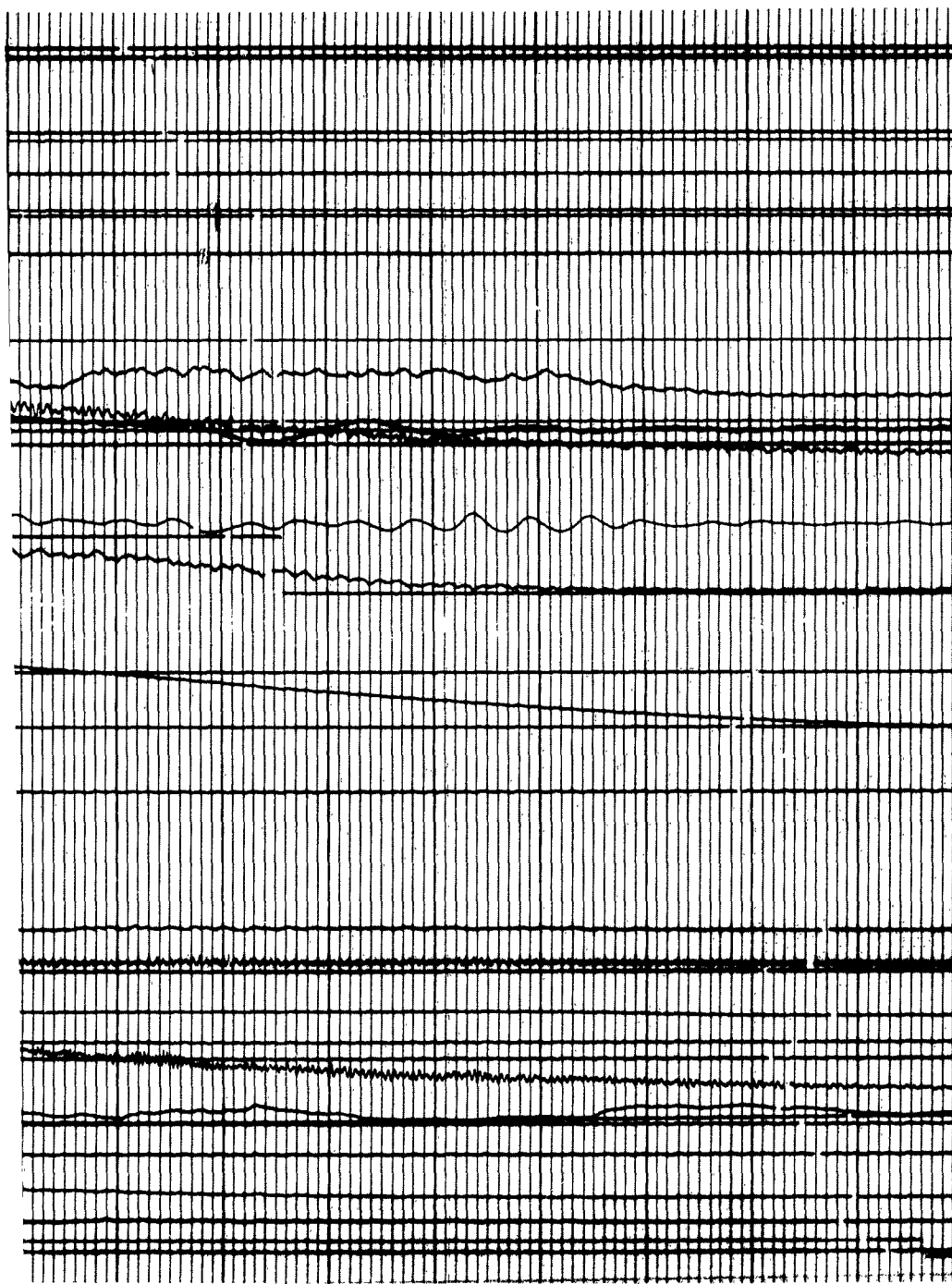
Figure 18 . Main Engine Typical Start  
Oscillographic Recording

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2



3

Figure 19 . Main Engine Typical Cutoff  
Oscillographic Recording

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TABLE 10

PRELAUNCH PROPELLANT CONSUMPTION\*

System	Propellant	
	LOX, pounds	Fuel, pounds
Vernier	6.17	4.52
Gas Generator	1.94	5.38
Ignition	--	3.12
Total Start Tank	8.11	13.02
Heat Exchanger	6.53	
Main Chamber	305	130

\*Based on static test performance with 15 to 30  
minute LOX chilldown

TABLE 11

START TANK REFILL CHARACTERISTICS

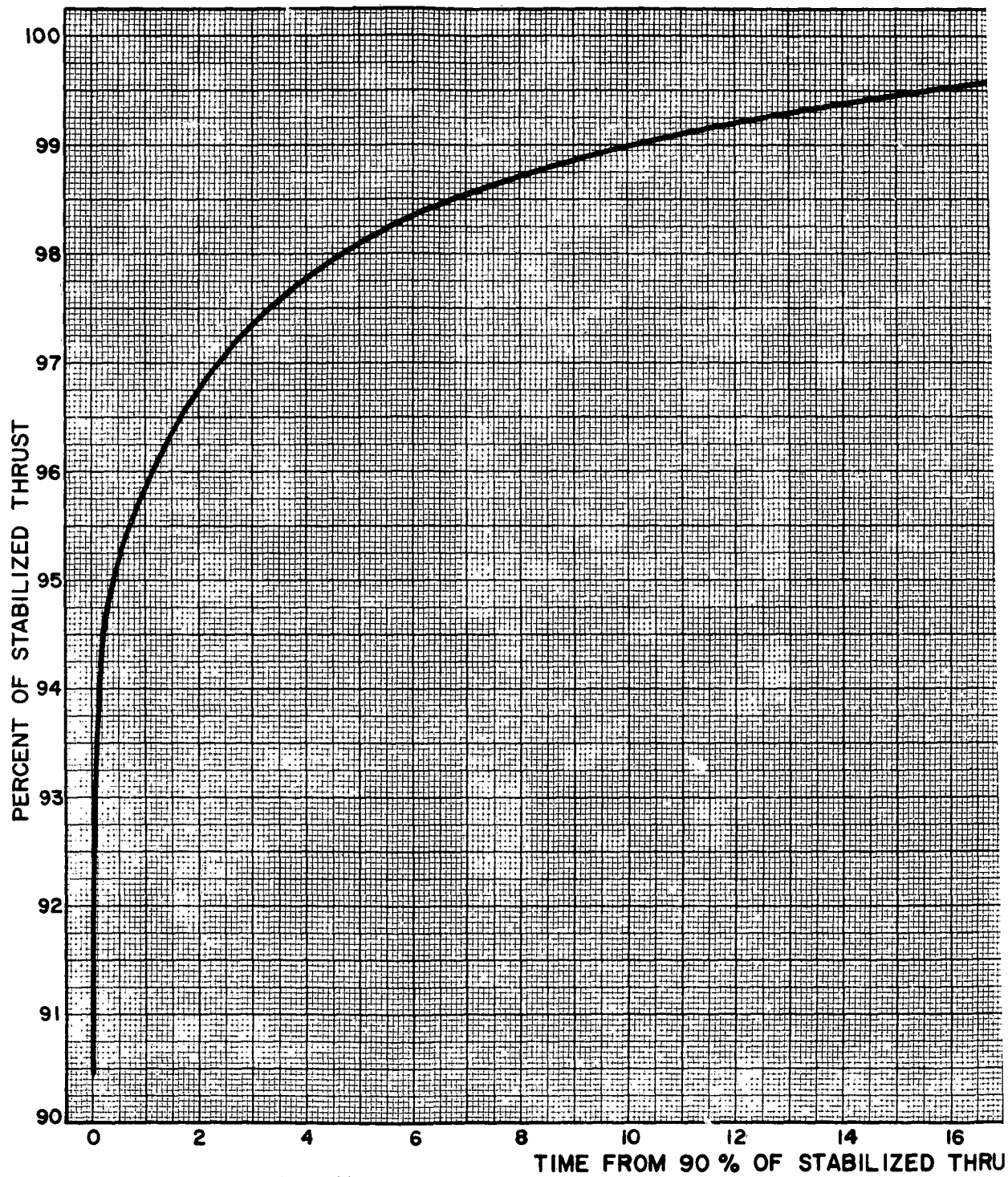
Start Tank	Normal Test Stand Start		Missile Simulated Start		Overboard Flowrate, lb/sec
	Refill Time*, seconds	Refill Rate, lb/sec	Refill Time*, seconds	Refill Rate, lb/sec	
Oxidizer	22	0.37	50	0.19	0.20
Fuel	60	0.20	60	0.20	0.02

\*Time from 90% chamber pressure to refill indication

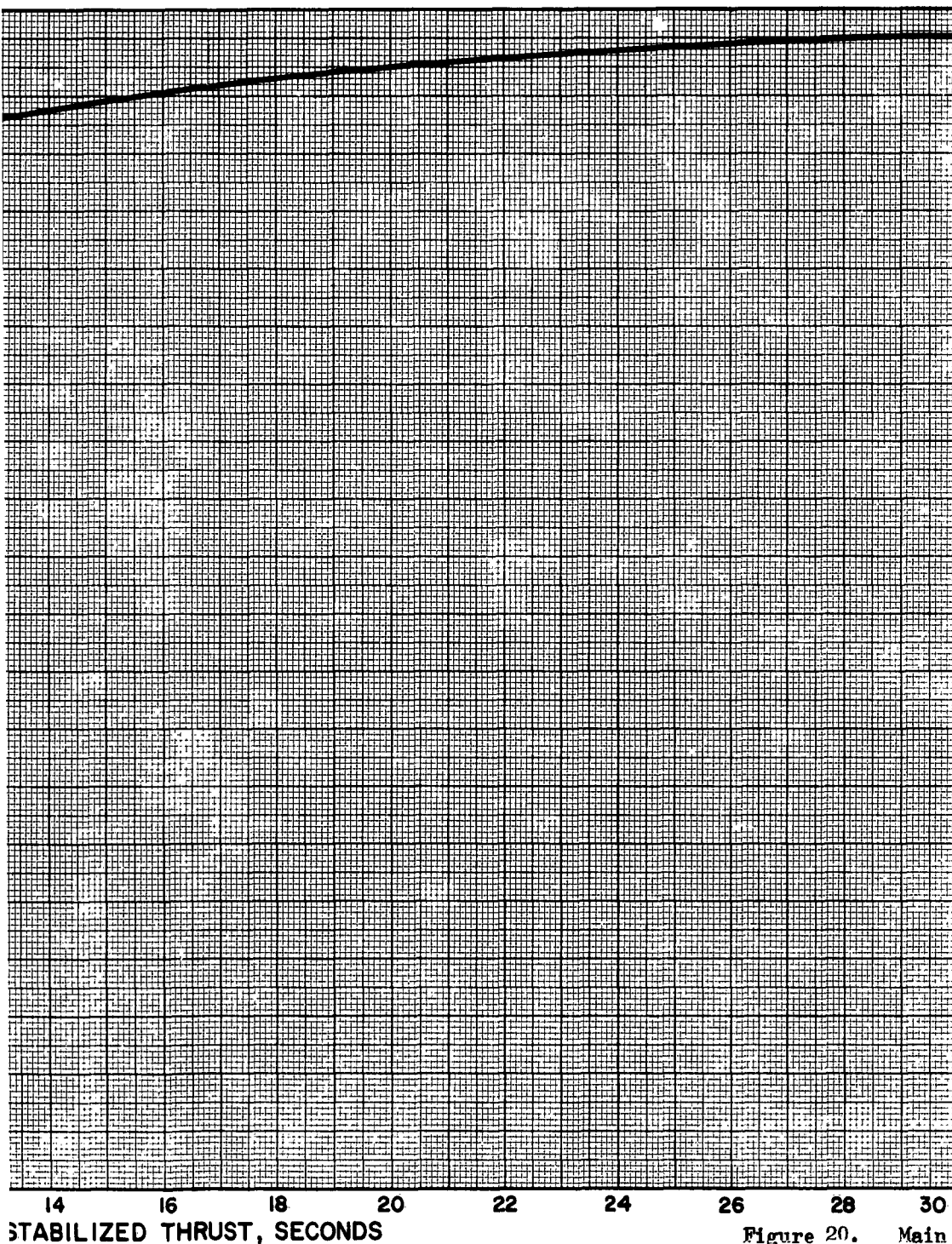
#### STABILIZATION CHARACTERISTICS

Gradual stabilizing of pressure-flow parameters under self-sustained operating conditions (bootstrapped power package) is a characteristic of liquid propellant engines with orificed control of gas generator propellant supply flows. The main engine generally attains stabilized operation 30 seconds from 90%. Varying test conditions and random engine hardware influences can, however, result in stabilization times ranging from 15 to 35 seconds from 90%.

The average thrust buildup from 90% to stabilized operation is shown in Fig. 20. Figures 21 through 23 present typical pump, chamber, and auxilliary systems stabilization characteristics (including vernier engines). The test from which the latter relationships were obtained stabilized in 20 seconds, which is not an abnormal condition.



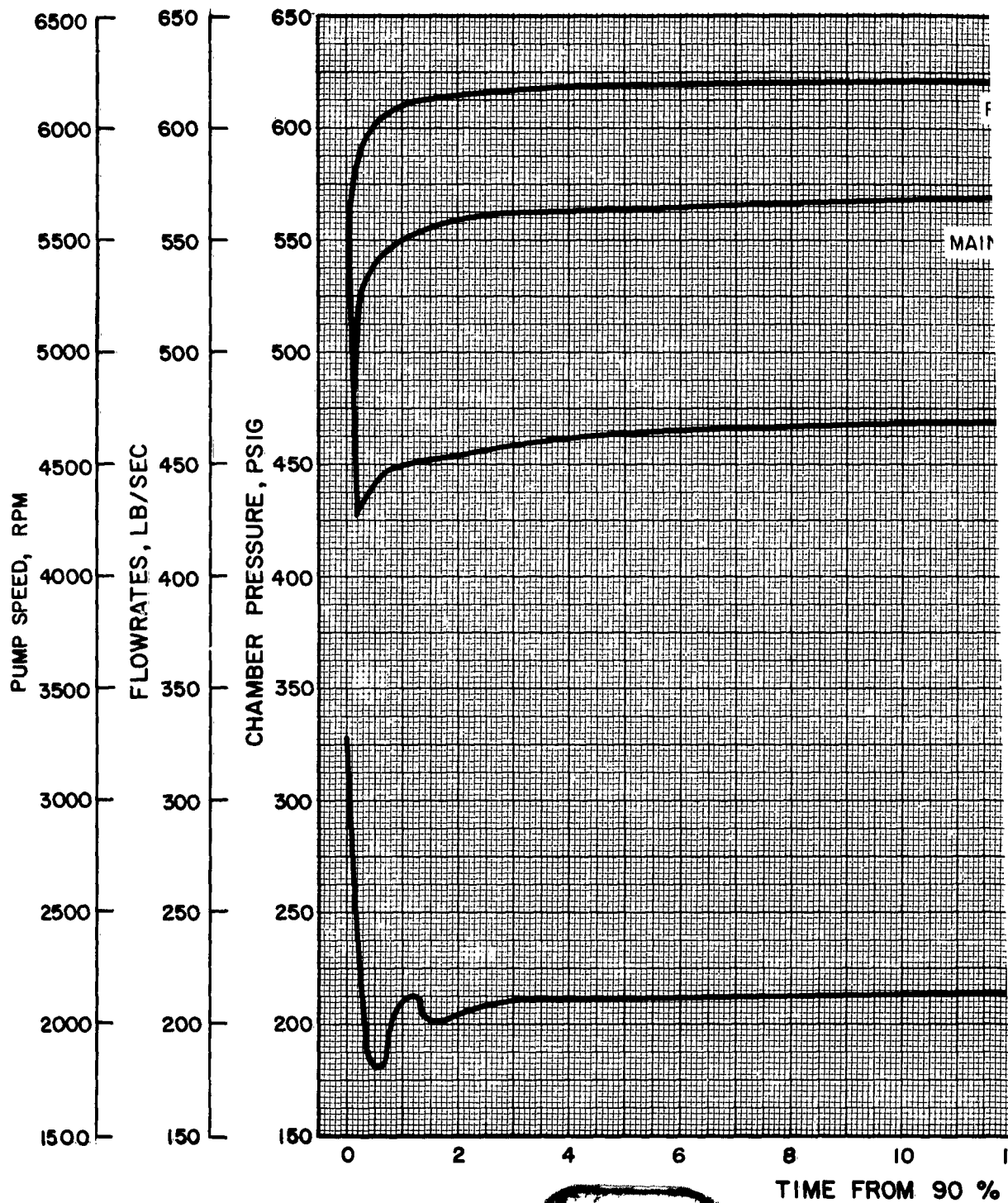




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Figure 20. Main Engine Thrust Stabilization Characteristics

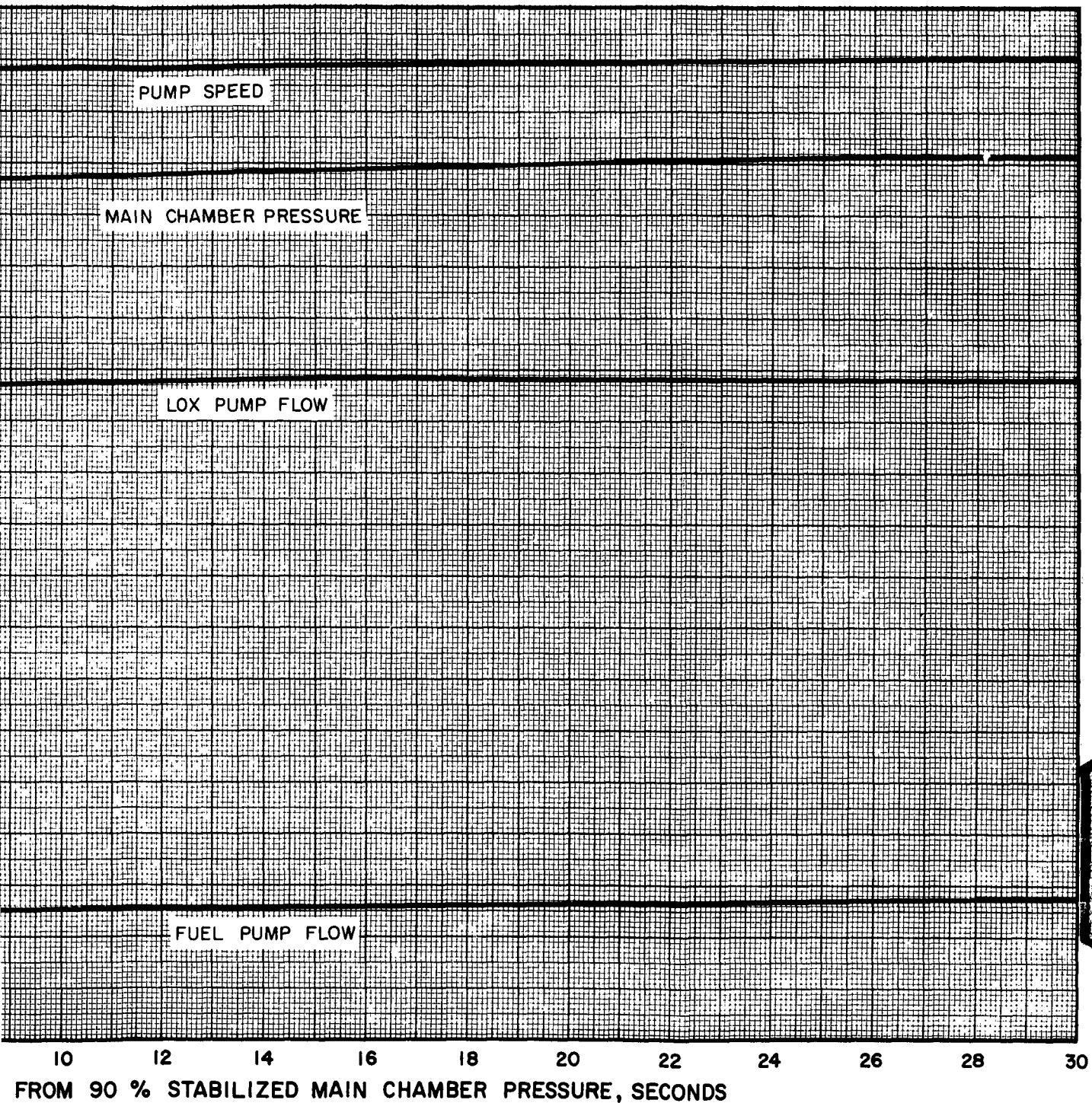




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Figure 21. Main Engine System  
Stabilization Characteristics

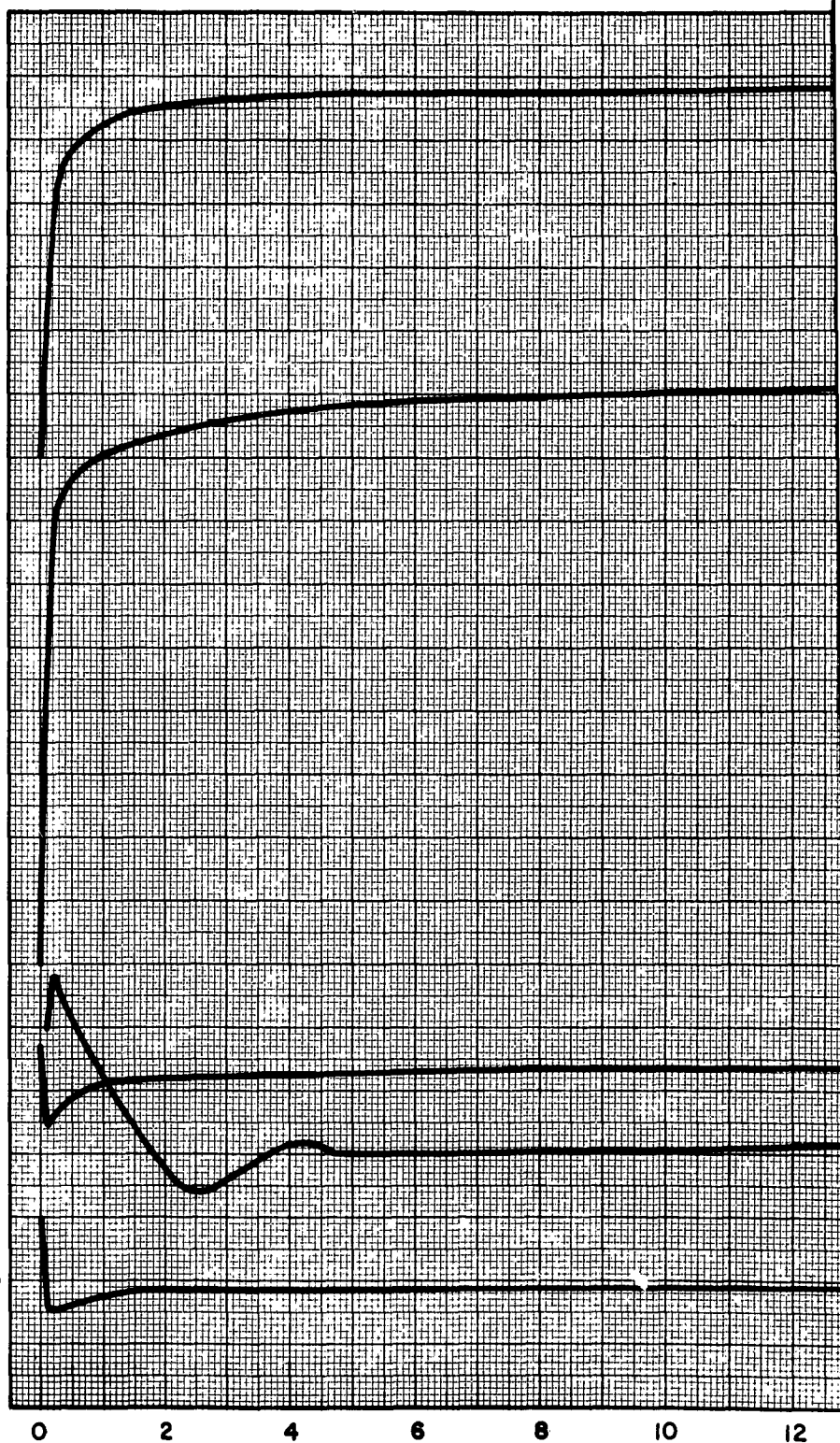
1

FLOWRATES, LB/SEC

12  
11  
10  
9  
8  
7  
6  
5  
4  
3  
2  
1

PRESSURE, PSIG

520  
480  
440  
400  
360  
320  
280  
240  
200



TIME FROM 90% MA

GAS GENERATOR FUEL FLOW

GAS GENERATOR CHAMBER PRESSURE

GAS GENERATOR LOX FLOW

HEAT EXCHANGER LOX FLOW

IGNITER FUEL FLOW

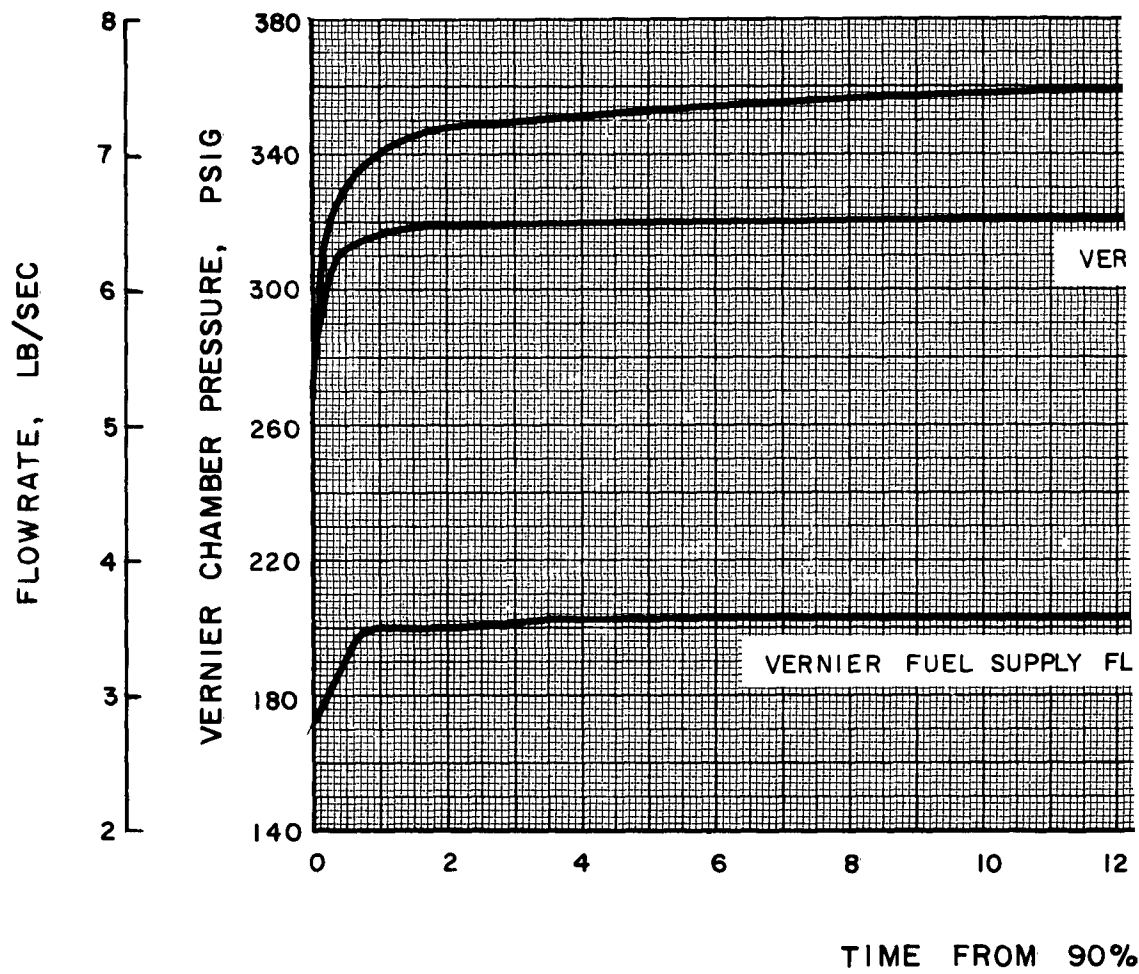
10 12 14 16 18 20 22 24 26 28 30

FROM 90% MAIN CHAMBER PRESSURE, ~SECONDS

Figure 22. Gas Generator and Auxiliary Flows  
Stabilization Characteristics

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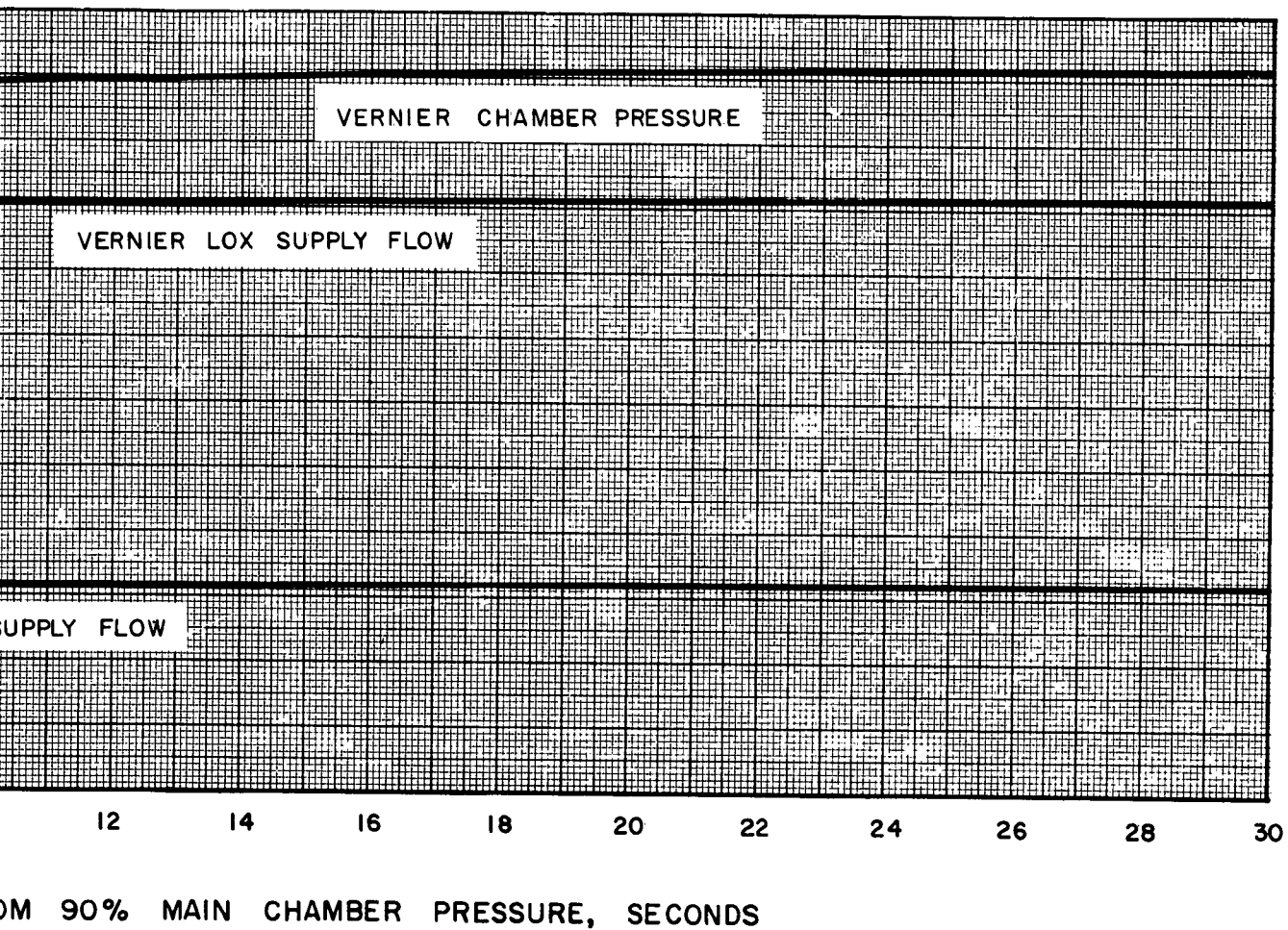
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2

Figure 23. Vernier System Stabilization Characteristics